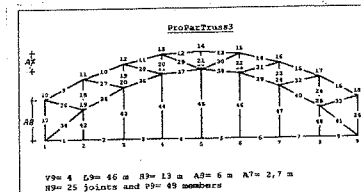
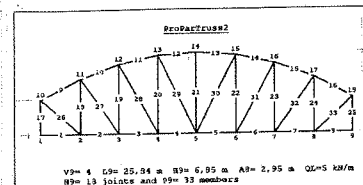
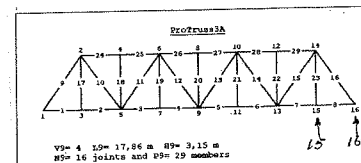
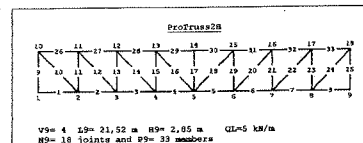
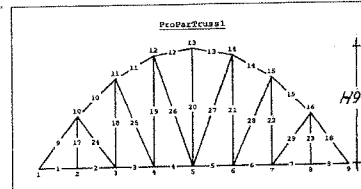
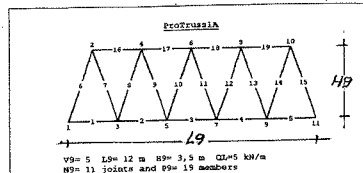


Part 10

Program **TRUSSPROGRAM4444**

Calculation of member(end) forces and joint displacements of several trusses.

1 - 8



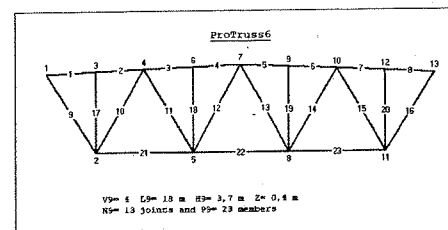
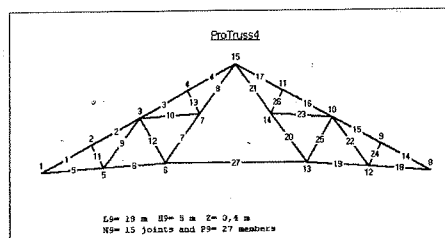
Trusses with movable force systems.

9 -20

Program **TRUSSPROGRAM5555**

'Roof trusses'

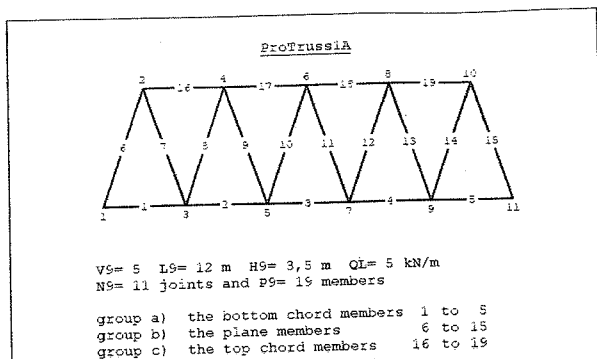
21-30



Program code for the construction data of these 'roof trusses'.

31-41

Own weight, joint loads, wind and snow loads.



STORE NR= GET

Storing following data.

V9, L9, H9, A8, A7, QL, QE, N9, P9, MF, TRU, MF
 TRU is truss number.

```

For P=1 To P9
LL(P), HH(P), A11(P), NFH(P), EAA(P), QEE(P)
Next P
For I=1 To N9
FX(I), PH(I), SH(I), X1(I)
FY(I), PV(I), SV(I), Y1(I)
Next I
For I=1 To MF : MFF(I), MA(I) : Next I
  
```

TNVF, suppose 2 vertical load forces to put in, $FY(4) = -12$ and $FY(6) = -15$, then type 2 in text box TNVF and in TSTRING 4, -12 Enter and 6, -15 Enter.

Mobile load force system, input variables in TSTRING.
 A click on ForceDivision determines all load force cases, a click on

CalculateMobForces calculates the member end forces for all the cases, plus the largest member tension and compression force for each group of members.

For the second form, click go to FDATA, for printing results on the form or printed by the printer. Shown with the examples.

TRUSSPROGRAM444 and form controls.

Preprogrammed data with a click on EX1A to EX3, combined with their preprogrammed truss data with ProTruss1A to ProParTruss3.
 Click both EX1A and ProTruss1A, and Show shows the data belonging to them.

These data of EX1A can be put in in the text boxes TV9, TL9, TH9, TA8 and TA9.

TQL for the distributed load QL for all bottom chord members. If not given at the start then type in TQL a value and click again the concerning truss, click Show and its there.

TQE for own weight QE for all members.

The large text TSTRING.

If $PV(3) = 1$ then the vertical displacement of joint 3 is prescribed, start value $UV(3) = 0$. To give it a value e.g. 7 (/EA) then to type in TSTRING PV(3)=7 Enter.

This way following variables can get a value, displacement values UH(), UV(), prescribed values PV(), PH(), 1 or 0, joint load values FX() and FY().
 E.g. FY(4)=-12 Enter, FY(6)=-15 Enter.

Strain stiffness of members.

For the trusses all strain stiffnesses at the start are $1 \cdot EA$. Suppose members 16 to 19 get another value, $1.3 \cdot EA$.

PEAA, P1, P2, ST, EA To type in TSTRING PEAA, 16, 19, 1, 1.3 Enter.

Numbering step $ST = 1$, 16-17-18-19. In some cases step $ST = 2$.

And for a single member $P = 17$ with PEAA, 17, 17, 1, 1.3 Enter.

Own weight of members.

For the trusses own weight $QE = 0$ at the start. When typing a value in text box TQE all members get that value.

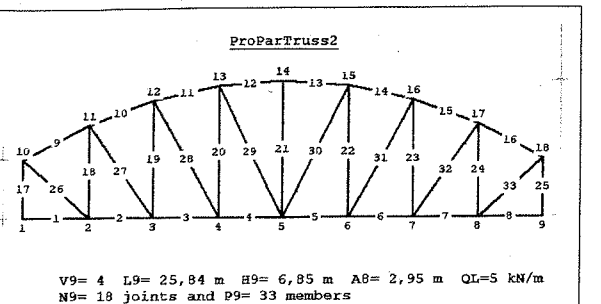
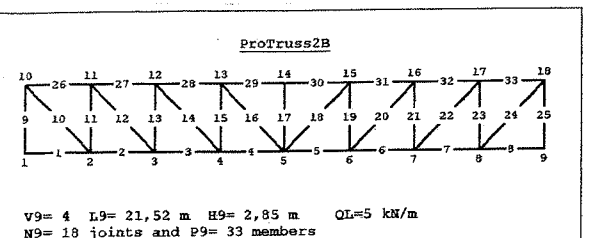
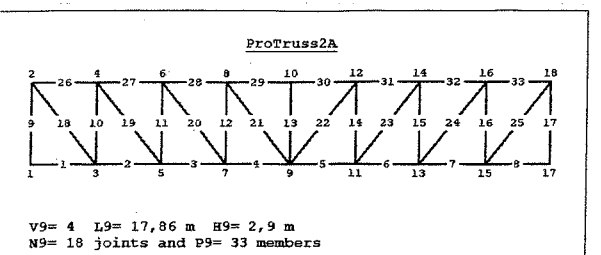
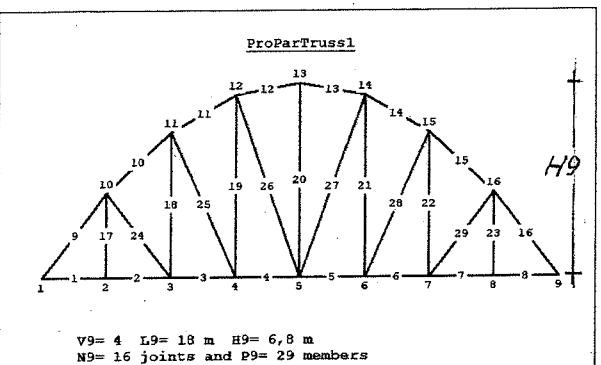
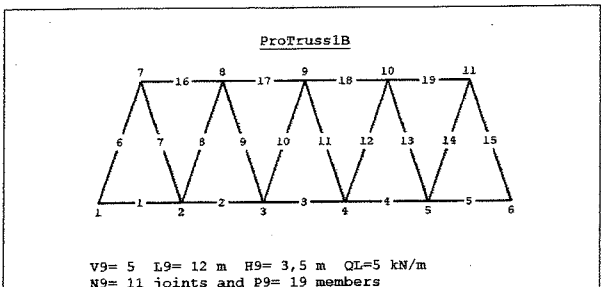
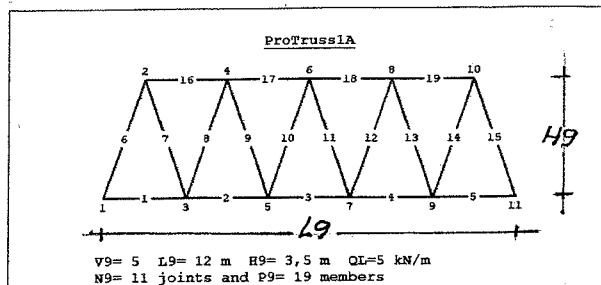
Suppose members 6 to 15 get another value, $QE = 0.7$ kN/m.

PQEE, P1, P2, ST, QE To type in TSTRING PQEE, 6, 15, 1, .7 Enter.

A click on UH(I)=0 UV(I)=0 makes all 'displacements' to be calculated zero again.

V9=	L9=	H9=	A8=	<u>AOagain</u>	<u>ProTruss1A</u>	<u>ProTruss1B</u>	<u>ProParTruss1</u>	E n d
A7=	<u>Show</u>		<u>OK</u>	EX1A	EX1B	EX1		
NVF=	QL=	QE=	<u>Calculate</u>	EX2A	EX2B	EX2		
Loads zero	<u>STORE</u>	NR=	<u>GET</u>	EX3A	EX3B	EX3		
PrF	IRO	<u>ForceDivision</u>	<u>CalculateMobForces</u>	<u>go to FDATA</u>	<u>DrawTF</u>	<u>TrussNumb</u>	<u>DrawTFD</u>	Cls

<u>Cls</u>	<u>MFORCES</u>	<u>AMEFORCES</u>	<u>PDATA</u>	<u>X1Y1</u>	<u>FXFY</u>	<u>UHUV</u>	<u>MOBMFORCES</u>	E N D
	<u>MFORCESPR</u>	<u>AMEFORCESPR</u>	<u>MOBMFORCESPR</u>	<u>SHORT</u>				
PrF	back to form TRUSSPROGRAM4						PrPr OK	



Nine trusses with preprogrammed data.

ProTruss1A Bottom chord with V9=5 spans
Length L9= 12 m Height H9= 3,5 m
For a quick view click [EX1A](#) for these data, and
click [ProTruss1A](#), becoming blue,
click [DrawTF](#) to draw the truss,
click [TrussNumb](#) to number joints and members,
click [Calculate](#) and [DrawTFD](#) to draw the deformation of the truss.

ProTruss1B Like ProTruss1A but with different joint numbering, with [EX1B](#).

ProParTruss1 With [EX1](#).

ProTruss1A	ProTruss1B	ProParTruss1
EX1A	EX1B	EX1
ProTruss2A	ProTruss2B	ProParTruss2
EX2A	EX2B	EX2
ProTruss3A	ProTruss3B	ProParTruss3
EX3A	EX3B	EX3
DrawTF	TrussNumb	DrawTFD

End

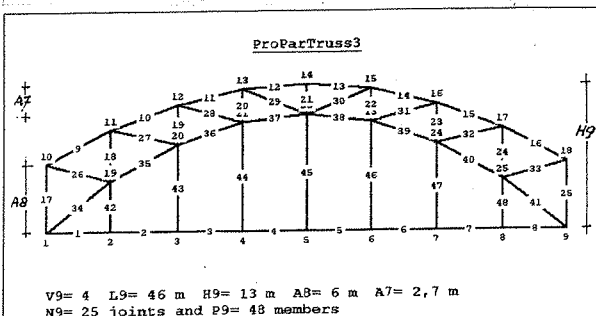
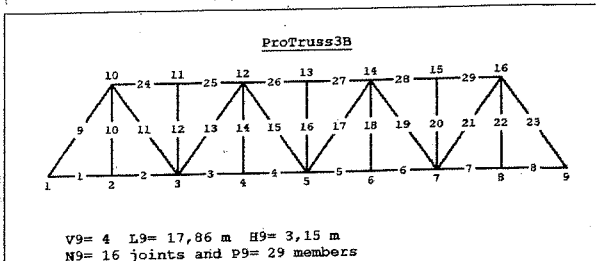
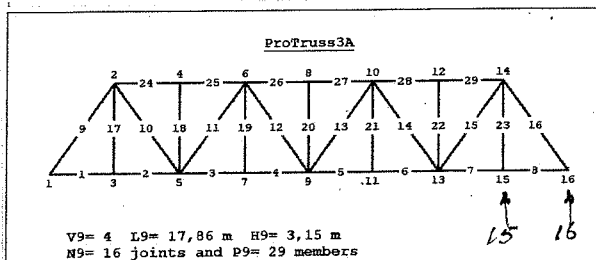
ProTruss2A [EX2A](#) and **ProTruss2B** [EX2B](#), same truss but with different joint and member numbering.

ProParTruss2 with [EX2](#).

ProTruss3A [EX3A](#) with an irregular bottom chord joint numbering, this picture with 1-3-5-7-9-11-13-15-16, no problem, but movable load system cannot be applied; a warning is given when trying it.

ProTruss3B [EX3B](#) like truss **ProTruss3A** but with different joint and member numbering.

ProParTruss3 with [EX3](#).



Examples TRUSSPROGRAM444.

ProTruss1A EX1A

Main variables to put in.
V9=4 number of spans, equal joint distances,
L9=12 m length of the truss, and
H9=2 m height of the truss.

QL=8 kN/m Q loads on the bottom chords.

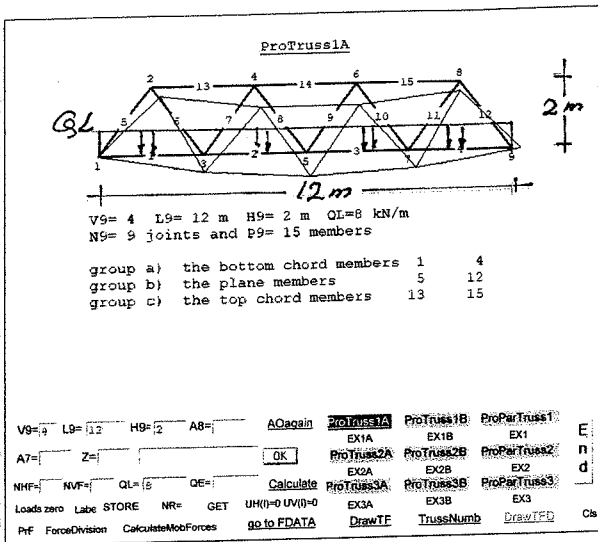
To get this truss input as follows.
At the start cursor in TV9, type 4, next Tab,
cursor in TL9, type 12 and Tab, cursor in TH9,
type 2.
Click in TQL and type 8 for the distributed
load on the bottom chords.

Click ProTruss1A, becomes blue. All members got
strain stiffness EAA(P)=1.
Click DRAWTF to draw the truss and prints the
data appearing below the drawn truss, with the
member groups with member numbers.
Click TrussNumb numberig joints and members.
Click Calculate, for the main calculations,
DRAWTFD gets enabled, and click DRAWTFD to draw
the deformed truss.

Or, at the start, click EX1A, giving data
V9=5, L9=12 m, H9=2 m and QL=8 kN/m. Next
click ProTruss1A, DRAWTF, Calculate, DRAWTFD.

Click go to FDATA, the second form, and click
PDATA to print member data P EA L1 QE, and
FXFY for joint load forces FX(I) and FY(I) and
reactions RH(I) and RV(I), and joint displacements
UH(I) and UV(I).

Click PrF to print it like (partly) shown here
below, on the left 45% size.



Member P, strain stiffness EA, length L1 and own weight QE.											
P	EA	L1	QE	P	EA	L1	QE	P	EA	L1	QE
1	1,00	3,00	0,00	2	1,00	3,00	0,00	3	1,00	3,00	0,00
5	1,00	2,50	0,00	6	1,00	2,50	0,00	7	1,00	2,50	0,00
9	1,00	2,50	0,00	10	1,00	2,50	0,00	11	1,00	2,50	0,00
13	1,00	3,00	0,00	14	1,00	3,00	0,00	15	1,00	3,00	0,00

Joint load forces FX(I) and FY(I).											
FX(1)	=	0 kN	FX(2)	=	0 kN	FX(3)	=	0 kN	FX(4)	=	0 kN
FX(5)	=	0 kN	FX(6)	=	0 kN	FX(7)	=	0 kN	FX(8)	=	0 kN
FX(9)	=	0 kN	FX(10)	=	0 kN	FX(11)	=	0 kN	FX(12)	=	0 kN
FX(13)	=	0 kN	FX(14)	=	0 kN	FX(15)	=	0 kN	FX(16)	=	0 kN

Support reactions RH(I) and RV(I).											
RH(1)	=	0,00 kN	RV(1)	=	48,00 kN	RH(2)	=	0,00 kN	RV(2)	=	48,00 kN
RH(3)	=	0,00 kN	RV(3)	=	48,00 kN	RH(4)	=	0,00 kN	RV(4)	=	48,00 kN
RH(5)	=	0,00 kN	RV(5)	=	48,00 kN	RH(6)	=	0,00 kN	RV(6)	=	48,00 kN
RH(7)	=	0,00 kN	RV(7)	=	48,00 kN	RH(8)	=	0,00 kN	RV(8)	=	48,00 kN

Member P, strain stiffness EA, length L1 and own weight QE.											
P	EA	L1	QE	P	EA	L1	QE	P	EA	L1	QE
1	1,00	3,00	0,00	2	1,00	3,00	0,00	3	1,00	3,00	0,00
5	1,00	2,50	0,00	6	1,00	2,50	0,00	7	1,00	2,50	0,00
9	1,00	2,50	0,00	10	1,00	2,50	0,00	11	1,00	2,50	0,00
13	1,00	3,00	0,00	14	1,00	3,00	0,00	15	1,00	3,00	0,00

Joint coordinates X1(I) and Y1(I).											
X1(1)	=	0 m	Y1(1)	=	0 m	X1(2)	=	1,500 m	Y1(2)	=	2,000 m
X1(3)	=	3,000 m	Y1(3)	=	0 m	X1(4)	=	4,500 m	Y1(4)	=	2,000 m
X1(5)	=	6,000 m	Y1(5)	=	0 m	X1(6)	=	7,500 m	Y1(6)	=	2,000 m

Joint load forces FX(I) and FY(I).											
FX(1)	=	0 kN	FX(2)	=	0 kN	FX(3)	=	0 kN	FX(4)	=	0 kN
FX(5)	=	0 kN	FX(6)	=	0 kN	FX(7)	=	0 kN	FX(8)	=	0 kN
FX(9)	=	0 kN	FX(10)	=	0 kN	FX(11)	=	0 kN	FX(12)	=	0 kN
FX(13)	=	0 kN	FX(14)	=	0 kN	FX(15)	=	0 kN	FX(16)	=	0 kN

Support reactions RH(I) and RV(I).											
RH(1)	=	0,00 kN	RV(1)	=	48,00 kN	RH(2)	=	0,00 kN	RV(2)	=	48,00 kN
RH(3)	=	0,00 kN	RV(3)	=	48,00 kN	RH(4)	=	0,00 kN	RV(4)	=	48,00 kN
RH(5)	=	0,00 kN	RV(5)	=	48,00 kN	RH(6)	=	0,00 kN	RV(6)	=	48,00 kN

Joint displacements UH(I) and UV(I).											
UH(1)	=	0 /EA	UV(1)	=	0 /EA	UH(2)	=	540 /EA	UV(2)	=	-546 /EA
UH(3)	=	81 /EA	UV(3)	=	-1031 /EA	UH(4)	=	378 /EA	UV(4)	=	-1300 /EA
UH(5)	=	270 /EA	UV(5)	=	-1428 /EA	UH(6)	=	162 /EA	UV(6)	=	-1300 /EA

ProTruss1A

group a) the bottom chord members

```

MFS(1) = 27,00 kN      NAA(3,1) = 27,00      MFS(2) = 63,00 kN      NAA(5,3) = 63,00
NAA(1,3) = -27,00      DAA(3,1) = 0,00      DAA(3,5) = 0,00      NAA(5,3) = 0,00
MFS(3) = 63,00 kN      MFS(4) = 27,00 kN      NAA(7,5) = 27,00      DAA(7,9) = 27,00
NAA(5,7) = -63,00      NAA(7,5) = 63,00      NAA(7,9) = -27,00      DAA(9,7) = 0,00
DAA(5,7) = 0,00        DAA(7,5) = 0,00        DAA(7,9) = 0,00
LTF(2) = 63,00 kN      LCF(0) = 0,00 kN

```

group b) the plane members

```

MFS(5) = -45,00 kN      NAA(2,1) = -45,00      NAA(2,3) = -45,00      NAA(3,2) = 45,00
NAA(1,2) = 45,00        DAA(2,1) = 0,00        DAA(2,3) = 0,00        DAA(3,2) = 0,00
MFS(7) = -15,00 kN      NAA(4,3) = -15,00      MFS(8) = 15,00 kN      NAA(5,4) = 15,00
DAA(3,4) = 0,00        DAA(4,3) = 0,00        DAA(4,5) = 0,00        DAA(5,4) = 0,00
MFS(9) = 15,00 kN      NAA(6,5) = 15,00      MFS(10) = -15,00 kN    NAA(7,6) = -15,00
DAA(5,6) = -15,00       DAA(6,5) = 0,00        DAA(6,7) = 0,00        DAA(7,6) = 0,00
MFS(11) = 45,00 kN      NAA(8,7) = 45,00      MFS(12) = -45,00 kN    NAA(9,8) = -45,00
NAA(7,8) = -45,00       DAA(8,7) = 0,00        DAA(8,9) = 0,00        DAA(9,8) = -45,00
DAA(7,8) = 0,00        LCF(5) = -45,00 kN
LTF(11) = 45,00 kN

```

group c) the top chord members

```

MFS(13) = -54,00 kN     NAA(4,2) = -54,00      NAA(4,6) = 72,00       NAA(6,4) = -72,00
NAA(2,4) = 54,00        DAA(4,2) = 0,00        DAA(4,6) = 0,00        DAA(6,4) = 0,00
MFS(15) = -54,00 kN     NAA(8,6) = -54,00
NAA(6,8) = 54,00        DAA(8,6) = 0,00
DAA(6,8) = 0,00        LCF(14) = -72,00 kN
LTF(0) = 0,00 kN

```

☐ CIs ☐ MFORCES ☐ AMEFORCES ☐ PDATA ☐ X1Y1 ☐ FXFY ☐ UHUV ☐ MOBMFORCES ☐ E N D
☐ DrawTPR ☐ MFORCESPR ☐ AMEFORCESPR ☐ MOBMFORCESPR ☐ SHORT ☐ PPr OK
PPr back to form TRUSSPROGRAM

Going on with FDATA.

A click on AMEFORCES prints

'member forces' MFS(P),
Member end forces NAA(L,H) and NAA(H,L) and
perpendicular to the member axis
DAA(L,H) and DAA(H,L) and
the largest 'member force' MFS() for each
group of members.

ProTruss1A

group a) the bottom chord members

```

MFS(1) = 27,00 kN      MFS(2) = 63,00 kN      MFS(3) = 63,00 kN      MFS(4) = 27,00 kN
LTF(2) = 63,00 kN      LCF(0) = 0,00 kN

```

group b) the plane members

```

MFS(5) = -45,00 kN      MFS(6) = 45,00 kN      MFS(7) = -15,00 kN      MFS(8) = 15,00 kN
NAA(2,3) = -45,00       NAA(3,2) = 45,00       NAA(5,4) = 15,00       NAA(7,6) = -15,00
DAA(2,3) = 0,00         DAA(3,2) = 0,00         DAA(5,4) = 0,00         DAA(7,6) = 0,00
MFS(9) = 15,00 kN      MFS(10) = -15,00 kN    MFS(11) = 45,00 kN      MFS(12) = -45,00 kN
LTF(11) = 45,00 kN      LCF(5) = -45,00 kN

```

group c) the top chord members

```

MFS(13) = -54,00 kN     MFS(14) = -72,00 kN    MFS(15) = -54,00 kN
LTF(0) = 0,00 kN        LCF(14) = -72,00 kN

```

Assumed direction for NAA(L,H) and NAA(H,L) is from lowest to highest member end number.

Member 7 with L=3 and H=4, of group b).

NAA(3,4)= 15,00 kN, directed as assumed.
NAA(4,3)= -15,00 kN, not directed as assumed
but opposite directed.
Member 7 is a compression member, indicated
with a member sign, so MFS(7)= -15,00 kN.

With a click on MFORCES the largest tension
force LTF() and largest compression force LCF()
of a group are determined and printed.
Group b) LTF(11)= 45 kN and LCF(5)= -45 kN.

group b) the plane members

```

MFS(5) = -45,00 kN      NAA(2,1) = -45,00      NAA(2,3) = -45,00      NAA(3,2) = 45,00
NAA(1,2) = 45,00        DAA(2,1) = 0,00        DAA(2,3) = 0,00        DAA(3,2) = 0,00
MFS(7) = -15,00 kN      NAA(4,3) = -15,00      MFS(8) = 15,00 kN      NAA(5,4) = 15,00
DAA(3,4) = 0,00        DAA(4,3) = 0,00        DAA(4,5) = 0,00        DAA(5,4) = 0,00
MFS(9) = 15,00 kN      NAA(6,5) = 15,00      MFS(10) = -15,00 kN    NAA(7,6) = -15,00
DAA(5,6) = -15,00       DAA(6,5) = 0,00        DAA(6,7) = 0,00        DAA(7,6) = 0,00
MFS(11) = 45,00 kN      NAA(8,7) = 45,00      MFS(12) = -45,00 kN    NAA(9,8) = -45,00
NAA(7,8) = -45,00       DAA(8,7) = 0,00        DAA(8,9) = 0,00        DAA(9,8) = -45,00
DAA(7,8) = 0,00        LCF(5) = -45,00 kN
LTF(11) = 45,00 kN

```

ProTruss1A

group a) the bottom chord members

```

MFS(1) = 27,00 kN      MFS(2) = 63,00 kN      MFS(3) = 63,00 kN      MFS(4) = 27,00 kN
LTF(2) = 63,00 kN      LCF(0) = 0,00 kN

```

group b) the plane members

```

MFS(5) = -45,00 kN      MFS(6) = 45,00 kN      MFS(7) = -15,00 kN      MFS(8) = 15,00 kN
MFS(9) = 15,00 kN      MFS(10) = -15,00 kN    MFS(11) = 45,00 kN      MFS(12) = -45,00 kN
LTF(11) = 45,00 kN      LCF(5) = -45,00 kN

```

group c) the top chord members

```

MFS(13) = -54,00 kN     MFS(14) = -72,00 kN    MFS(15) = -54,00 kN
LTF(0) = 0,00 kN        LCF(14) = -72,00 kN

```

ProTruss1B

V9= 5 L9= 12 m H9= 3 m QL= 4 kN/m
N9= 11 joints and P9= 19 members

group a) the bottom chord members 1 5
group b) the plane members 6 15
group c) the top chord members 16 19

Label1 Label1 Label1 Label1

V9= L9= H9= A8= AOagain ProTruss1A ProTruss1B ProParTruss1
A7= Show EX1A EX1B EX1
OK ProTruss2A ProTruss2B ProParTruss2
NHFF= NVF= QL= QE= Calculate EX2A EX2B EX2
ProTruss3A ProTruss3B ProParTruss3
Loads zero STORE NR= GET UH(1)=0 UV(1)=0 EX3A EX3B EX3
P/F IRO ForceDivision CalculateMobForces go to FDATA DrawTF TrussNumb DrawTFD Cts

ProTruss1B
group a) the bottom chord members

MFS(1) = 7,68 kN	MFS(2) = 19,20 kN
NAA(1,2) = -7,68	NAA(2,3) = -19,20
DAA(1,2) = 0,00	DAA(2,3) = 0,00
MFS(3) = 23,04 kN	MFS(4) = 15,20 kN
NAA(3,4) = -23,04	NAA(4,5) = -19,20
DAA(3,4) = 0,00	DAA(4,5) = 0,00
MFS(5) = 7,68 kN	MFS(6) = 7,68
NAA(5,6) = -7,68	NAA(6,5) = 7,68
DAA(5,6) = 0,00	DAA(6,5) = 0,00
LTF(3) = 23,04 kN	LTF(10) = 0,00 kN

group b) the plane members

MFS(7) = -20,68 kN	MFS(7) = 20,68 kN
NAA(1,7) = 20,68	NAA(2,7) = -20,68
DAA(1,7) = 0,00	DAA(2,7) = 0,00
MFS(8) = -10,34 kN	MFS(9) = 10,34 kN
NAA(2,8) = 10,34	NAA(3,9) = -10,34
DAA(2,8) = 0,00	DAA(3,9) = 0,00
MFS(10) = 0,00 kN	MFS(11) = 0,00 kN
NAA(3,10) = 0,00	NAA(4,11) = 0,00
DAA(3,10) = 0,00	DAA(4,11) = 0,00
MFS(12) = 10,34 kN	MFS(13) = -10,34 kN
NAA(4,12) = -10,34	NAA(5,13) = 10,34
DAA(4,12) = 0,00	DAA(5,13) = 0,00
MFS(14) = 20,68 kN	MFS(15) = -20,68 kN
NAA(5,14) = -20,68	NAA(6,15) = 20,68
DAA(5,14) = 0,00	DAA(6,15) = 0,00
LTF(7) = 20,68 kN	LTF(15) = -20,68 kN

group c) the top chord members

MFS(16) = -15,36 kN	MFS(17) = -23,04 kN
NAA(7,16) = 15,36	NAA(8,17) = 23,04
DAA(7,16) = 0,00	DAA(8,17) = 0,00

Joint load forces FX(I) and FY(I)

FX(1) = 0 kN	FY(1) = -4,80 kN	FX(2) = 0 kN	FY(2) = -5,60 kN
FX(3) = 0 kN	FY(3) = -5,60 kN	FX(4) = 0 kN	FY(4) = -5,60 kN
FX(5) = 0 kN	FY(5) = -5,60 kN	FX(6) = 0 kN	FY(6) = -4,80 kN
FX(7) = 0 kN	FY(7) = 0 kN	FX(8) = 0 kN	FY(8) = 0 kN
FX(9) = 0 kN	FY(9) = 0 kN	FX(10) = 0 kN	FY(10) = 0 kN
FX(11) = 0 kN	FY(11) = 0 kN		

Support reactions RH(I) and RV(I)

RH(1) = 0,00 kN	RV(1) = 24,00 kN	RV(6) = 24,00 kN
-----------------	------------------	------------------

Joint displacements UH(I) and UV(I)

UH(1) = 0,0 /EA	UV(1) = -3,3 /EA	UH(2) = 13,4 /EA	UV(2) = -234,0 /EA
UH(3) = 64,5 /EA	UV(3) = -440,8 /EA	UH(4) = 119,8 /EA	UV(4) = -440,8 /EA
UH(5) = 165,9 /EA	UV(5) = -294,0 /EA	UH(6) = 184,3 /EA	UV(6) = 0,0 /EA
UH(7) = 184,3 /EA	UV(7) = -145,7 /EA	UH(8) = 147,5 /EA	UV(8) = -371,6 /EA
UH(9) = 92,2 /EA	UV(9) = -451,8 /EA	UH(10) = 36,9 /EA	UV(10) = -371,6 /EA
UH(11) = 0,0 /EA	UV(11) = -145,7 /EA		

Support reactions RH(I) and RV(I)

RH(1) = 0,00 kN	RV(1) = 24,00 kN	RV(6) = 24,00 kN
-----------------	------------------	------------------

Joint displacements UH(I) and UV(I)

UH(1) = 0,0 /EA	UV(1) = 0,0 /EA	UH(2) = 5,2 /EA	UV(2) = -214,0 /EA
UH(3) = 32,3 /EA	UV(3) = -328,3 /EA	UH(4) = 69,9 /EA	UV(4) = -328,3 /EA
UH(5) = 92,9 /EA	UV(5) = -214,0 /EA	UH(6) = 52,2 /EA	UV(6) = 0,0 /EA
UH(7) = 92,9 /EA	UV(7) = -139,8 /EA	UH(8) = 73,7 /EA	UV(8) = -275,9 /EA
UH(9) = 46,1 /EA	UV(9) = -333,9 /EA	UH(10) = 18,4 /EA	UV(10) = -275,9 /EA
UH(11) = 0,0 /EA	UV(11) = -108,8 /EA		

MFS(2) = 19,20 kN	
NAA(2,3) = -19,20	NAA(3,2) = 19,20
DAA(2,3) = 0,00	DAA(3,2) = 0,00
MFS(9) = 10,34 kN	
NAA(3,8) = -10,34	NAA(8,3) = 10,34
DAA(3,8) = 0,00	DAA(8,3) = 0,00
MFS(17) = -23,04 kN	
NAA(8,9) = 23,04	NAA(9,8) = -23,04
DAA(8,9) = 0,00	DAA(9,8) = 0,00

ProTruss1B EX1B

First case.

Basic variables to put in.
V9=5 number of spans, equal joint distances,
real number of spans becomes 2*4=8.
L9=12 m length of the truss, and
H9=3 m height of the truss.
Assumed no own weight. QL= 4 kN/m.

At the start cursor in TV9, type 5, next Tab,
cursor in TL9, type 12 and Tab, cursor in TH9,
type 3. Put cursor in TQL and type 4.

Click ProTruss1B, becomes blue. All members got
strain stiffness EAA(P)=1.

Click DRAWTF to draw the truss, the data just
put in appear below it plus member data. Click
TrussNumb for joint and member numbering. Next
Calculate and DRAWTFD for the truss deformatin.

Click go to FDATA. and AMEFORCES. Results for
some members are shown on the left.
A click on UXUY shows the joint displacements.

Second case.

Click AOAgain, input like above (or click EX1B
and ProTruss1B), next DrawTF and TrussNumb.

Now some members get strainstiffness 2EA in-
stead of 1EA, the members

1 to 5 of group a) and 16 to 19 of group c).

ST=1 for step in 1,2,3,4,5 etc.

Type in TSTRING for PEAA,P1,P2,ST,EA

PEAA,1,5,1,2 Enter and PEAA,16,19,1,2 Enter.

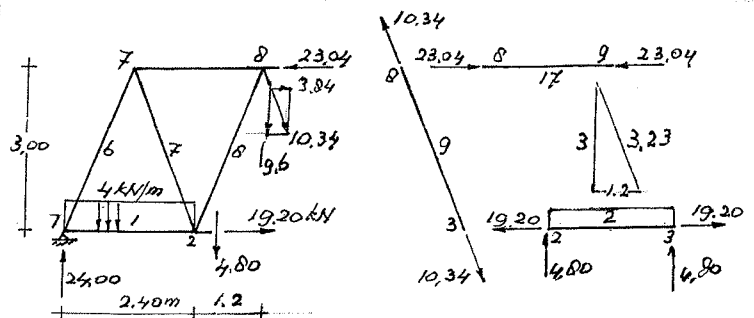
Next click Calculate, DRAWTFD and go to FDATA.

Check member 2 L= 2,4 m $\Delta L = F \cdot L / EA$

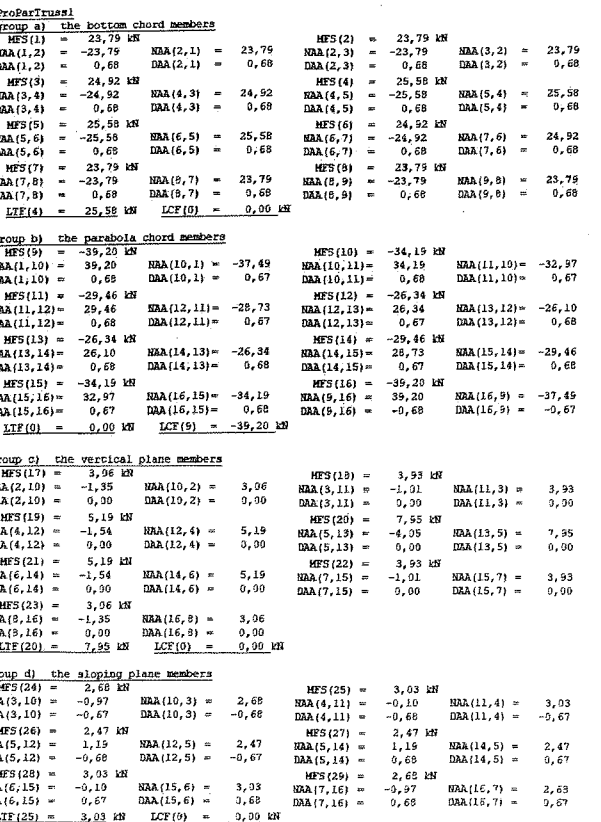
Case 1 $UH(3) - UH(2) = (64,5 - 18,4) / EA = 46,1 / EA$
 $\Delta L = (19,20 \cdot 2,4) / 1EA = 46,1 / EA$ ok

Case 2 $UH(2) - UH(3) = (32,3 - 0,2) / EA = 23,1 / EA$
 $\Delta L = (19,20 \cdot 2,4) / 2EA = 23,1 / EA$ ok

Both cases same member end forces but different
joint displacements. The truss is internally
and externally statically determinate; member
ends and joints are seen as hinges.



A part of the truss. Components of 10,34 kN,
(10,34/3,23)*1,2 = 3,84 kN and
(10,34/3,23)*3 = 9,60 kN. Equilibrium?
 Σ mom. joint 2 = 0?
 $24 \cdot 2,4 - 4 \cdot 2,4 \cdot 1,2 + 3,84 \cdot 3 + 9,6 \cdot 1,2 - 23,04 \cdot 3 =$
 $57,6 - 11,5 + 11,5 + 11,5 - 69,1 = 0$ ok



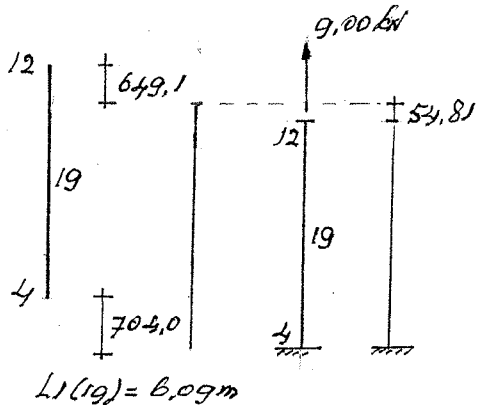
largest compression force $LCF(0)=0$, all members 4 to 29 are tension members.

group c) the vertical plane members

MFS(17) = 9,00 kN	NAA(2,10) = -9,00	NAA(10,2) = 9,00	MFS(18) = 9,00 kN	NAA(3,11) = -9,00	NAA(11,3) = 9,00
DAA(2,10) = 0,00	DAA(10,2) = 0,00		DAA(3,11) = 0,00	DAA(11,3) = 0,00	
MFS(19) = 9,00 kN	NAA(4,12) = -9,00	NAA(12,4) = 9,00	MFS(20) = 9,00 kN	NAA(5,13) = -9,00	NAA(13,5) = 9,00
DAA(4,12) = 0,00	DAA(12,4) = 0,00		DAA(5,13) = 0,00	DAA(13,5) = 0,00	
MFS(21) = 9,00 kN	NAA(6,14) = -9,00	NAA(14,6) = 9,00	MFS(22) = 9,00 kN	NAA(7,15) = -9,00	NAA(15,7) = 9,00
DAA(6,14) = 0,00	DAA(14,6) = 0,00		DAA(7,15) = 0,00	DAA(15,7) = 0,00	
MFS(23) = 9,00 kN	NAA(8,16) = -9,00	NAA(16,8) = 9,00			
DAA(8,16) = 0,00	DAA(16,8) = 0,00				
LTF(18) = 9,00 kN	LCF(9) = 0,00 kN				

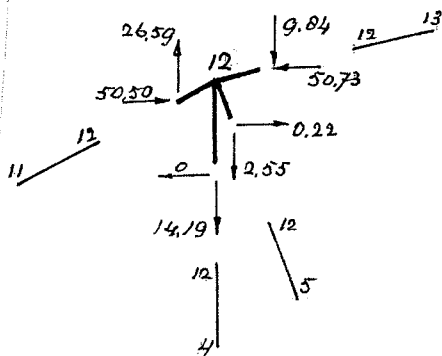
group d) the sloping plane members

MFS(24) = 0,00 kN	NAA(3,10) = 0,00	NAA(10,3) = 0,00	MFS(25) = 0,00 kN	NAA(4,11) = 0,00	NAA(11,4) = 0,00
DAA(3,10) = 0,00	DAA(10,3) = 0,00		DAA(4,11) = 0,00	DAA(11,4) = 0,00	
MFS(26) = 0,00 kN	NAA(5,12) = 0,00	NAA(12,5) = 0,00	MFS(27) = 0,00 kN	NAA(6,13) = 0,00	NAA(13,6) = 0,00
DAA(5,12) = 0,00	DAA(12,5) = 0,00		DAA(6,13) = 0,00	DAA(13,6) = 0,00	
MFS(28) = 0,00 kN	NAA(7,14) = 0,00	NAA(14,7) = 0,00	MFS(29) = 0,00 kN	NAA(8,15) = 0,00	NAA(15,8) = 0,00
DAA(7,14) = 0,00	DAA(14,7) = 0,00		DAA(8,15) = 0,00	DAA(15,8) = 0,00	
LTF(26) = 0,00 kN	LCF(24) = 0,00 kN				



group b) the parabola chord members

MFS(9) = -79,37 kN	D5(1,10) = 48,72	D6(1,10) = 62,66	MFS(10) = -67,76 kN	D5(10,11) = 49,85	D6(10,11) = 45,91
MFS(11) = -57,80 kN	D5(11,12) = 50,50	D6(11,12) = 28,12	MFS(12) = -51,67 kN	D5(12,13) = 50,73	D6(12,13) = 9,84
MFS(13) = -51,67 kN	D5(13,14) = 50,73	D6(13,14) = -8,47	MFS(14) = -57,80 kN	D5(14,15) = 50,50	D6(14,15) = -26,59
MFS(15) = -67,76 kN	D5(15,16) = 49,85	D6(15,16) = -44,09	MFS(16) = -79,37 kN	D5(16,17) = 48,72	D6(16,17) = -60,48
LTF(9) = 0,00 kN	LCF(9) = -79,37 kN				



group c) the vertical plane members

MFS(17) = 12,06 kN	D5(2,10) = 0,00	D6(2,10) = -10,35	MFS(18) = 12,93 kN	D5(3,11) = 0,00	D6(3,11) = -10,01
MFS(19) = 14,19 kN	D5(4,12) = 0,00	D6(4,12) = -10,54	MFS(20) = 16,95 kN	D5(5,13) = 0,00	D6(5,13) = -13,05
MFS(21) = 14,15 kN	D5(6,14) = 0,00	D6(6,14) = -10,54	MFS(22) = 12,93 kN	D5(7,15) = 0,00	D6(7,15) = -10,01
MFS(23) = 12,06 kN	D5(8,16) = 0,00	D6(8,16) = -10,35			
LTF(20) = 16,95 kN	LCF(9) = 0,00 kN				

group d) the sloping plane members

MFS(24) = 2,68 kN	D5(3,10) = 1,13	D6(3,10) = -0,34	MFS(25) = 3,03 kN	D5(4,11) = 0,66	D6(4,11) = 0,19
MFS(26) = 2,47 kN	D5(5,12) = 0,22	D6(5,12) = 1,35	MFS(27) = 2,47 kN	D5(6,13) = -0,22	D6(6,13) = 1,35
MFS(28) = 3,03 kN	D5(7,14) = -0,66	D6(7,14) = 0,19	MFS(29) = 2,68 kN	D5(8,15) = -1,13	D6(8,15) = -0,34
LTF(28) = 3,03 kN	LCF(9) = 0,00 kN				

Going on with ProParTruss1 preceding page.

Click back to form TRUSSPROGRAM444, click on the form next AOAgain.

V9=4 number of spans,

L9=18 m length of the truss,

H9=6,5 m height of the truss. Own weight QE=0.

Load on bottom chord members QL=4 kN/m.

Type 4 in TV9, Tab, 18 in TL9, Tab, 6.5 in TH9 and 4 in TQL, after input of these data

Click ProParTruss1,

next DrawTF, TrussNumb, controls disappear, and DrawTF is replaced by Calculate, click on it then DRAWTFD, go to FDATA, AMEFORCES two times Members of group d, in this case, are zero members because of symmetric loading.

About the vertical member 19 of group c).

The vertical member end displacements are UV(4) = -704,0/EA and UV(12) = -649,1/EA, both negative value, so not as assumed upward but downward. The member lengthens $(704,0 - 649,1)/EA = 54,90/EA$.

Suppose the member is clamped at member end 4. Member end force NAA(12,4) = 9,00 kN, that's upward as assumed.

With Hooke's $\Delta L = FL/EA$ follows

$9,00 \times 6,09 = 54,81/EA$ 'is' $94,90/EA$. ok

Going on with ProParTruss1. Click AOagain.

V9=4, L9=18 m, H9= 6,5 m and QL=4 kN/m.

After input of these data click ProParTruss1.

Next type .6 in TQE for own weight 0,6 kN/m.

Click DrawTF, TrussNumb, Calculate, DrawTFD and go to FDATA and click on the left Cls.

Click AMEFORCES with right mouse button to get member end forces, D5(,) assumed to the right and D6(,) assumed upward, acting at member ends, at the joint as large as but opposite directed,

Check of equilibrium of joint 12.

member 11 group b

D5(12,11) = -50,50 kN D6(12,11) = -26,59 kN

member 12 group b

D5(12,13) = 50,73 kN D6(12,13) = 9,84 kN

member 19 group c

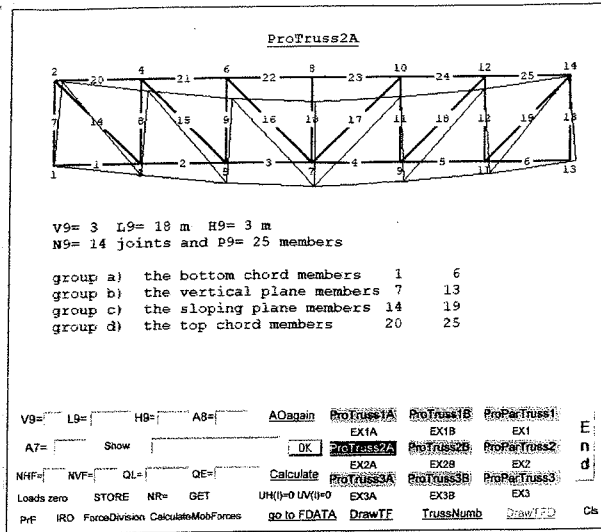
D5(12,4) = 0 kN D5(12,4) = 14,19 kN

member 26 group d

D5(12,5) = -0,22 kN D6(12,5) = 2,55 kN +

-0,01 kN 0,01 kN

Joint 12 is in horizontal and vertical equilibrium... as expected.



ProTruss2A

group a) the bottom chord members

MFS(1) = 0,00 kN	MFS(2) = 6,00 kN	MFS(3) = 8,00 kN	MFS(4) = 8,00 kN
MFS(5) = 6,00 kN	MFS(6) = 0,00 kN		
LTF(4) = 8,00 kN	LCF(1) = 0,00 kN		

group b) the vertical plane members

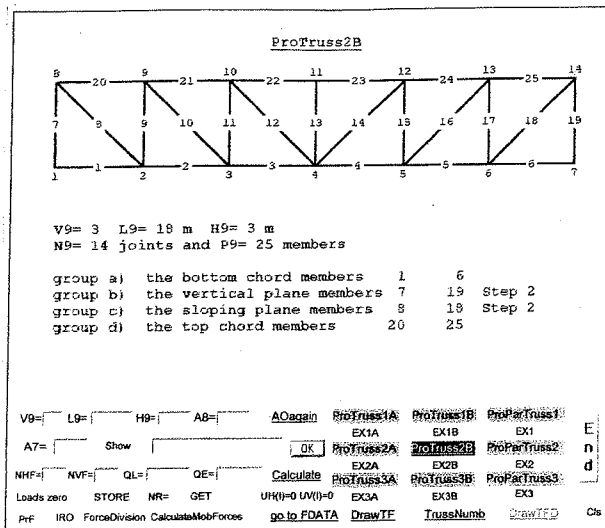
MFS(7) = -6,30 kN	MFS(8) = -6,30 kN	MFS(9) = -2,30 kN	MFS(10) = -4,30 kN
MFS(11) = -2,30 kN	MFS(12) = -6,30 kN	MFS(13) = -6,30 kN	
LTF(9) = 0,00 kN	LCF(3) = -6,30 kN		

group c) the sloping plane members

MFS(14) = 8,49 kN	MFS(15) = 2,83 kN	MFS(16) = 2,83 kN	MFS(17) = 2,83 kN
MFS(18) = 2,83 kN	MFS(19) = 8,49 kN		
LTF(14) = 8,49 kN	LCF(0) = 0,00 kN		

group c) the sloping plane members

MFS(14) = 8,49 kN	MFS(15) = 2,83 kN
MFS(18) = 2,83 kN	MFS(19) = 8,49 kN
LTF(14) = 8,49 kN	LCF(0) = 0,00 kN



ProTruss2B

group a) the bottom chord members

MFS(1) = 0,00 kN	MFS(2) = 6,00 kN	MFS(3) = 8,00 kN	MFS(4) = 8,00 kN
MFS(5) = 6,00 kN	MFS(6) = 0,00 kN		
LTF(4) = 8,00 kN	LCF(1) = 0,00 kN		

group b) the vertical plane members

MFS(7) = -6,00 kN	MFS(8) = -6,00 kN	MFS(9) = -2,00 kN	MFS(10) = -4,00 kN
MFS(11) = -2,00 kN	MFS(12) = -6,00 kN	MFS(13) = -6,00 kN	
LTF(9) = 0,00 kN	LCF(7) = -6,00 kN		

group c) the sloping plane members

MFS(8) = 8,49 kN	MFS(10) = 2,83 kN	MFS(12) = 2,83 kN	MFS(14) = 2,83 kN
MFS(16) = 2,83 kN	MFS(18) = 8,49 kN		
LTF(18) = 8,49 kN	LCF(0) = 0,00 kN		

group c) the sloping plane members

MFS(8) = 8,49 kN	MFS(10) = 2,83 kN
MFS(16) = 2,83 kN	MFS(18) = 8,49 kN
LTF(18) = 8,49 kN	LCF(0) = 0,00 kN

PROTRUSS2A

Basic variables to put in.

V9=3 number of spans; equal joint distances,
real number of spans becomes $2 \times 3 = 6$.

L9=18 m length of the truss, and

H9=3 m height of the truss.

At the start cursor in TV9, type 3, next Tab,
cursor in TL9, type 18 and Tab, cursor in TH9,
type 3. No own weight QE.

Numbering joints 1-3-5-7-9-11-13 and
2-4-6-8-10-12-14 with step ST=2.
Numbering members, bottom chord 1-2-3-4-5-6,
verticals 7-8-9-10-11-12-13, ST=1,
sloping members 14-15-16-17-18-19 and
top chord members 20-21-22-23-24-25. ST=1

Joints 4, 8 and 12 are loaded with vertical
load forces of 4 kN. Then type in TSTRING
FY(4)=-4 Enter, FY(8)=-4 Enter and
FY(12)=-4 Enter.

Or in another way, type 3 in TNFV, and
in TSTRING for I, FY(I)
4,-4 Enter, 8,-4, Enter and 12,-4 Enter.

Click ProTruss2A and
click DrawTF, TrussNumb, Calculate, DrawTFd and
go to FDATAFDA and Cls if necessary.

To determine the largest tension and compres-
sion member per group click MFORCES. Group a),
b) and c) printed on the left, and d).
Group c) gives LTF(14)= 8,49 kN, tension mem-
ber. Can be member 19 as well, symmetry.
No compression member, with LCF(0)= 0 kN.

ProTruss2B Click AOagain first.

Again V9=3, L9=18 and H9=3.

With different joint and member numbering.

Numbering joints 1-2-3-4-5-6 and
8-9-10-11-12-13-14 with step ST=1
Numbering members, bottom chord 1-2-3-4-5-6,
verticals 7-9-11-13-15-17-19
sloping members 8-10-12-14-16-18 and ST=2
top chord members 20-21-22-23-24-25. ST=1

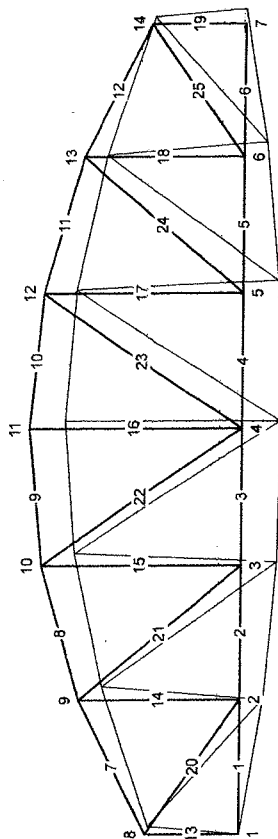
Comparing with ProTruss2A different joint num-
bers for input of joint load forces at same
places. After data input like done above
Joints 9, 11 and 13 are loaded with vertical
load forces of 4 kN. Then type in TSTRING
FY(9)=-4 Enter, FY(11)=-4 Enter and
FY(13)=-4 Enter.

Or in another way, type in TNFV 3,
in TSTRING for I, FY(I)
9,-4 Enter, 11,-4, Enter and 13,-4 Enter.

Click ProTruss2b, etc, and
go to FDATA and click MFORCES.

Group c) gives LTF(18)= 8,49 kN, tension mem-
ber. Can be member 8 as well, symmetry.
No compression member, with LCF(0)= 0 kN.
Group b) with LCF(7)= -6,00 kN, compression in-
dicated with a minus sign.

ProparTruss2



V9= 3 L9= 25,84 m H9= 6,85 m A8= 2,95 m
N9= 14 joints and p9= 25 members QL= 5 kN/m

group a)	the bottom chord members	1	To 6
group b)	the parabola chord members	7	To 12
group c)	the vertical plane members	13	To 19
group d)	the sloping plane members	20	To 25

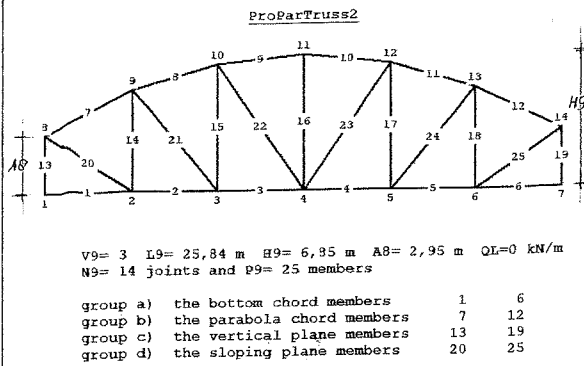
ProparTruss2

group a) the bottom chord members				group b) the parabola chord members				group c) the vertical plane members				group d) the sloping plane members					
MFS(1)	=	0,00 kN	MFS(2)	=	45,31 kN	MFS(7)	=	-50,72 kN	MFS(8)	=	-60,39 kN	MFS(13)	=	-53,83 kN	MFS(14)	=	-9,50 kN
MFS(5)	=	45,31 kN	MFS(6)	=	0,00 kN	MFS(11)	=	-60,39 kN	MFS(12)	=	-50,72 kN	MFS(17)	=	6,68 kN	MFS(18)	=	-9,50 kN
LTF(3)	=	57,81 kN	LCF(1)	=	0,00 kN	LTF(0)	=	0,00 kN	LCF(9)	=	-61,23 kN	LTF(16)	=	12,26 kN	LCF(13)	=	-53,83 kN
MFS(3)	=	57,81 kN	MFS(4)	=	57,81 kN	MFS(9)	=	-61,23 kN	MFS(10)	=	-61,23 kN	MFS(15)	=	6,68 kN	MFS(16)	=	12,26 kN
MFS(22)	=	5,58 kN	MFS(23)	=	5,58 kN												

QL=5 kN/m - FDATA - MFORCESPR - PRPROK 70%

group d) the sloping plane members	
MFS(20) =	54,92 kN
NAA(2,8) =	-54,92 kN
DA(2,8) =	0,00
DA(2,8) =	0,00
MFS(22) =	5,58 kN
NAA(4,10) =	-5,58
DA(4,10) =	0,00
NAA(4,10) =	5,58
DA(4,10) =	0,00
MFS(24) =	19,41 kN
NAA(5,13) =	-19,41
DA(5,13) =	0,00
NAA(5,13) =	19,41
DA(5,13) =	0,00
LCF(20) =	54,92 kN
LCF(0) =	0,00 kN
MFS(21) =	19,41 kN
NAA(3,9) =	-19,41
DA(3,9) =	0,00
NAA(3,9) =	19,41
DA(3,9) =	0,00
MFS(23) =	5,58 kN
NAA(4,12) =	-5,58
DA(4,12) =	0,00
NAA(4,12) =	5,58
DA(4,12) =	0,00
MFS(25) =	54,92 kN
NAA(6,14) =	-54,92
DA(6,14) =	0,00
NAA(6,14) =	54,92
DA(6,14) =	0,00

QL=5 kN/m - FDATA - AMEFORCESPR - PrPROK 70%

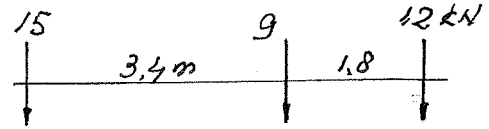


Like on the preceding page,
V9=3, L9=25.84 m, H9=6.85 m and A8= 2.95 m.
Click AOagain for new start.
At the start cursor in TV9, type 3, Tab, cursor
in TL9, type 25.84, Tab, cursor in TH9, type
6.85, Tab, cursor in TA8, type 2.95.
In TQL type QL=0.

Click ProParTruss2, DrawTF. All controls disappear except at the bottom, with
go to FDATA, Calculate appeared,
TrussNumb and DRAWTFD. Click TrussNumb.

No loads so nothing happens when clicking
Calculate and DrawTFD. Click on the form to get
back the controls.

A mobile force system.



MF=3 forces.

Type in TSTRING MF=3 Enter, next
1,12,0 Enter, 2,9,1.8 Enter, 3,15,3.4 Enter.

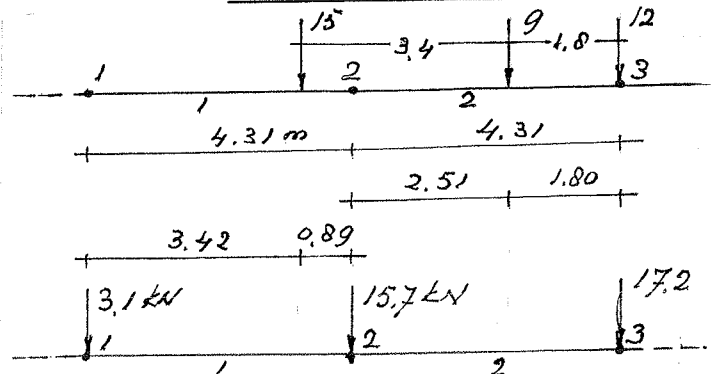
Each force is placed on a joint of the bottom
chord, the other two forces will be divided to
be placed (and added) on the corresponding
joints.

With a click on ForceDivision controls disappear
and all possibilities appear on the form
like shown on the left.

Click somewhere on the form to get the controls
back. Going on on next page.

ProParTruss2, mobile forces case I3=3 K=1.

Click AOagain for new start. In TQL type QL=0.
Input like done above, no mobile forces.
Underlined case, I3=3 K=1 12 kN on joint 3.



To type in TSTRING FY(1)=-3.1 Enter,
FY(2)=-15.7 Enter, FY(3)=-17.2 Enter. Etc.

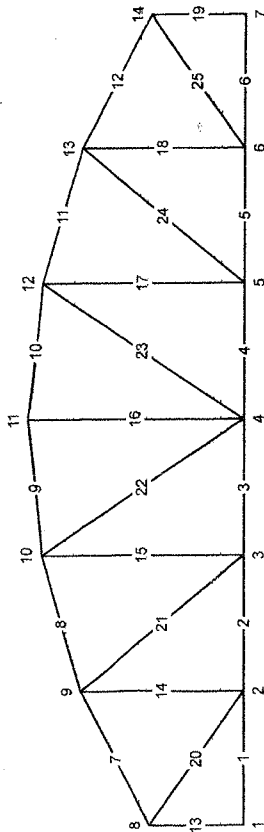
HFS(19) = -8.35 kN
NAA(7,14) = 8.35
DAA(7,14) = 0.00
LTF(15) = 15.12 kN

NAA(14,7) = -8.35
DAA(14,7) = 0.00
LCF(13) = -24.55 kN

group d) the sloping plane members
HFS(20) = 25.05 kN
NAA(2,8) = -25.05
DAA(2,8) = 0.00
HFS(22) = -11.96 kN
NAA(4,10) = 11.96
DAA(4,10) = 0.00
HFS(24) = 6.49 kN
NAA(5,13) = -6.49
DAA(5,13) = 0.00
LTF(20) = 25.05 kN
LCF(22) = -11.96 kN

HFS(21) = 2.72 kN
NAA(3,9) = -2.72
DAA(3,9) = 0.00
HFS(23) = 3.15 kN
NAA(4,12) = -3.15
DAA(4,12) = 0.00
HFS(25) = 3.52 kN
NAA(6,14) = -3.52
DAA(6,14) = 0.00

ProParTruss2



V9= 3 L9= 25,84 m H9= 6,85 m A8= 2,95 m
N9= 14 joints and P9= 25 members

- group a) the bottom chord members 1 To 6
- group b) the parabola chord members 7 To 12
- group c) the vertical plane members 13 To 19
- group d) the sloping plane members 20 To 25

MF= 3 mobile forces

MFF(1) = 12,00 kN MA(1) = 0,00 m
MFF(2) = 9,00 kN MA(2) = 1,80 m
MFF(3) = 15,00 kN MA(3) = 3,40 m

I3= 1 KI= 3

group a) the bottom chord members
LTFI(2) = 13,05 kN LCFI(1) = 0,00 kN
group b) the parabola chord members
LTFI(0) = 0,00 kN LCFI(7) = -14,61 kN
group c) the vertical plane members
LTFI(14) = 7,68 kN LCFI(13) = -15,51 kN
group d) the sloping plane members
LTFI(20) = 15,82 kN LCFI(21) = -5,26 kN

I3= 2 KI= 1

LTFI(2) = 12,09 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(7) = -13,54 kN
LTFI(14) = 8,96 kN LCFI(13) = -14,37 kN
LTFI(20) = 14,66 kN LCFI(21) = -6,80 kN

I3= 2 KI= 3

LTFI(3) = 24,10 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -25,17 kN
LTFI(15) = 14,38 kN LCFI(13) = -26,40 kN
LTFI(20) = 26,93 kN LCFI(22) = -10,76 kN

I3= 3 KI= 1

LTFI(3) = 22,43 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -23,43 kN
LTFI(15) = 15,12 kN LCFI(13) = -24,53 kN
LTFI(20) = 25,03 kN LCFI(22) = -11,97 kN

I3= 3 KI= 3

LTFI(3) = 27,38 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -28,61 kN
LTFI(16) = 5,61 kN LCFI(13) = -20,40 kN
LTFI(20) = 20,81 kN LCFI(0) = 0,00 kN

I3= 2 KI= 2

LTFI(2) = 16,24 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(7) = -18,18 kN
LTFI(15) = 8,80 kN LCFI(13) = -19,30 kN
LTFI(20) = 19,69 kN LCFI(22) = -6,97 kN

I3= 3 KI= 2

LTFI(3) = 25,80 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -26,94 kN
LTFI(15) = 13,63 kN LCFI(13) = -25,14 kN
LTFI(20) = 25,65 kN LCFI(22) = -9,52 kN

case I3=3 K=1 see prec. page

I3= 4 KI= 1
LTFI(3) = 26,97 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -28,17 kN
LTFI(16) = 5,45 kN LCFI(13) = -21,65 kN
LTFI(20) = 22,08 kN LCFI(0) = 0,00 kN

I3= 4 KI= 2
LTFI(3) = 25,69 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(8) = -28,80 kN
LTFI(16) = 5,77 kN LCFI(13) = -19,14 kN
LTFI(20) = 19,52 kN LCFI(0) = 0,00 kN

I3= 4 KI= 3

LTFI(4) = 27,32 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(11) = -28,54 kN
LTFI(17) = 5,75 kN LCFI(19) = -21,80 kN
LTFI(25) = 22,04 kN LCFI(23) = -0,29 kN

I3= 5 KI= 1

LTFI(4) = 27,32 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(11) = -28,54 kN
LTFI(16) = 5,54 kN LCFI(19) = -20,35 kN
LTFI(25) = 20,77 kN LCFI(0) = 0,00 kN

I3= 5 KI= 3

LTFI(4) = 22,55 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(12) = -23,66 kN
LTFI(17) = 15,21 kN LCFI(19) = -25,11 kN
LTFI(25) = 25,82 kN LCFI(23) = -12,04 kN

I3= 6 KI= 1

LTFI(4) = 23,81 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(11) = -24,87 kN
LTFI(17) = 13,72 kN LCFI(19) = -26,35 kN
LTFI(25) = 26,89 kN LCFI(23) = -10,07 kN

I3= 6 KI= 3

LTFI(5) = 11,85 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(12) = -13,27 kN
LTFI(18) = 8,78 kN LCFI(19) = -14,08 kN
LTFI(25) = 14,36 kN LCFI(24) = -6,66 kN

I3= 7 KI= 1

LTFI(5) = 12,72 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(12) = -14,24 kN
LTFI(18) = 6,94 kN LCFI(19) = -15,12 kN
LTFI(25) = 15,42 kN LCFI(23) = -5,22 kN

group a) the bottom chord members
LTFI(3) = 27,38 kN LCFI(1) = 0,00 kN

group c) the vertical plane members
LTFI(17) = 15,21 kN LCFI(13) = -26,40 kN

group b) the parabola chord members
LTFI(12) = 0,00 kN LCFI(10) = -28,80 kN

group d) the sloping plane members
LTFI(20) = 26,93 kN LCFI(23) = -12,04 kN

Going on with first example of the preceding page. After a click on ForceDivision follows a click on CalculateMobForces.

With 7 joints 1 to 7 and 3 mobile forces 7*3=21 main calculations are carried out. Each time one of the three forces is put on a joint.

Next click go to FDATA and click MOBMOFORCESPR of the 'check control', click finally PrProK to get all the results of the 21 calculations printed.

To compare the values of the preceding page with the case I3=3 KI=1.

LTFI(3)= 22,43 kN and MFS(3)= 22,42 kN
LTFI(20)= 25,03 kN and MFS(20)= 25,05 kN
LCFI(13)=-24,53 kN and MFS(13)=-24,55 kN etc.

Here below for each group of members the largest member tension forces LTFI() and member compression forces LCFI() of all calculations.

I3= 6 KI= 2
LTFI(5) = 20,07 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(12) = -22,47 kN
LTFI(17) = 12,82 kN LCFI(19) = -23,85 kN
LTFI(25) = 24,33 kN LCFI(23) = -10,23 kN

I3= 5 KI= 2
LTFI(4) = 27,32 kN LCFI(1) = 0,00 kN
LTFI(0) = 0,00 kN LCFI(11) = -28,54 kN
LTFI(17) = 9,54 kN LCFI(19) = -22,86 kN
LTFI(25) = 23,32 kN LCFI(23) = -4,56 kN

ProTruss3A

V9= 4 L9= 17,86 m H9= 3,15 m QL=5 kN/m
N9= 16 joints and P9= 29 members

group a) the bottom chord members 1 To 9
group b) the sloping plane members 9 To 16
group c) the vertical plane members 17 To 23
group d) the top chord members 24 To 29

V9= L9= H9= A8= AOagain EX1A EX1B EX1
A7= Show OK EX1A EX1B EX1
H9= N9= QL= QE= Calculate EX2A EX2B EX2
Loads zero STORE NR= GET UH(0)=0 UV(0)=0 EX3A EX3B EX3
P9= IRO ForceDivision CalculateMobForces go to FDATA DrawTF TrussNum DrawTFD Cts

ProTruss3A

group a) the bottom chord members

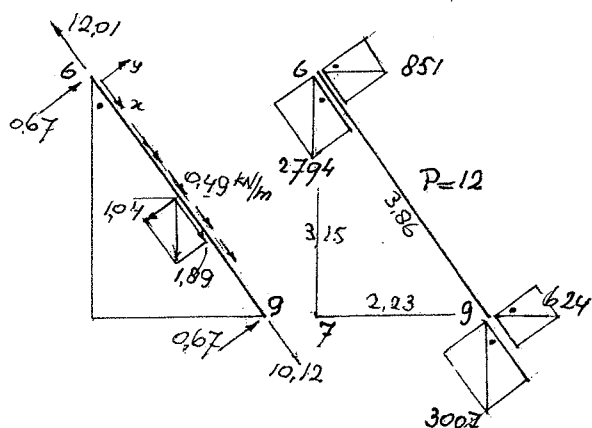
HFS(1) = 44,29 kN	NAA(3,1) = 44,29	HFS(2) = 44,29 kN	NAA(5,3) = 44,29
NAA(1,3) = -44,29	DAA(3,1) = 0,67	NAA(3,5) = -44,29	DAA(5,3) = 0,67
DAA(1,3) = 0,67	HFS(3) = 95,46 kN	NAA(7,5) = 95,46	DAA(7,5) = 0,67
HFS(3) = 95,46 kN	NAA(5,7) = 95,46	HFS(4) = 95,46 kN	NAA(9,7) = 95,46
NAA(5,7) = 95,46	DAA(7,5) = 0,67	NAA(7,9) = -95,46	DAA(9,7) = 0,67
DAA(5,7) = 0,67	HFS(5) = 95,46 kN	NAA(11,9) = 95,46	DAA(13,11) = 95,46
HFS(5) = 95,46 kN	NAA(11,13) = 95,46	HFS(6) = 95,46 kN	NAA(13,15) = 95,46
NAA(11,13) = 95,46	DAA(13,11) = 0,67	NAA(15,16) = -44,29	DAA(16,15) = 0,67
DAA(9,11) = 0,67	HFS(7) = 44,29 kN	NAA(15,16) = -44,29	DAA(16,15) = 0,67
HFS(7) = 44,29 kN	NAA(15,16) = -44,29	NAA(15,16) = -44,29	DAA(16,15) = 0,67
NAA(15,16) = -44,29	DAA(15,13) = 0,67	DAA(15,16) = 0,67	DAA(16,15) = 0,67
DAA(13,15) = 0,67	LTF(5) = 95,46 kN	LTF(0) = 0,00 kN	

group b) the sloping plane members

HFS(9) = -77,55 kN	NAA(2,1) = -77,55	HFS(10) = 56,25 kN	NAA(5,2) = 54,36
NAA(1,2) = 77,55	DAA(2,1) = 0,67	NAA(2,5) = -56,25	DAA(5,2) = 0,67
DAA(1,2) = 0,67	HFS(11) = -34,13 kN	NAA(6,9) = -12,01	NAA(9,6) = 10,12
HFS(11) = -34,13 kN	NAA(6,5) = -32,24	NAA(6,9) = -12,01	NAA(9,6) = 10,12
NAA(6,5) = -32,24	DAA(5,6) = 0,67	NAA(10,13) = 32,24	DAA(13,10) = -34,13
DAA(6,5) = 0,67	HFS(13) = 12,01 kN	NAA(10,13) = 32,24	DAA(13,10) = -34,13
HFS(13) = 12,01 kN	NAA(10,9) = 12,01	NAA(12,14) = -77,55	NAA(14,12) = -77,55
NAA(10,9) = 12,01	DAA(10,9) = 0,67	NAA(14,16) = 76,66	DAA(16,14) = 0,67
DAA(9,10) = 0,67	HFS(15) = 56,25 kN	NAA(14,16) = 76,66	DAA(16,14) = 0,67
HFS(15) = 56,25 kN	NAA(16,13) = 56,25	NAA(16,15) = -44,29	DAA(16,15) = 0,67
NAA(16,13) = 56,25	DAA(14,16) = 0,67	DAA(14,16) = 0,67	DAA(16,15) = 0,67
DAA(13,14) = 0,67	LTF(15) = 56,25 kN	LTF(16) = -77,55 kN	

group c) the vertical plane members

HFS(9) = -77,55 kN	NAA(2,1) = -77,55	HFS(10) = 56,25 kN	NAA(5,2) = 54,36
NAA(1,2) = 77,55	DAA(2,1) = 0,67	NAA(2,5) = -56,25	DAA(5,2) = 0,67
DAA(1,2) = 0,67	HFS(11) = -34,13 kN	NAA(6,9) = -12,01	NAA(9,6) = 10,12
HFS(11) = -34,13 kN	NAA(6,5) = -32,24	NAA(6,9) = -12,01	NAA(9,6) = 10,12
NAA(6,5) = -32,24	DAA(5,6) = 0,67	NAA(10,13) = 32,24	DAA(13,10) = -34,13
DAA(6,5) = 0,67	HFS(13) = 12,01 kN	NAA(10,13) = 32,24	DAA(13,10) = -34,13
HFS(13) = 12,01 kN	NAA(10,9) = 12,01	NAA(12,14) = -77,55	NAA(14,12) = -77,55
NAA(10,9) = 12,01	DAA(10,9) = 0,67	NAA(14,16) = 76,66	DAA(16,14) = 0,67
DAA(9,10) = 0,67	HFS(15) = 56,25 kN	NAA(14,16) = 76,66	DAA(16,14) = 0,67
HFS(15) = 56,25 kN	NAA(16,13) = 56,25	NAA(16,15) = -44,29	DAA(16,15) = 0,67
NAA(16,13) = 56,25	DAA(14,16) = 0,67	DAA(14,16) = 0,67	DAA(16,15) = 0,67
DAA(13,14) = 0,67	LTF(15) = 56,25 kN	LTF(16) = -77,55 kN	



UH(1) = 0,00 kN	RV(1) = 69,91 kN	RV(16) = 69,91 kN
UH(2) = 0,00 kN	UV(1) = 0,00 kN	UH(2) = 1191,9 kN
UH(3) = 98,9 kN	UV(2) = -1249,6 kN	UH(4) = 1023,7 kN
UH(4) = 197,8 kN	UV(3) = -2173,6 kN	UH(5) = 851,4 kN
UH(5) = 410,9 kN	UV(4) = -2836,2 kN	UH(6) = 624,0 kN
UH(6) = 624,0 kN	UV(5) = -3007,3 kN	UH(7) = 396,6 kN
UH(7) = 837,1 kN	UV(6) = -2936,2 kN	UH(8) = 226,3 kN
UH(8) = 1050,2 kN	UV(7) = -2173,6 kN	UH(9) = 56,1 kN
UH(9) = 1149,1 kN	UV(8) = -1249,6 kN	UH(10) = 1249,6 kN
UH(10) = 0,00 kN	UV(9) = 0,00 kN	UH(11) = -1207,3 kN
UH(11) = 98,9 kN	UV(10) = -2173,6 kN	UH(12) = -2180,8 kN
UH(12) = 197,8 kN	UV(11) = -2836,2 kN	UH(13) = -2793,8 kN
UH(13) = 410,9 kN	UV(12) = -3007,3 kN	UH(14) = -3014,5 kN
UH(14) = 624,0 kN	UV(13) = -2936,2 kN	UH(15) = -1207,3 kN
UH(15) = 837,1 kN	UV(14) = -2173,6 kN	UH(16) = 0,00 kN

ProTruss3A EX3A

V9=4, L9=17,86 m, H9=3,15 m and QL= 5 kN/m.
Click AOagain to start.
Type 4 in TV9, Tab, 17.86 in TL9, Tab,
3.15 in TH9 and 5 in TQL.

Click now ProTruss3A before typing .6 in TQE
for own weight of 0,6 kN/m of all members.

Click DrawTF, TrussNum, Calculate, DrawTFD for
the form print.

Next go to FDATA, PDATA to see the lengths of
the members, AMEFORCES and UHUV for the displace-
ments.

Consideration of member 12.

In the figure the lengths of the members
P=12 3,86 m, P=19 3,15 m, P=4 2,23 m.

UH(6)= 851/EA and UV(6)= -2794/EA,
UH(9)= 624/EA, and UV(9)= -3007/EA

The joint displacements are drawn with their
real directions.

The components along the member axis, x /EA,
member end 6

$(851/3,86)*2,23= 492$ $(2794/3,86)*3,15= 2280$

member end 9

$(624/3,86)*2,23= 360$ $(3007/3,86)*3,15= 2454$

Member end 6 displaces in direction 6-9

$492 + 2280 = 2772$ /EA and

member end 9 displaces in direction 6-9

$360 + 2454 = 2814$ /EA,

member 12 lengthens $2814 - 2772 = 42$ /EA.

Suppose member end 9 is a clamp. Member 12 is
loaded with member end force of 12,01 kN, and
own weight load of 0,6 kN/m with the component
along the member $(0,6/3,86)*3,15= 0,50$ kN/m.

Member end force 12,01 kN lengthens member 12,

$(12,01*3,86)/EA= 46/EA$

The distributed load of 0,50 kN/m shortens mem-

ber 12, and with formula $Q*L^2/2EA$ follows

$(0,5*3,86^2)/2EA= 4/EA,$

member 12 lengthens $46 - 4 = 42/EA$ like above.

Or, suppose member end 6 is a clamp.

Member end force 10,12 kN lengthens member 12,

$(10,12*3,86)/EA= 39/EA$

The distributed load of 0,50 kN/m lengthens

member 12, $(0,5*3,86^2)/2EA= 4/EA,$

member 12 lengthens $39 + 4 = 43/EA$ 'is' 42/EA.

Reactions RV(1) and RV(16) both 69,91 kN.

Own weight 0,6 kN/m.

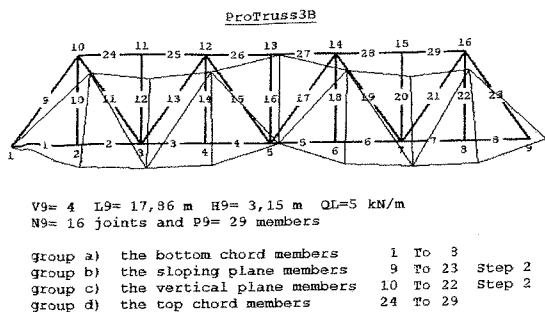
14 horizontal members, $14*2,23*0,6= 18,73$ kN

7 vertical members, $7*3,15*0,6= 13,23$ kN

8 sloping members, $8*3,86*0,6= 18,53$ kN

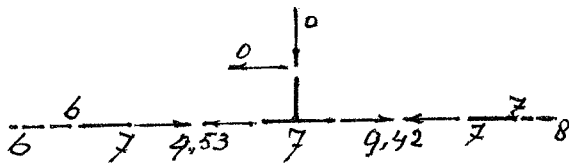
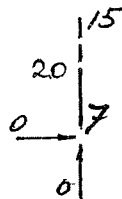
QL=5 kN/m $8*2,23*5= 89,20$ kN
139,69 kN

That's $139,69/2= 69,85$ kN 'is' 69,91 kN.



c)

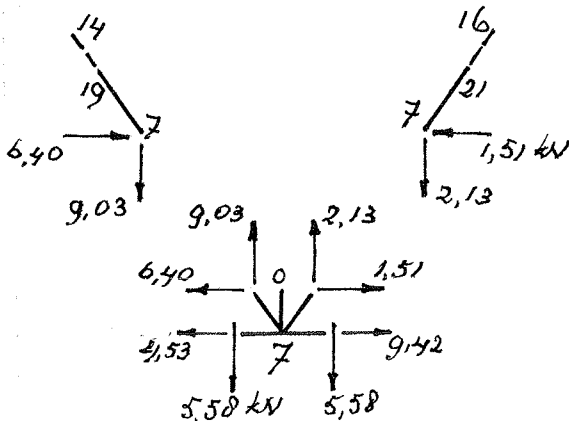
$$\begin{aligned} \text{MFS}(20) &= 0,00 \text{ kN} \\ \text{D5}(7,15) &= 0,00 & \text{D5}(15,7) &= 0,00 \\ \text{D6}(7,15) &= 0,00 & \text{D6}(15,7) &= 0,00 \end{aligned}$$



a)

$$\begin{aligned} \text{MFS}(7) &= 9,42 \text{ kN} \\ \text{D5}(7,8) &= -9,42 & \text{D5}(8,7) &= 9,42 \\ \text{D6}(7,8) &= 0,00 & \text{D6}(8,7) &= 0,00 \end{aligned}$$

$$\begin{aligned} \text{MFS}(6) &= 4,53 \text{ kN} \\ \text{D5}(6,7) &= -4,53 & \text{D5}(7,6) &= 4,53 \\ \text{D6}(6,7) &= 0,00 & \text{D6}(7,6) &= 0,00 \end{aligned}$$



b)

$$\begin{aligned} \text{MFS}(19) &= 11,07 \text{ kN} \\ \text{D5}(7,14) &= 6,40 & \text{D5}(14,7) &= -6,40 \\ \text{D6}(7,14) &= -9,03 & \text{D6}(14,7) &= 9,03 \end{aligned}$$

$$\begin{aligned} \text{MFS}(21) &= 2,61 \text{ kN} \\ \text{D5}(7,16) &= -1,51 & \text{D5}(16,7) &= 1,51 \\ \text{D6}(7,16) &= -2,13 & \text{D6}(16,7) &= 2,13 \end{aligned}$$

Like ProTruss3A but with different joint and member numbering, except the horizontal member numbering.
V9=4, L9=17,86 m, H9=3,15 m and QL= 5 kN/m.
No own weight.
Click ProTruss3B after putting in the given start data.

A change. Joint 5 is now supported by a roller support. Therefore type in TSTRING
PV(5)=1 Enter and UV(5)=0 Enter.

Click DrawTF, TrussNumb, Calculate, DrawTFD for the form print.

Next go to FDATA and click AMEFORCES with right mouse button to get member end forces D5(L,H), D6(L,H), D5(H,L) and D6(H,L).
Some results of member 7 are shown on the left.

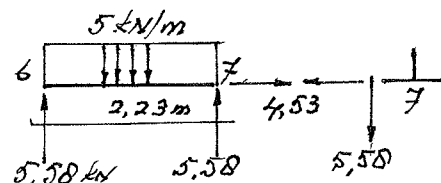
Consideration of joint 7 separated from the truss. Checking equilibrium.

Member end forces D5(,) assumed to be directed to the right, and member end forces D6(,) assumed to be directed upward. (Later with frames assumed downward.)
At the joint act member end forces as large as but opposite directed.

First picture on the left.

Member 20 is a zero member, D5(7,15)=0 and D6(7,15)=0. Member 12 and 16 are zero members as well.

member 6 D5(7,6)= 4,53 kN, to the right
D6(7,6)= 0



Due to 5 kN/m (2,23*5)/2= 5,58 kN upward.
At joint 7 as large as but opposite directed.

member 7 D5(7,8)= -9,42 kN, not to the right but to the left.
D6(7,8)= 0

Due to 5 kN/m (2,23*5)/2= 5,58 kN upward.

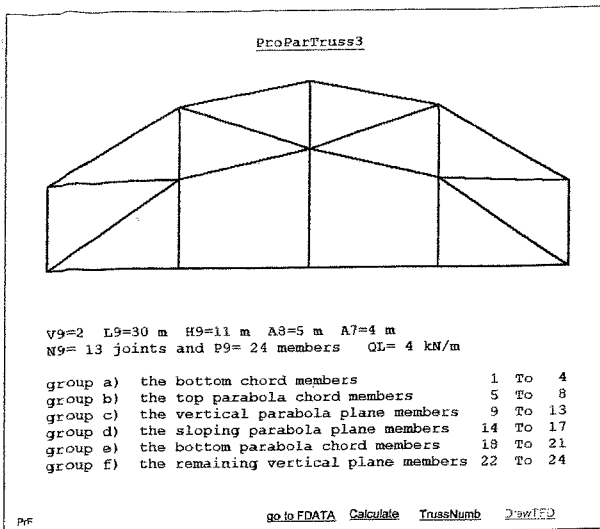
Second picture.

member 19 D5(7,14)= 6,40 kN, to the right.
D6(7,14)= -9,03 kN, downward.

member 21 D5(7,16)= -1,51 kN, to the left
D6(7,16)= -2,13 kN, downward.

$\Sigma \text{ hor.} = 0?$
6,40+4,53 -1,51-9,42= 10,93-10,93= 0 ok

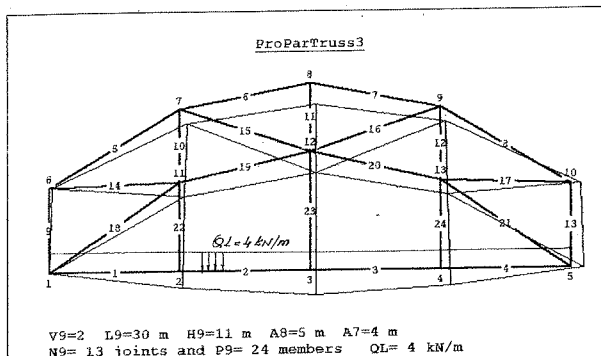
$\Sigma \text{ vert.} = 0?$
9,03+2,13 -5,58-5,58= 11,16-11,16= 0 ok



Joint displacements UH(I) and UV(I).

UH(1) =	0 /EA	UV(1) =	0 /EA
UH(3) =	615 /EA	UV(3) =	-2568 /EA
UH(5) =	1230 /EA	UV(5) =	0 /EA
UH(7) =	786 /EA	UV(7) =	-1528 /EA
UH(9) =	444 /EA	UV(9) =	-1528 /EA

MFS(3) =	40,99 kN		
NAA(3,4) =	-40,99	NAA(4,3) =	40,99
DAA(3,4) =	0,00	DAA(4,3) =	0,00
LTF(3) =	40,99 kN	LCF(0) =	0,00



Joint displacements UH(I) and UV(I).

UH(1) =	0 /EA	UV(1) =	0 /EA
UH(3) =	596 /EA	UV(3) =	-1856 /EA
UH(5) =	1191 /EA	UV(5) =	0 /EA
UH(7) =	669 /EA	UV(7) =	-1091 /EA
UH(9) =	522 /EA	UV(9) =	-1091 /EA

ProParTruss3

group a) the bottom chord members

MFS(1) =	39,70 kN		
NAA(1,2) =	-39,70	NAA(2,1) =	39,70
DAA(1,2) =	0,00	DAA(2,1) =	0,00
MFS(3) =	39,70 kN		
NAA(3,4) =	-39,70	NAA(4,3) =	39,70
DAA(3,4) =	0,00	DAA(4,3) =	0,00
LTF(3) =	39,70 kN	LCF(0) =	0,00 kN

ProParTruss3

V9=2 L9=30 m H9=11 m A8=5 m A7=4 m
QL= 4 kN/m.
No own weight. All member ends are hinges.
Click AOagain for new start.

Type 2 in TV9, Tab, 30 in TL9, Tab, 11 in TH9,
Tab, 5 in TA8, 4 in TA7 and 4 in TQL.

Click ProParTruss3.

First case.

Click DrawTF, controls disappear, at the bottom
of the form to be seen

go to FDATA Calculate TrussNumb DrawTFD.

Click TrussNumb, Calculate, and DrawTFD for the
final form print with deformed truss.

Next go to FDATA and click PDATA, UHUV and
MFORCES, see some results on the left.

Second case.

Like above same data to put in. All members
have strain stiffness 1'EA'.

Next the strain stiffness EA of the members of
group b) and group e) are changed to 2'EA'.

Therefore to type in TSTRING PEAA,P1,P2,ST,EA,
for group b) PEAA,5,8,1,2 Enter,
for group e) PEAA,18,21,1,2 Enter. Etc.

The truss is internal statically indeterminate,
the results of both cases will be different.

Case 1	UH(3)= 615/EA	UV(3)= -2568/EA
Case 2	UH(3)= 596/EA	UV(3)= -1856/EA

Case 1	NAA(3,4)=-40,99 kN	NAA(6,7)= 33,55 kN
Case 2	NAA(3,4)=-39,70 kN	NAA(6,7)= 35,42 kN

A small truss with ProParTruss3.

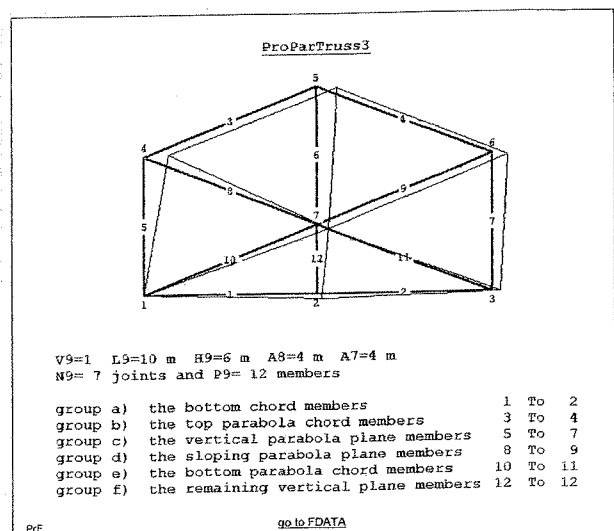
V9=1 L9=10 m H9=6 m A8=4 m A7=4 m FX(4)=10

A value A7 >=0 must be put in TA7.

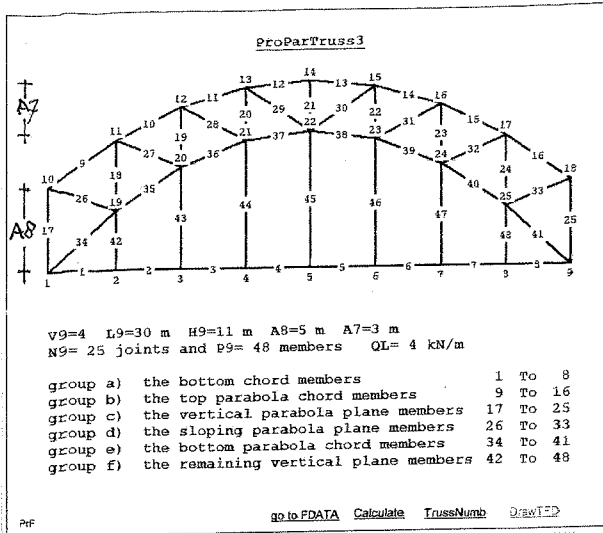
In TSTRING FX(4)=10 Enter.

After input of data click ProParTruss3, etc.

The truss is internal statically indeterminate.

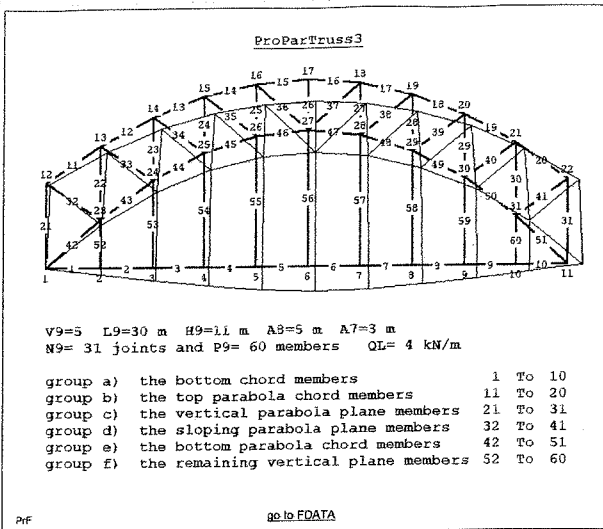


ProParTruss3 EX3



<u>ProParTruss3</u>													
<u>group a) the bottom chord members</u>													
MFS(1) =	60,78 kN	MFS(3) =	60,78 kN	MFS(5) =	60,78 kN	MFS(7) =	60,78 kN	MFS(9) =	60,78 kN	MFS(11) =	60,78 kN	MFS(13) =	60,78 kN
MFS(15) =	60,78 kN	MFS(17) =	60,78 kN	MFS(19) =	60,78 kN	MFS(21) =	60,78 kN	MFS(23) =	60,78 kN	MFS(25) =	60,78 kN	MFS(27) =	60,78 kN
LTF(4) =	0,00 kN	LCF(12) =	0,00 kN										
<u>group b) the top parabola chord members</u>													
MFS(14) =	-47,70 kN	MFS(16) =	-62,52 kN	MFS(18) =	-66,88 kN	MFS(20) =	-66,88 kN	MFS(22) =	-47,70 kN	MFS(24) =	-25,79 kN	MFS(26) =	-25,79 kN
MFS(28) =	-25,79 kN	MFS(30) =	-25,79 kN	MFS(32) =	-25,79 kN	MFS(34) =	-25,79 kN	MFS(36) =	-25,79 kN	MFS(38) =	-25,79 kN	MFS(40) =	-25,79 kN
LTF(9) =	0,00 kN	LCF(12) =	-66,88 kN										
<u>group c) the vertical parabola plane members</u>													
MFS(17) =	-25,69 kN	MFS(19) =	-19,17 kN	MFS(21) =	-8,35 kN	MFS(23) =	-8,35 kN	MFS(25) =	4,69 kN	MFS(27) =	4,69 kN	MFS(29) =	19,17 kN
MFS(31) =	25,69 kN	MFS(33) =	19,17 kN	MFS(35) =	8,35 kN	MFS(37) =	8,35 kN	MFS(39) =	25,69 kN	MFS(41) =	25,69 kN	MFS(43) =	25,69 kN
LTF(21) =	12,17 kN	LCF(26) =	-25,69 kN										
<u>group d) the sloping parabola plane members</u>													
MFS(26) =	22,63 kN	MFS(27) =	23,79 kN	MFS(29) =	19,52 kN	MFS(31) =	19,52 kN	MFS(33) =	22,63 kN	MFS(35) =	22,63 kN	MFS(37) =	23,79 kN
MFS(39) =	3,66 kN	MFS(41) =	3,66 kN	MFS(43) =	3,66 kN	MFS(45) =	3,66 kN	MFS(47) =	3,66 kN	MFS(49) =	3,66 kN	MFS(51) =	3,66 kN
LTF(27) =	23,79 kN	LCF(39) =	0,00 kN										
<u>group e) the bottom parabola chord members</u>													
MFS(34) =	-93,66 kN	MFS(35) =	-48,42 kN	MFS(36) =	-20,01 kN	MFS(37) =	-1,14 kN	MFS(38) =	-1,14 kN	MFS(39) =	-48,42 kN	MFS(40) =	-93,66 kN
MFS(41) =	-93,66 kN	MFS(42) =	-48,42 kN	MFS(43) =	-20,01 kN	MFS(44) =	-1,14 kN	MFS(45) =	-1,14 kN	MFS(46) =	-48,42 kN	MFS(47) =	-93,66 kN
LTF(9) =	0,00 kN	LCF(34) =	-93,66 kN										
<u>group f) the remaining vertical plane members</u>													
MFS(42) =	17,18 kN	MFS(43) =	17,18 kN	MFS(44) =	18,38 kN	MFS(45) =	18,38 kN	MFS(46) =	17,18 kN	MFS(47) =	17,18 kN	MFS(48) =	17,18 kN
MFS(49) =	18,38 kN	MFS(50) =	18,38 kN	MFS(51) =	18,38 kN	MFS(52) =	18,38 kN	MFS(53) =	18,38 kN	MFS(54) =	18,38 kN	MFS(55) =	18,38 kN
LTF(45) =	18,53 kN	LCF(51) =	0,00 kN										

group b) the top parabola chord members	MFS(9) = -25,79 kN	MFS(10) = -47,70 kN	MFS(11) = -62,52 kN	MFS(12) = -66,88 kN	MFS(13) = -66,88 kN	MFS(14) = -47,70 kN	MFS(15) = -25,79 kN	MFS(16) = -25,79 kN	LTF(0) = 0,00 kN	LCF(12) = -66,88 kN
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D5(11,22) = 0,00	D5(22,11) = 0,00	D6(11,22) = 27,13	D6(22,11) = -25,63	LTF(26) = 10,27 kN	LCF(21) = -27,13 kN
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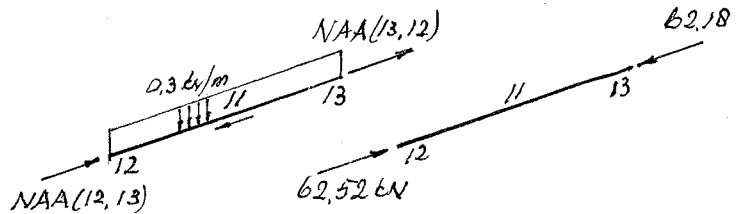
group d) the sloping parabola plane members

MFS(32) = 21,37 kN	MFS(33) = 22,48 kN	D5(12,23) = -17,19	D5(23,12) = 17,19	D6(12,23) = 12,70	D6(23,12) = -11,60
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V9=4 L9=30 m H9=11 m A8=5 m A7=3 m
QL= 4 kN/m Input own weight QE= 0,3 kN/m in
TQE after a click on ProParTruss3!!
Click AOagain for new start.
After data typed in the text boxes, DrawTF,
controls disappear, at the bottom of appear
go to FDATA Calculate TrussNumb DrawTFD.

Click TrussNumb, Calculate, and DrawTFD.
Next go to FDATA and click MFORCES showing for
the members of each group if it is a tension
member or a compression member, with MFS(P).

For instance group b), member 11, 12-13.
The largest of the two member end forces is
62,52 kN, pushes at member end 12, so member 11
is a compression member, MFS(11)= -62,52 kN.
The minus sign is assumed to indicate a 'com-
pression member'.
The Largest of group b) is MFS(12)= -66,88 kN,
LCF(12)= -66,88 kN. C for compression.
No tension member, LTF(0)= 0 kN.

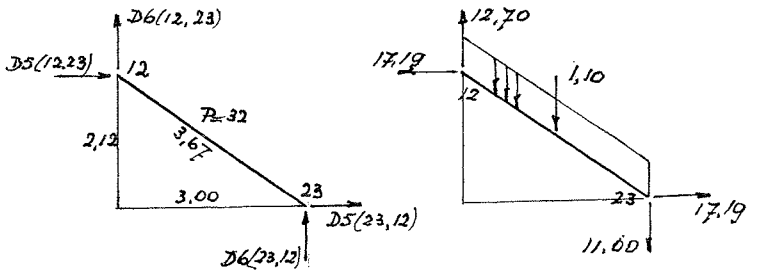


Next page after AMEFORCESPR and PrPrOK.

MFS(11) = -62,52 kN	MFS(12) = -66,88 kN
MFS(15) = -47,70 kN	MFS(16) = -25,79 kN

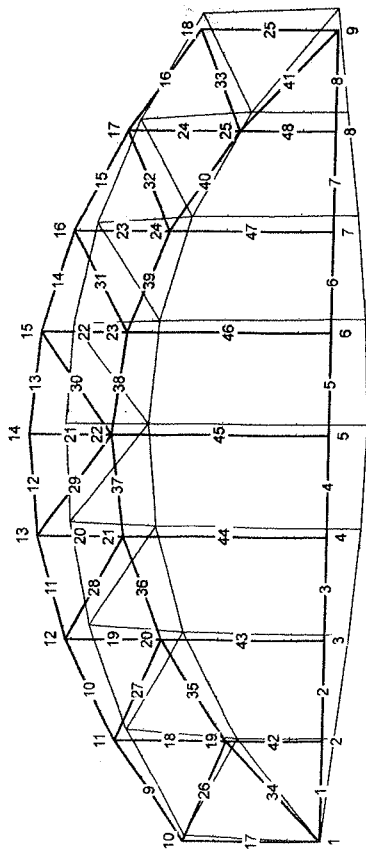
ProParTruss3

V9=5 L9=30 m H9=11 m A8=5 m A7=3 m
QL= 4 kN/m. Own weight QE=0,3 kN/m.
Click AOagain for new start. After input of
data and calculations go to FDATA and click
with right mouse button
AMEFORCES for the member end forces D5(,) as-
sumed to the right, and D6(,) assumed upward.



Member 32 Own weight 3,67*0,3=1,10 kN.
After drawing the member end forces with their
real directions is $\sum \text{hor.} = 0$, $\sum \text{vert.} = 0$ and
 $\sum \text{mom.} = 0$.

ProParTruss3



V9= 4 L9= 30 m H9= 11 m A8= 5 m A7= 3 m QL= 4 kN/m QE= 0,3 kN/m
N9= 25 joints and P9= 48 members

- group a) the bottom chord members
- group b) the top parabola chord members
- group c) the vertical parabola plane members
- group d) the sloping parabola plane members
- group e) the bottom parabola chord members
- group f) the remaining vertical plane members

ProParTruss3

group a) the bottom chord members

MFS(1)	= 60,78 kN
NAA(1,2)	= -60,78
DAA(1,2)	= 0,56
MFS(3)	= 60,78 kN
NAA(3,4)	= -60,78
DAA(3,4)	= 0,56
MFS(5)	= 60,78 kN
NAA(5,6)	= -60,78
DAA(5,6)	= 0,56
MFS(7)	= 60,78 kN
NAA(7,8)	= -60,78
DAA(7,8)	= 0,56
LTF(4)	= 60,78 kN
LCF(0)	= 0,00 kN

group b) the top parabola chord members

MFS(9)	= -25,79 kN
NAA(10,11)	= 25,79
DAA(10,11)	= 0,56
MFS(11)	= -62,52 kN
NAA(12,13)	= 62,52
DAA(12,13)	= 0,56
MFS(13)	= -66,88 kN
NAA(14,15)	= 66,88
DAA(14,15)	= 0,56
MFS(15)	= -47,70 kN
NAA(16,17)	= 47,70
DAA(16,17)	= 0,56
LTF(0)	= 0,00 kN
LCF(12)	= -66,88 kN

MFS(2)	= 60,78 kN
NAA(2,3)	= -60,78
DAA(2,3)	= 0,56
MFS(4)	= 60,78 kN
NAA(4,5)	= -60,78
DAA(4,5)	= 0,56
MFS(6)	= 60,78 kN
NAA(6,7)	= -60,78
DAA(6,7)	= 0,56
MFS(8)	= 60,78 kN
NAA(8,9)	= -60,78
DAA(8,9)	= 0,56

MFS(10)	= -47,70 kN
NAA(11,12)	= 47,70
DAA(11,12)	= 0,56
MFS(12)	= -66,88 kN
NAA(13,14)	= 66,88
DAA(13,14)	= 0,56
MFS(14)	= -62,52 kN
NAA(15,16)	= 62,52
DAA(15,16)	= 0,56
MFS(16)	= -25,79 kN
NAA(17,18)	= 25,79
DAA(17,18)	= 0,56

group c) the vertical parabola plane members

MFS(17)	= -25,68 kN
NAA(10,1)	= -24,18
DAA(10,1)	= 0,56
MFS(19)	= -8,85 kN
NAA(12,20)	= 7,80
DAA(12,20)	= 0,00
MFS(21)	= 12,17 kN
NAA(14,22)	= -12,17
DAA(14,22)	= 0,00
MFS(23)	= -8,85 kN
NAA(16,24)	= 7,80
DAA(16,24)	= 0,00
MFS(25)	= -25,68 kN
NAA(18,2)	= -24,18
DAA(18,2)	= 0,56
LTF(21)	= 12,17 kN
LCF(25)	= -25,68 kN

group d) the sloping parabola plane members

MFS(26)	= -22,63 kN
NAA(10,19)	= -22,63
DAA(10,19)	= 0,56
MFS(28)	= 19,92 kN
NAA(12,21)	= -19,92
DAA(12,21)	= 0,56
MFS(30)	= 8,66 kN
NAA(15,22)	= -8,66
DAA(15,22)	= -0,56
MFS(32)	= 23,79 kN
NAA(17,24)	= -23,79
DAA(17,24)	= -0,56
LTF(27)	= 23,79 kN
LCF(0)	= 8,66 kN

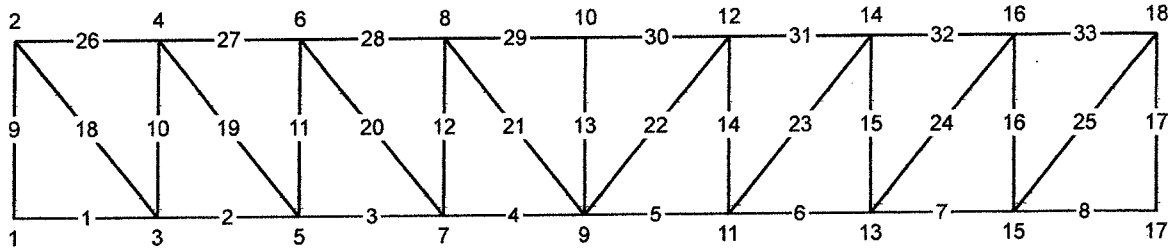
group e) the bottom parabola chord members

MFS(34)	= -33,66 kN
NAA(19,1)	= -32,51
DAA(19,1)	= 0,56
MFS(36)	= -20,01 kN
NAA(20,21)	= 20,01
DAA(20,21)	= 0,56
MFS(38)	= -1,14 kN
NAA(22,23)	= 0,99
DAA(22,23)	= 0,56
MFS(40)	= -48,42 kN
NAA(24,25)	= 47,67
DAA(24,25)	= 0,56
LTF(0)	= 0,00 kN
LCF(34)	= -82,61 kN

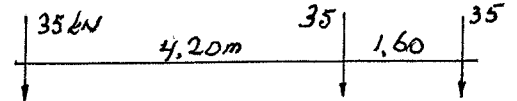
group f) the remaining vertical plane members

MFS(42)	= 17,93 kN
NAA(2,19)	= -16,13
DAA(2,19)	= 0,00
MFS(44)	= 18,38 kN
NAA(4,21)	= -16,13
DAA(4,21)	= 0,00
MFS(46)	= 18,38 kN
NAA(6,23)	= -16,13
DAA(6,23)	= 0,00
MFS(48)	= 17,18 kN
NAA(8,25)	= -16,13
DAA(8,25)	= 0,00
LTF(45)	= 18,53 kN
LCF(0)	= -1,00 kN

ProTruss2A



V9= 4 L9= 16,8 m H9= 2,6 m
N9= 18 joints and P9= 33 members



group a)	the bottom chord members	1 To 8
group b)	the vertical plane members	9 To 17
group c)	the sloping plane members	18 To 25
group d)	the top chord members	26 To 33

MF= 3 mobile forces

MFF(1) = 35,00 kN MA(1) = 0,00 m
MFF(2) = 35,00 kN MA(2) = 1,60 m
MFF(3) = 35,00 kN MA(3) = 4,20 m

I3= 1 K1= 3

group a) the bottom chord members
LTF1(4) = 84,13 kN LCF1(1) = 0,00 kN
group b) the vertical plane members
LTF1(12) = 20,83 kN LCF1(10) = -49,17 kN
group c) the sloping plane members
LTF1(18) = 63,20 kN LCF1(21) = -26,78 kN
group d) the top chord members
LTF1(0) = 0,00 kN LCF1(28) = -84,13 kN

I3= 3 K1= 1

LTF1(2) = 30,62 kN LCF1(1) = 0,00 kN
LTF1(12) = 5,42 kN LCF1(9) = -37,92 kN
LTF1(18) = 48,74 kN LCF1(19) = -6,96 kN
LTF1(0) = 0,00 kN LCF1(26) = -30,63 kN

I3= 3 K1= 3

LTF1(4) = 115,60 kN LCF1(1) = 0,00 kN
LTF1(12) = 7,29 kN LCF1(9) = -71,04 kN
LTF1(18) = 91,32 kN LCF1(21) = -9,37 kN
LTF1(0) = 0,00 kN LCF1(28) = -115,60 kN

I3= 5 K1= 1

LTF1(3) = 68,65 kN LCF1(1) = 0,00 kN
LTF1(12) = 14,17 kN LCF1(9) = -55,83 kN
LTF1(18) = 71,77 kN LCF1(20) = -18,21 kN
LTF1(0) = 0,00 kN LCF1(27) = -68,65 kN

I3= 5 K1= 3

LTF1(5) = 114,09 kN LCF1(1) = 0,00 kN
LTF1(13) = 0,00 kN LCF1(9) = -57,92 kN
LTF1(18) = 74,45 kN LCF1(0) = 0,00 kN
LTF1(0) = 0,00 kN LCF1(29) = -130,58 kN

I3= 7 K1= 1

LTF1(4) = 96,75 kN LCF1(1) = 0,00 kN
LTF1(12) = 23,96 kN LCF1(9) = -54,37 kN
LTF1(18) = 69,90 kN LCF1(21) = -30,80 kN
LTF1(0) = 0,00 kN LCF1(28) = -96,75 kN

After input of truss data and mobile forces click ForceDivision, load cases appear, not all visible if too many, click on the form to delete them and click CalculateMobForces. So 2 cases omitted.

Click Go to FDATA and click MOBMFORCESPR, next PrProK to print the results by the printer.

I3 is joint number of the bottom chord. K1 is force number.

I3=1 and K1=3, the 3rd force of 35 kN on joint 1, the 2nd and 1st force on the right of it.
I3=5 and K1=2, the 2nd force on joint 5, the 1st on the right and the 3rd on the left of it.

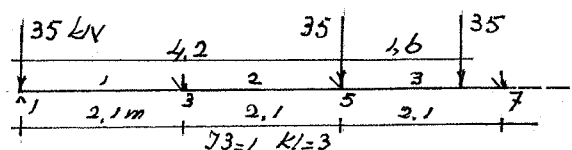
I3= 3 K1= 2

LTF1(3) = 58,56 kN LCF1(1) = 0,00 kN
LTF1(12) = 12,08 kN LCF1(9) = -57,92 kN
LTF1(18) = 74,45 kN LCF1(20) = -15,53 kN
LTF1(0) = 0,00 kN LCF1(27) = -58,56 kN

Case I3=1 - K1=1, 2nd and 3rd on the left of joint 1 omitted, and
case I3=1 - K1=2, 1st on the right of joint 1 and 3rd on the left of joint 1 omitted.
So 2 cases omitted.

I3= 5 K1= 2

LTF1(4) = 84,13 kN LCF1(1) = 0,00 kN
LTF1(12) = 20,83 kN LCF1(10) = -49,17 kN
LTF1(18) = 63,20 kN LCF1(21) = -26,78 kN
LTF1(0) = 0,00 kN LCF1(28) = -84,13 kN



I3= 7 K1= 2

LTF1(4) = 115,60 kN LCF1(1) = 0,00 kN
LTF1(12) = 7,29 kN LCF1(9) = -71,04 kN
LTF1(18) = 91,32 kN LCF1(21) = -9,37 kN
LTF1(0) = 0,00 kN LCF1(28) = -115,60 kN

I3= 7 K1= 3
 LTF1(5) = 124,35 kN
 LTF1(14)= 9,79 kN
 LTF1(24)= 77,39 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(16)= -60,21 kN
 LCF1(22)= -12,59 kN
 LCF1(31)= -124,35 kN

I3= 9 K1= 1
 LTF1(4) = 114,76 kN
 LTF1(13)= 0,00 kN
 LTF1(18)= 87,30 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(9) = -67,92 kN
 LCF1(0) = 0,00 kN
 LCF1(29)= -119,81 kN

I3= 9 K1= 2

LTF1(5) = 114,09 kN
 LTF1(0) = 0,00 kN
 LTF1(19)= 74,45 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(9) = -57,92 kN
 LCF1(0) = 0,00 kN
 LCF1(30)= -130,58 kN

I3= 9 K1= 3
 LTF1(5) = 99,62 kN
 LTF1(0) = 0,00 kN
 LTF1(25)= 94,27 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -73,33 kN
 LCF1(0) = 0,00 kN
 LCF1(30)= -102,31 kN

I3= 11 K1= 1
 LTF1(5) = 121,66 kN
 LTF1(0) = 0,00 kN
 LTF1(19)= 70,43 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(9) = -54,79 kN
 LCF1(0) = 0,00 kN
 LCF1(29)= -127,21 kN

I3= 11 K1= 2

LTF1(5) = 124,35 kN
 LTF1(14)= 9,79 kN
 LTF1(24)= 77,39 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(16)= -60,21 kN
 LCF1(22)= -12,59 kN
 LCF1(31)= -124,35 kN

I3= 11 K1= 3
 LTF1(5) = 74,88 kN
 LTF1(14)= 18,54 kN
 LTF1(25)= 76,86 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -59,79 kN
 LCF1(22)= -23,83 kN
 LCF1(31)= -74,88 kN

I3= 13 K1= 1
 LTF1(5) = 118,46 kN
 LTF1(14)= 6,67 kN
 LTF1(24)= 81,41 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(16)= -63,33 kN
 LCF1(22)= -8,57 kN
 LCF1(31)= -118,46 kN

I3= 13 K1= 2

LTF1(5) = 99,62 kN
 LTF1(13)= 0,00 kN
 LTF1(25)= 94,27 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -73,33 kN
 LCF1(0) = 0,00 kN
 LCF1(30)= -102,31 kN

I3= 13 K1= 3
 LTF1(6) = 42,40 kN
 LTF1(15)= 8,75 kN
 LTF1(24)= 33,74 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(16)= -26,25 kN
 LCF1(23)= -11,25 kN
 LCF1(32)= -42,40 kN

I3= 15 K1= 1
 LTF1(5) = 93,73 kN
 LTF1(14)= 1,88 kN
 LTF1(25)= 98,28 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -76,46 kN
 LCF1(22)= -2,41 kN
 LCF1(31)= -93,73 kN

I3= 15 K1= 2

LTF1(5) = 74,88 kN
 LTF1(14)= 18,54 kN
 LTF1(25)= 76,86 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -59,79 kN
 LCF1(22)= -23,83 kN
 LCF1(31)= -74,88 kN

I3= 15 K1= 3
 LTF1(7) = 24,74 kN
 LTF1(16)= 4,38 kN
 LTF1(25)= 39,37 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -30,62 kN
 LCF1(24)= -5,62 kN
 LCF1(33)= -24,74 kN

I3= 17 K1= 1
 LTF1(5) = 62,26 kN
 LTF1(14)= 15,42 kN
 LTF1(25)= 59,45 kN
 LTF1(0) = 0,00 kN

LCF1(1) = 0,00 kN
 LCF1(17)= -46,25 kN
 LCF1(22)= -19,82 kN
 LCF1(31)= -62,26 kN

Case I3=17 - K1=2, 1st on the right of joint 17 and 3rd force on the left of joint 17, and case I3=17 - K1=3, 1st and 2nd force on the right of joint 17.

Four cases calculated but results not shown. With 9 bottom chord joints results of 9*MF= 9*3= 27 minus 2*2 is 23 cases are shown. When clicking MOBFORCES results of all cases appear on the screen in a single column, just click and click...

group a) the bottom chord members
 LLTF(5) = 124,35 kN LLCF(1) = 0,00 kN

group b) the vertical plane members page 19
 LLTF(12)= 23,96 kN LLCF(17)= -76,46 kN

group c) the sloping plane members
 LLTF(25)= 98,28 kN LLCF(21)= -30,80 kN

group d) the top chord members
 LLTF(33)= 0,00 kN LLCF(29)= -130,58 kN

With forces in reversed order final results.

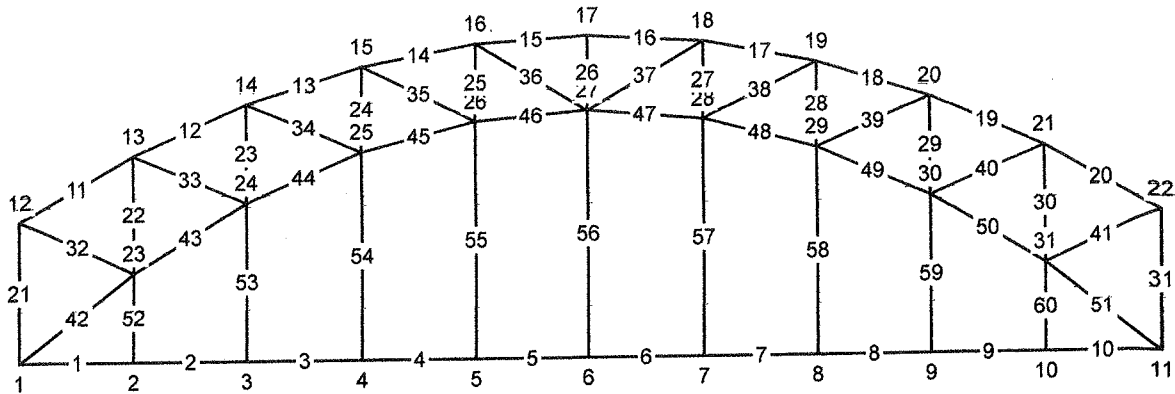
group a) the bottom chord members
 LLTF(4) = 124,35 kN LLCF(1) = 0,00 kN

group b) the vertical plane members
 LLTF(14)= 23,96 kN LLCF(9) = -76,46 kN

group c) the sloping plane members
 LLTF(18)= 98,28 kN LLCF(22)= -30,80 kN

group d) the top chord members
 LLTF(33)= 0,00 kN LLCF(29)= -130,58 kN

ProParTruss3



V9= 5 L9= 36,4 m H9= 10,3 m A8= 4,5 m A7= 2,4 m
N9= 31 joints and P9= 60 members

group a)	the bottom chord members	1 To 10
group b)	the top parabola chord members	11 To 20
group c)	the vertical parabola plane members	21 To 31
group d)	the sloping parabola plane members	32 To 41
group e)	the bottom parabola chord members	42 To 51
group f)	the remaining vertical plane members	52 To 60

MF= 2 mobile forces

MFF(1) = 82,00 kN MA(1) = 0,00 m
MFF(2) = 82,00 kN MA(2) = 8,37 m

I3= 1 K1= 2

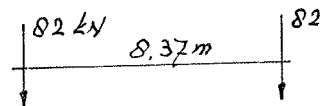
group a) the bottom chord members
LTF1(10)= 36,98 kN LCF1(0) = 0,00 kN
group b) the top parabola chord members
LTF1(19)= 17,24 kN LCF1(12)= -94,63 kN
group c) the vertical parabola plane members
LTF1(24)= 33,49 kN LCF1(22)= -41,81 kN
group d) the sloping parabola plane members
LTF1(33)= 57,63 kN LCF1(36)= -36,80 kN
group e) the bottom parabola chord members
LTF1(44)= 53,89 kN LCF1(49)= -57,48 kN
group f) the remaining vertical plane members
LTF1(53)= 57,45 kN LCF1(0) = 0,00 kN

I3= 2 K1= 1

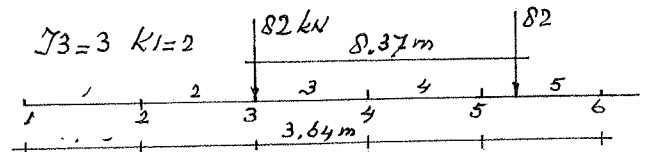
LTF1(10)= 17,59 kN	LCF1(0) = 0,00 kN
LTF1(18)= 10,44 kN	LCF1(11)= -67,31 kN
LTF1(22)= 16,90 kN	LCF1(21)= -60,05 kN
LTF1(32)= 64,14 kN	LCF1(35)= -17,06 kN
LTF1(43)= 47,73 kN	LCF1(49)= -29,29 kN
LTF1(52)= 82,00 kN	LCF1(0) = 0,00 kN

I3= 3 K1= 1

LTF1(8)= 33,23 kN	LCF1(0) = 0,00 kN
LTF1(19)= 16,87 kN	LCF1(12)= -107,40 kN
LTF1(23)= 32,01 kN	LCF1(22)= -46,72 kN
LTF1(33)= 64,61 kN	LCF1(35)= -32,75 kN
LTF1(44)= 70,70 kN	LCF1(49)= -53,03 kN
LTF1(53)= 82,00 kN	LCF1(0) = 0,00 kN



After input mobile forces click
ForceDivision and CalculateMobForces.



Click Go to FDATA next
MOBMOFORCESPR, SHORT and PrPrOK to get
the results by the printer shown here.

I3= 2 K1= 2

LTF1(10)= 65,77 kN	LCF1(0) = 0,00 kN
LTF1(19)= 26,33 kN	LCF1(13)= -142,89 kN
LTF1(25)= 52,36 kN	LCF1(21)= -77,36 kN
LTF1(32)= 82,63 kN	LCF1(36)= -67,87 kN
LTF1(45)= 72,72 kN	LCF1(49)= -97,91 kN
LTF1(52)= 82,00 kN	LCF1(0) = 0,00 kN

I3= 3 K1= 2

LTF1(10)= 87,87 kN	LCF1(0) = 0,00 kN
LTF1(19)= 23,67 kN	LCF1(14)= -152,62 kN
LTF1(25)= 50,38 kN	LCF1(22)= -60,39 kN
LTF1(33)= 82,35 kN	LCF1(36)= -55,20 kN
LTF1(46)= 62,27 kN	LCF1(50)= -122,16 kN
LTF1(53)= 82,00 kN	LCF1(0) = 0,00 kN

I3= 4 K1= 1
 LTF1(10)= 58,07 kN
 LTF1(19)= 25,22 kN
 LTF1(24)= 53,72 kN
 LTF1(32)= 68,07 kN
 LTF1(45)= 86,47 kN
 LTF1(54)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(13)= -148,77 kN
 LCF1(21)= -63,73 kN
 LCF1(36)= -58,82 kN
 LCF1(49)= -88,41 kN
 LCF1(0) = 0,00 kN

I3= 4 K1= 2
 LTF1(10)= 101,42 kN
 LTF1(20)= 12,54 kN
 LTF1(24)= 20,45 kN
 LTF1(34)= 85,12 kN
 LTF1(45)= 36,72 kN
 LTF1(54)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(16)= -145,31 kN
 LCF1(23)= -51,21 kN
 LCF1(41)= -11,95 kN
 LCF1(50)= -131,40 kN
 LCF1(0) = 0,00 kN

I3= 5 K1= 1
 LTF1(10)= 82,42 kN
 LTF1(19)= 26,50 kN
 LTF1(25)= 70,54 kN
 LTF1(37)= 70,80 kN
 LTF1(46)= 77,24 kN
 LTF1(55)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(14)= -162,25 kN
 LCF1(21)= -52,86 kN
 LCF1(36)= -88,66 kN
 LCF1(50)= -116,52 kN
 LCF1(0) = 0,00 kN

I3= 5 K1= 2
 LTF1(10)= 105,30 kN
 LTF1(11)= 3,06 kN
 LTF1(25)= 26,71 kN
 LTF1(35)= 92,11 kN
 LTF1(46)= 39,61 kN
 LTF1(55)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(14)= -147,38 kN
 LCF1(24)= -48,50 kN
 LCF1(36)= -14,57 kN
 LCF1(42)= -133,63 kN
 LCF1(0) = 0,00 kN

I3= 6 K1= 1
 LTF1(10)= 98,44 kN
 LTF1(20)= 15,44 kN
 LTF1(26)= 19,73 kN
 LTF1(37)= 99,22 kN
 LTF1(46)= 36,15 kN
 LTF1(56)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(16)= -155,11 kN
 LCF1(27)= -47,34 kN
 LCF1(41)= -14,71 kN
 LCF1(50)= -130,86 kN
 LCF1(0) = 0,00 kN

I3= 6 K1= 2
 LTF1(8)= 98,44 kN
 LTF1(11)= 15,44 kN
 LTF1(26)= 19,73 kN
 LTF1(36)= 99,22 kN
 LTF1(47)= 36,15 kN
 LTF1(56)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(16)= -155,11 kN
 LCF1(25)= -47,34 kN
 LCF1(32)= -14,71 kN
 LCF1(43)= -130,86 kN
 LCF1(0) = 0,00 kN

I3= 7 K1= 1
 LTF1(10)= 105,30 kN
 LTF1(20)= 3,06 kN
 LTF1(27)= 26,71 kN
 LTF1(38)= 92,11 kN
 LTF1(47)= 39,61 kN
 LTF1(57)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(17)= -147,38 kN
 LCF1(28)= -48,50 kN
 LCF1(37)= -14,57 kN
 LCF1(42)= -133,63 kN
 LCF1(0) = 0,00 kN

I3= 7 K1= 2
 LTF1(8)= 82,42 kN
 LTF1(12)= 26,50 kN
 LTF1(27)= 70,54 kN
 LTF1(36)= 70,80 kN
 LTF1(47)= 77,24 kN
 LTF1(57)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(17)= -162,25 kN
 LCF1(31)= -52,86 kN
 LCF1(37)= -88,66 kN
 LCF1(43)= -116,52 kN
 LCF1(0) = 0,00 kN

I3= 8 K1= 1
 LTF1(8)= 101,42 kN
 LTF1(11)= 12,54 kN
 LTF1(28)= 20,45 kN
 LTF1(39)= 85,12 kN
 LTF1(48)= 36,72 kN
 LTF1(58)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(15)= -145,31 kN
 LCF1(29)= -51,21 kN
 LCF1(32)= -11,95 kN
 LCF1(43)= -131,40 kN
 LCF1(0) = 0,00 kN

I3= 8 K1= 2
 LTF1(7)= 58,07 kN
 LTF1(12)= 25,22 kN
 LTF1(28)= 53,72 kN
 LTF1(41)= 68,07 kN
 LTF1(48)= 86,47 kN
 LTF1(58)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(18)= -148,77 kN
 LCF1(31)= -63,73 kN
 LCF1(37)= -58,82 kN
 LCF1(44)= -88,41 kN
 LCF1(0) = 0,00 kN

I3= 9 K1= 1
 LTF1(10)= 87,87 kN
 LTF1(12)= 23,67 kN
 LTF1(27)= 50,38 kN
 LTF1(40)= 82,35 kN
 LTF1(47)= 62,27 kN
 LTF1(59)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(17)= -152,62 kN
 LCF1(30)= -60,39 kN
 LCF1(37)= -55,20 kN
 LCF1(43)= -122,16 kN
 LCF1(0) = 0,00 kN

I3= 9 K1= 2
 LTF1(10)= 33,23 kN
 LTF1(12)= 16,87 kN
 LTF1(29)= 32,01 kN
 LTF1(40)= 64,61 kN
 LTF1(49)= 70,70 kN
 LTF1(59)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(19)= -107,40 kN
 LCF1(30)= -46,72 kN
 LCF1(38)= -32,75 kN
 LCF1(44)= -53,03 kN
 LCF1(0) = 0,00 kN

I3= 10 K1= 1
 LTF1(10)= 65,77 kN
 LTF1(12)= 26,33 kN
 LTF1(27)= 52,36 kN
 LTF1(41)= 82,63 kN
 LTF1(48)= 72,72 kN
 LTF1(60)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(18)= -142,89 kN
 LCF1(31)= -77,36 kN
 LCF1(37)= -67,87 kN
 LCF1(44)= -97,91 kN
 LCF1(0) = 0,00 kN

I3= 10 K1= 2
 LTF1(10)= 17,59 kN
 LTF1(13)= 10,44 kN
 LTF1(30)= 16,90 kN
 LTF1(41)= 64,14 kN
 LTF1(50)= 47,73 kN
 LTF1(60)= 82,00 kN

LCF1(0) = 0,00 kN
 LCF1(20)= -67,31 kN
 LCF1(31)= -60,05 kN
 LCF1(38)= -17,06 kN
 LCF1(44)= -29,29 kN
 LCF1(0) = 0,00 kN

I3= 11 K1= 1
 LTF1(7)= 36,98 kN
 LTF1(12)= 17,24 kN
 LTF1(28)= 33,49 kN
 LTF1(40)= 57,63 kN
 LTF1(49)= 53,89 kN
 LTF1(59)= 57,45 kN

LCF1(0) = 0,00 kN
 LCF1(19)= -94,63 kN
 LCF1(30)= -41,81 kN
 LCF1(37)= -36,80 kN
 LCF1(44)= -57,48 kN
 LCF1(0) = 0,00 kN

Click MOBMFORCESPR and SHORT, then the truss, input data, mobile forces and the final results here below are printed by the printer.

group a) the bottom chord members
 LLTF(10)= 105,30 kN LLCF(0) = 0,00 kN

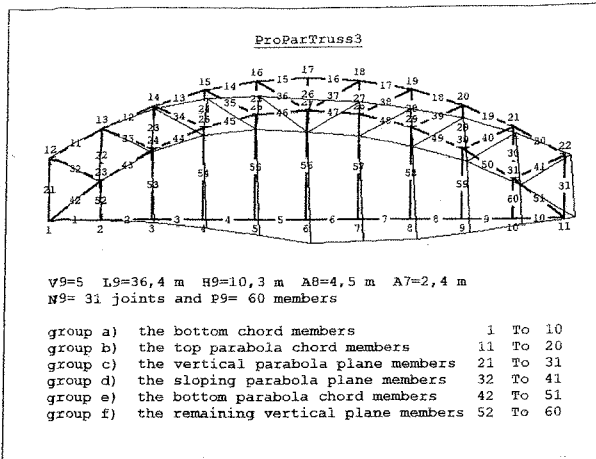
group b) the top parabola chord members
 LLTF(19)= 26,50 kN LLCF(14)= -162,25 kN

group c) the vertical parabola plane members
 LLTF(27)= 70,54 kN LLCF(31)= -77,36 kN

group d) the sloping parabola plane members
 LLTF(36)= 99,22 kN LLCF(36)= -88,66 kN

group e) the bottom parabola chord members
 LLTF(48)= 86,47 kN LLCF(42)= -133,63 kN

group f) the remaining vertical plane members
 LLTF(60)= 82,00 kN LLCF(0) = 0,00 kN



NAA(20,21)= 82,00 NAA(21,20)= -82,00 NAA(21,22)= 26,84 NAA(22,21)= -26,84
DAA(20,21)= 0,00 DAA(21,20)= 0,00 DAA(21,22)= 0,00 DAA(22,21)= 0,00
LTF(11)= 15,43 kN LCF(16)= -155,10 kN

group c) the vertical parabola plane members

MFS(21)= 13,77 kN NAA(12,1)= 13,77 MFS(22)= -2,86 kN NAA(23,13)= -2,86
NAA(1,12)= -13,77 NAA(12,1)= 13,77 DAA(13,23)= 2,86 DAA(23,13)= 0,00
DAA(1,12)= 0,00 DAA(12,1)= 0,00
MFS(23)= -20,56 kN NAA(24,14)= -20,56 MFS(24)= -36,73 kN NAA(25,15)= -36,73
NAA(14,24)= 20,56 NAA(24,14)= -20,56 DAA(15,25)= 36,73 DAA(25,15)= 0,00
DAA(14,24)= 0,00 DAA(24,14)= 0,00
MFS(25)= -47,33 kN NAA(26,16)= -47,33 MFS(26)= 19,73 kN NAA(27,17)= 19,73
NAA(16,26)= 47,33 NAA(26,16)= -47,33 DAA(17,27)= -19,73 DAA(27,17)= 0,00
DAA(16,26)= 0,00 DAA(26,16)= 0,00
MFS(27)= 3,72 kN NAA(28,18)= 3,72 MFS(28)= 14,41 kN NAA(29,19)= 14,41
NAA(18,28)= -3,72 NAA(28,18)= 3,72 DAA(19,29)= -14,41 DAA(29,19)= 0,00
DAA(18,28)= 0,00 DAA(28,18)= 0,00
MFS(29)= -32,63 kN NAA(30,20)= -32,63 MFS(30)= -41,83 kN NAA(31,21)= -41,83
NAA(20,30)= 32,63 NAA(30,20)= -32,63 DAA(21,31)= 41,83 DAA(31,21)= -41,83
DAA(20,30)= 0,00 DAA(30,20)= 0,00
MFS(31)= -23,95 kN NAA(22,11)= -23,95 MFS(32)= 19,73 kN LCF(25)= -47,33 kN
NAA(11,22)= 23,95 NAA(22,11)= -23,95 DAA(11,22)= 0,00 DAA(22,11)= 0,00
LTF(26)= 19,73 kN LCF(25)= -47,33 kN

I3= 6 K1= 2

LTF1(8)= 98,44 kN LCF1(0)= 0,00 kN a) LTF(8)= 98,44 kN LCF(0)= 0 kN
LTF1(11)= 15,44 kN LCF1(16)= -155,11 kN b) LTF(11)= 15,43 kN LCF(16)= -155,10 kN
LTF1(26)= 19,73 kN LCF1(25)= -47,34 kN c) LTF(26)= 19,73 kN LCF(25)= -47,33 kN
LTF1(36)= 99,22 kN LCF1(32)= -14,71 kN d) LTF(36)= 99,21 kN LCF(32)= -14,71 kN
LTF1(47)= 36,15 kN LCF1(43)= -130,86 kN e) LTF(47)= 36,14 kN LCF(43)= -130,85 kN
LTF1(56)= 82,00 kN LCF1(0)= 0,00 kN f) LTF(56)= 82,00 kN LCF(0)= 0

ProTruss2A of page 16.

V9=4 L9=16,8 m H9=2,6 m

After input click ProTruss2A, type in TSTRING
MF=3 Enter, 1,35,0 Enter,
2,35,1.6 Enter and 3,35,4.2 Enter.

After data input click Show to check input.
Click Forcedivision showing load force cases,
click the Form to get back the controls, click
CalculateMobForces, go to FDATA.
Click SHORT and PrPr OK to get the printer
print shown on the left with the largest LLTF()
and LLCF() for each group of members.

The mobile forces in reversed order.

Back to the first form, click UV(I)=0 UH(I)=0,
Click Show, ah, FY(17)=-35, make it zero in
TSTRING FY(17)=0 Enter. Click Show, ok,
click IRQ, Show, forces in reversed order.

ForceDivision, click form, CalculateMobForces,
go to FDATA, SHORT and PrPrOK, second results
below the first.

Comparing results.

LLTF(5)= 124,35 kN and LLTF(4)= 124,35 kN,
LLTF(25)= 98,28 kN and LLTF(18)= 98,28 kN,
LLCF(21)= -30,80 kN and LLCF(22)= -30,80 kN.
Note the different member numbers.

TRUSSPROGRAM5555

Three 'roof trusses'.

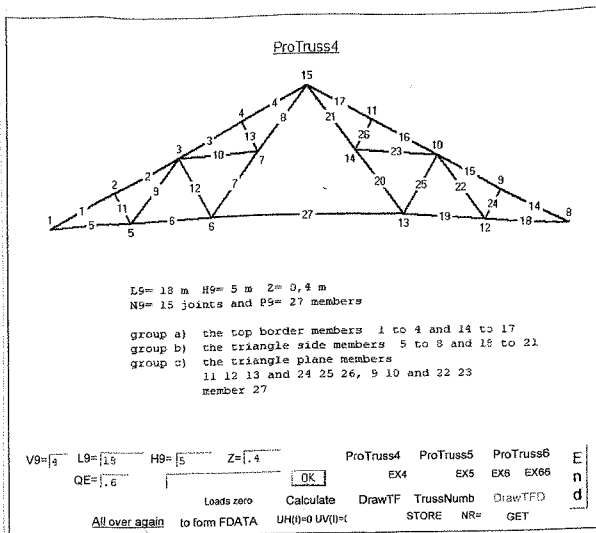
ProTruss4

page 22 31

L9=18 m H9=5 m Z=0.4 m

N9= 15 joints and
P9= 27 members divided into 4 groups.

- the top border members 1 to 4 and 14 to 17
- the triangle side members 5 to 8 and 18 to 21
- the triangle plane members
11 12 13 and 24 25 26, 9 10 and 22 23
member 27



ProTruss4 L9=18 m H9= 5 m Z= 0,4 m

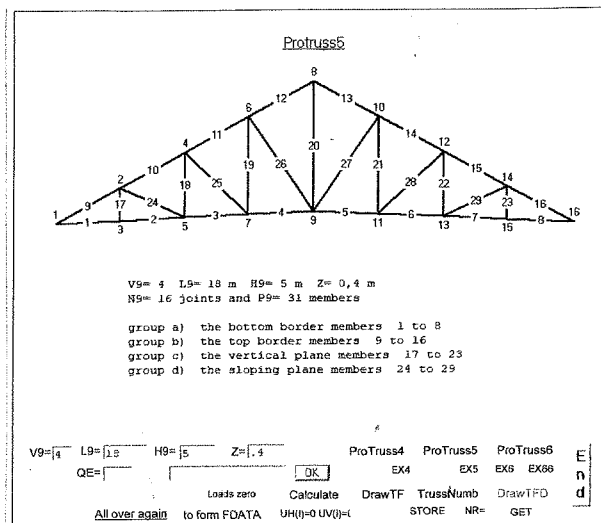
ProTruss5

page 25 34

V9=4 L9=18 m H9=5 m Z=0.4 m

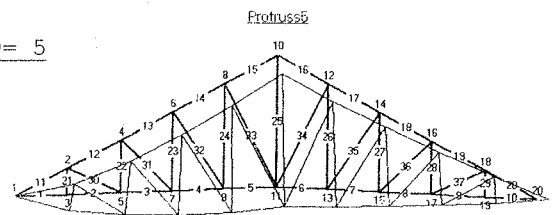
V9= 1, 2, 3 etc.
N9= V9*4= 16 joints and
P9= V9*8-3= 29 members divided into 4 groups.

- the bottom border members 1 to 8
- the top border members 9 to 16
- the vertical plane members 17 to 23
- the sloping plane members 24 to 29



ProTruss5 L9=18 m H9= 5 m Z= 0,4 m

V9= 5



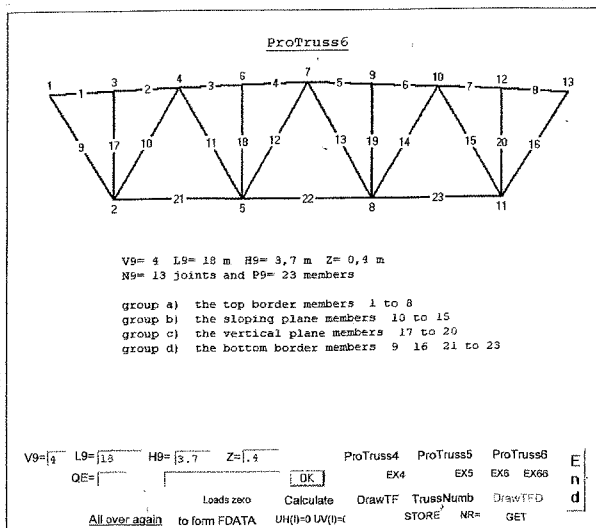
ProTruss6

page 27 38

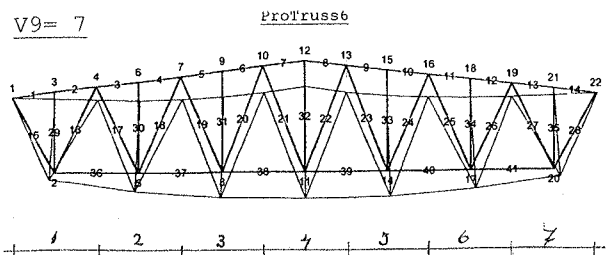
V9=4 L9=18 H9=3.7 Z=0.4

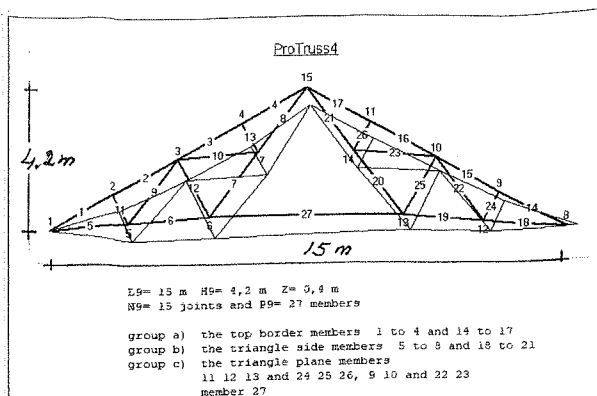
V9= 1, 2, 3 etc.
N9= V9*2+1= 13 joints and
P9= V9*6-1= 23 members divided into 4 groups.

- the top border members 1 to 8
- the sloping plane members 10 to 15
- the vertical plane members 17 to 20
- the bottom border members 9 16 21 to 23



ProTruss6 L9=18 m H9= 3,7 m Z= 0,4 m





ProTruss4
the top border members

MFS(1) = -53,24 kN	MFS(2) = -53,24 kN	MFS(3) = -53,24 kN	MFS(4) = -53,24 kN
MFS(14) = -29,72 kN	MFS(15) = -29,72 kN	MFS(16) = -29,72 kN	MFS(17) = -29,72 kN
LTF(0) = 0,00 kN	LCF(18) = -53,24 kN		

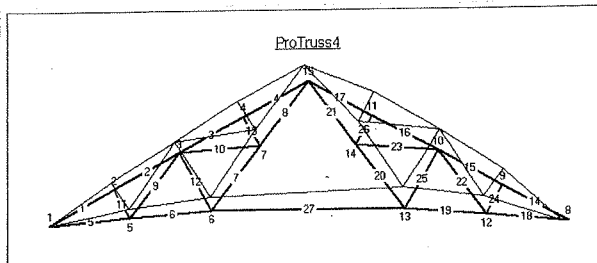
the triangle side members

MFS(5) = 65,05 kN	MFS(6) = 52,05 kN	MFS(7) = 20,76 kN	MFS(8) = 41,70 kN
MFS(18) = 26,02 kN	MFS(19) = 26,02 kN	MFS(20) = 2,74 kN	MFS(21) = 2,74 kN
LTF(5) = 65,05 kN	LCF(0) = 0,00 kN		

the triangle plane members

MFS(9) = 13,01 kN	MFS(10) = 13,01 kN	MFS(11) = -10,74 kN	MFS(12) = -21,49 kN
MFS(13) = -10,74 kN	MFS(14) = -10,74 kN	MFS(15) = -10,74 kN	MFS(16) = -10,74 kN
MFS(22) = 0,00 kN	MFS(23) = 0,00 kN	MFS(24) = 0,00 kN	MFS(25) = 0,00 kN
MFS(26) = 0,00 kN	MFS(27) = 24,31 kN		
LTF(10) = 13,01 kN	LCF(12) = -21,49 kN		

RV(1) = -21,00 kN	RV(11) = 25,19 kN	RV(8) = 12,32 kN
UH(1) = 0,0 /EA	UH(11) = 0,0 /EA	UH(2) = 571,9 /EA
UH(3) = 669,0 /EA	UH(9) = -1662,9 /EA	UH(4) = 679,3 /EA
UH(5) = 274,0 /EA	UH(10) = -1440,2 /EA	UH(6) = 426,3 /EA
UH(7) = 718,4 /EA	UH(12) = -1881,5 /EA	UH(8) = 791,4 /EA
UH(9) = 449,3 /EA	UH(13) = -741,5 /EA	UH(10) = 317,5 /EA
UH(11) = 226,1 /EA	UH(14) = -1401,6 /EA	UH(12) = 956,8 /EA
UH(13) = 562,3 /EA	UH(15) = -1244,4 /EA	UH(14) = 289,6 /EA
UH(15) = 279,8 /EA	UH(16) = -1436,3 /EA	UH(15) = -1437,2 /EA



ProTruss4
the top border members

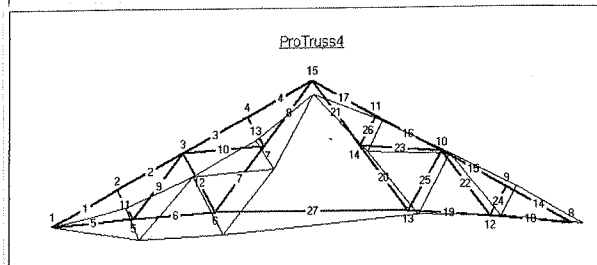
MFS(1) = 20,33 kN	MFS(2) = 20,33 kN	MFS(3) = 20,33 kN	MFS(4) = 20,33 kN
MFS(14) = 35,14 kN	MFS(15) = 35,14 kN	MFS(16) = 35,14 kN	MFS(17) = 35,14 kN
LTF(15) = 35,14 kN	LCF(0) = 0,00 kN		

the triangle side members

MFS(5) = -0,94 kN	MFS(6) = -0,94 kN	MFS(7) = -0,10 kN	MFS(8) = -0,10 kN
MFS(18) = -32,17 kN	MFS(19) = -21,76 kN	MFS(20) = -20,92 kN	MFS(21) = -31,33 kN
LTF(0) = 0,00 kN	LCF(18) = -32,17 kN		

the triangle plane members

MFS(9) = 0,00 kN	MFS(10) = 0,00 kN	MFS(11) = 0,00 kN	MFS(12) = 0,00 kN
MFS(13) = 0,00 kN	MFS(14) = 0,00 kN	MFS(15) = 0,00 kN	MFS(16) = 0,00 kN
MFS(22) = -10,41 kN	MFS(23) = -10,41 kN	MFS(24) = 9,60 kN	MFS(25) = 17,19 kN
MFS(26) = 9,60 kN	MFS(27) = -0,89 kN		
LTF(25) = 17,19 kN	LCF(22) = -10,41 kN		



ProTruss4
the top border members

MFS(1) = -32,91 kN	MFS(2) = -32,91 kN	MFS(3) = -32,91 kN	MFS(4) = -32,91 kN
MFS(14) = 9,42 kN	MFS(15) = 9,42 kN	MFS(16) = 9,42 kN	MFS(17) = 9,42 kN
LTF(16) = 9,42 kN	LCF(4) = -32,91 kN		

the triangle side members

MFS(5) = 64,12 kN	MFS(6) = 51,11 kN	MFS(7) = 28,66 kN	MFS(8) = 41,68 kN
MFS(18) = -6,14 kN	MFS(19) = 4,27 kN	MFS(20) = -18,18 kN	MFS(21) = -28,59 kN
LTF(5) = 64,12 kN	LCF(21) = -28,59 kN		

the triangle plane members

MFS(9) = 13,01 kN	MFS(10) = 13,01 kN	MFS(11) = -10,74 kN	MFS(12) = -21,49 kN
MFS(13) = -10,74 kN	MFS(14) = -10,74 kN	MFS(15) = -10,74 kN	MFS(16) = -10,74 kN
MFS(22) = -10,41 kN	MFS(23) = -10,41 kN	MFS(24) = 9,60 kN	MFS(25) = 17,19 kN
MFS(26) = 9,60 kN	MFS(27) = 23,49 kN		
LTF(25) = 17,19 kN	LCF(12) = -21,49 kN		

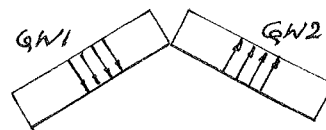
Example.

EX4

First case.

QW1= 5 kN/m QW2= 0 kN/m

Click in TL9 and type 15, Tab, cursor in TH9, type 4.2, Tab, cursor in TZ9, type .4.



Assumed direction of wind load forces, QW1 and QW2 belong together, in the example separated. After input of truss data click ProTruss4. Next the wind loads QW=,QW1,QW2 in TSTRING QW=,5,0 Enter. Or click EX4 and ProTruss4.

Next DRAWTF to draw the truss, click TrussNumb to number joints and members. Click Calculate and DrawTFD to draw the deformation of the truss.

Click to form FDATA and click MFORCES to get the member forces MFS(), the largest tension forces LTF() and compression forces LCF() for each group of members. And UHUV for the joint displacement

Second case. QW1= 0 kN/m QW2= 4 kN/m

Going on with the first case. Go back to the first form, click go back to TRUSSPROGRAMS.

Click Loads zero, UH(I)=0UV(I)=0 an Cls.

In TSTRING type QW=,0,4 Enter, and click DrawTF, TrussNumb, Calculate and DrawTFD, go to FDATA, Cls, MFORCES, and UHUV shown here below.

RV(1) = -16,80 kN	RV(11) = -5,95 kN	RV(8) = -20,15 kN
UH(1) = 0,0 /EA	UH(11) = 0,0 /EA	UH(2) = -165,3 /EA
UH(3) = -213,8 /EA	UH(9) = 560,6 /EA	UH(4) = -270,8 /EA
UH(5) = -39,0 /EA	UH(10) = 431,8 /EA	UH(6) = -69,5 /EA
UH(7) = -231,9 /EA	UH(12) = 778,7 /EA	UH(8) = -381,6 /EA
UH(9) = 57,6 /EA	UH(13) = 777,8 /EA	UH(10) = 88,4 /EA
UH(11) = 80,5 /EA	UH(14) = 1168,9 /EA	UH(12) = -131,1 /EA
UH(13) = -64,4 /EA	UH(15) = 1052,1 /EA	UH(14) = 129,6 /EA
UH(15) = -239,5 /EA	UH(16) = 774,5 /EA	UH(15) = 1129,2 /EA

Third case. QW1= 5 kN/m QW2= 4 kN/m

Click Loads zero and UH(I)=0UV(I)=0, next QW=,5,4 Enter, DrawTF, TrussNumb etc.

Comparing some calculation results.

Case 1 MFS(1)= -53,24 kN UV(15)= -1436/EA
Case 2 MFS(1)= 20,33 kN UV(15)= 775/EA +
Case 3 MFS(1)= -32,91 kN UV(15)= -662/EA

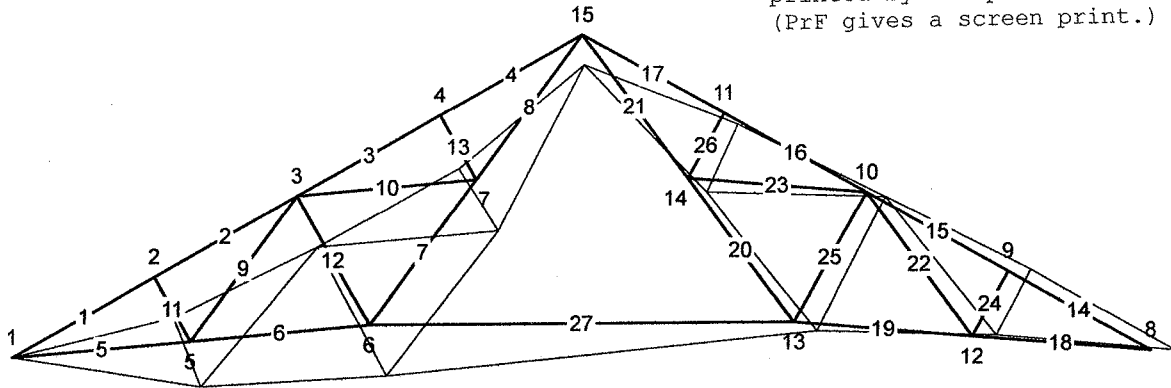
group b)

Case 1 LTF(5)= 65,05 kN LCF(0)= 0
Case 2 LTF(0)= 0 LCF(18)= -32,17 kN
Case 3 LTF(5)= 64,12 kN LCF(21)= -28,59 kN

RV(1) = -97,80 kN	RV(11) = 15,33 kN	RV(8) = -7,83 kN
UH(1) = 0,0 /EA	UH(11) = 0,0 /EA	UH(2) = 416,6 /EA
UH(3) = 455,2 /EA	UH(9) = -1102,3 /EA	UH(4) = 408,5 /EA
UH(5) = 235,1 /EA	UH(10) = -978,4 /EA	UH(6) = 366,9 /EA
UH(7) = 486,5 /EA	UH(12) = -1159,0 /EA	UH(8) = 509,8 /EA
UH(9) = 506,9 /EA	UH(13) = 36,3 /EA	UH(10) = 406,0 /EA
UH(11) = 396,5 /EA	UH(14) = -238,6 /EA	UH(12) = 526,7 /EA
UH(13) = 497,5 /EA	UH(15) = -192,9 /EA	UH(14) = 413,2 /EA
UH(15) = 46,4 /EA	UH(16) = -661,9 /EA	UH(15) = -307,9 /EA

ProTruss4

Click met left mouse button
AMEFORCESPR for these results
printed by the printer.
(PrF gives a screen print.)



L9= 15 m H9= 4,2 m Z= 0,4 m
N9= 15 joints and P9= 27 members

Third case prec. page.

- group a) the top border members 1 to 4 and 14 to 17
group b) the triangle side members 5 to 8 and 18 to 21
group c) the triangle plane members
11 12 13 and 24 25 26, 9 10 and 22 23
member 27

ProTruss4

the top border members

MFS(1) =	-32,91 kN	MFS(2) =	-32,91 kN	MFS(3) =	-32,91 kN
NAA(1,2) =	32,91	NAA(2,3) =	32,91	NAA(3,4) =	32,91
DAA(1,2) =	0,00	DAA(2,3) =	0,00	DAA(3,4) =	0,00
MFS(4) =	-32,91 kN	MFS(5) =	-32,91 kN	MFS(6) =	-32,91 kN
NAA(4,3) =	-32,91	NAA(4,15) =	32,91	NAA(4,15) =	32,91
DAA(4,3) =	0,00	DAA(4,15) =	0,00	DAA(4,15) =	0,00
MFS(14) =	9,42 kN	MFS(15) =	9,42 kN	MFS(16) =	9,42 kN
NAA(8,9) =	-9,42	NAA(9,10) =	-9,42	NAA(10,11) =	-9,42
DAA(8,9) =	0,00	DAA(9,10) =	0,00	DAA(10,11) =	0,00
MFS(16) =	9,42 kN	MFS(17) =	9,42 kN	MFS(18) =	9,42 kN
NAA(10,11) =	-9,42	NAA(11,15) =	-9,42	NAA(12,13) =	-9,42
DAA(10,11) =	0,00	DAA(11,15) =	0,00	DAA(12,13) =	0,00
LTF(16) =	9,42 kN	LCF(4) =	-32,91 kN	LTF(16) =	9,42 kN

the triangle side members

MFS(5) =	64,12 kN	MFS(6) =	51,11 kN	MFS(7) =	28,66 kN
NAA(1,5) =	-64,12	NAA(5,6) =	-51,11	NAA(6,7) =	-28,66
DAA(1,5) =	0,00	DAA(5,6) =	0,00	DAA(6,7) =	0,00
MFS(8) =	28,66 kN	MFS(9) =	41,68 kN	MFS(10) =	41,68 kN
NAA(6,7) =	-28,66	NAA(7,15) =	-41,68	NAA(8,12) =	-41,68
DAA(6,7) =	0,00	DAA(7,15) =	0,00	DAA(8,12) =	0,00
MFS(18) =	-6,14 kN	MFS(19) =	4,27 kN	MFS(20) =	-18,18 kN
NAA(8,12) =	6,14	NAA(12,13) =	-4,27	NAA(13,14) =	18,18
DAA(8,12) =	0,00	DAA(12,13) =	0,00	DAA(13,14) =	0,00
MFS(20) =	-18,18 kN	MFS(21) =	-28,59 kN	MFS(22) =	-10,41 kN
NAA(13,14) =	18,18	NAA(14,15) =	28,59	NAA(15,16) =	-10,41
DAA(13,14) =	0,00	DAA(14,15) =	0,00	DAA(15,16) =	0,00
LTF(5) =	64,12 kN	LCF(21) =	-28,59 kN	LTF(5) =	64,12 kN

the triangle plane members

MFS(9) =	13,01 kN	MFS(10) =	13,01 kN	MFS(11) =	-10,74 kN
NAA(3,5) =	-13,01	NAA(3,7) =	-13,01	NAA(2,5) =	10,74
DAA(3,5) =	0,00	DAA(3,7) =	0,00	DAA(2,5) =	0,00
MFS(12) =	-21,49 kN	MFS(13) =	-10,74 kN	MFS(14) =	-10,74 kN
NAA(5,2) =	-10,74	NAA(5,3) =	13,01	NAA(4,7) =	10,74
DAA(5,2) =	0,00	DAA(5,3) =	0,00	DAA(4,7) =	0,00
MFS(23) =	-10,41 kN	MFS(24) =	10,41 kN	MFS(25) =	10,41 kN
NAA(3,6) =	0,00	NAA(3,6) =	0,00	NAA(10,12) =	10,41
DAA(3,6) =	0,00	DAA(3,6) =	0,00	DAA(10,12) =	0,00
MFS(26) =	10,41 kN	MFS(27) =	10,41 kN	MFS(28) =	10,41 kN
NAA(6,3) =	-21,49	NAA(6,3) =	-21,49	NAA(12,10) =	-10,41
DAA(6,3) =	0,00	DAA(6,3) =	0,00	DAA(12,10) =	0,00
MFS(29) =	10,41 kN	MFS(30) =	10,41 kN	MFS(31) =	10,41 kN
NAA(14,10) =	-10,41	NAA(14,10) =	-10,41	NAA(16,10) =	-10,41
DAA(14,10) =	0,00	DAA(14,10) =	0,00	DAA(16,10) =	0,00

MFS(24) = 8,60 kN	MFS(25) = 17,19 kN
NAA(9,12) = -8,60	NAA(12,9) = 8,60
DAA(9,12) = 0,00	DAA(12,9) = 0,00
MFS(26) = 8,60 kN	MFS(25) = 17,19 kN
NAA(11,14) = -8,60	NAA(14,11) = 8,60
DAA(11,14) = 0,00	DAA(14,11) = 0,00
LTF(25) = 17,19 kN	LCF(12) = -21,49 kN

MFS(27) = 23,43 kN

ProTruss4

the top border members

MFS(1) = -32,91 kN	MFS(2) = -32,91 kN	MFS(3) = -32,91 kN	MFS(4) = -32,91 kN
MFS(14) = 9,42 kN	MFS(15) = 9,42 kN	MFS(16) = 9,42 kN	MFS(17) = 9,42 kN
LTF(16) = 9,42 kN	LCF(4) = -32,91 kN		

the triangle side members

MFS(5) = 64,12 kN	MFS(6) = 51,11 kN	MFS(7) = 28,66 kN	MFS(8) = 41,68 kN
MFS(18) = -6,14 kN	MFS(19) = 4,27 kN	MFS(20) = -18,18 kN	MFS(21) = -28,59 kN
LTF(5) = 64,12 kN	LCF(21) = -28,59 kN		

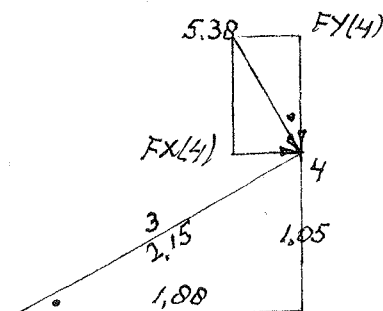
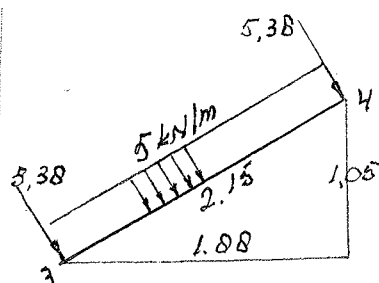
the triangle plane members

MFS(9) = 13,01 kN	MFS(10) = 13,01 kN	MFS(11) = -10,74 kN	MFS(12) = -21,49 kN
MFS(13) = -10,74 kN			
MFS(22) = -10,41 kN	MFS(23) = -10,41 kN	MFS(24) = 8,60 kN	MFS(25) = 17,19 kN
MFS(26) = 8,60 kN			
LTF(25) = 17,19 kN	LCF(12) = -21,49 kN		

MFS(27) = 23,43 kN

X1(1) = 0,000 m	Y1(1) = 0,000 m	X1(2) = 1,875 m	Y1(2) = 1,050 m
X1(3) = 3,750 m	Y1(3) = 2,100 m	X1(4) = 5,625 m	Y1(4) = 3,150 m
X1(5) = 2,381 m	Y1(5) = 0,200 m	X1(6) = 4,702 m	Y1(6) = 0,400 m
X1(7) = 6,101 m	Y1(7) = 2,300 m	X1(8) = 15,000 m	Y1(8) = 0,000 m
X1(9) = 13,125 m	Y1(9) = 1,050 m	X1(10) = 11,250 m	Y1(10) = 2,100 m

FX(1) = 2,63 kN	FY(1) = -4,69 kN	FX(2) = 5,25 kN	FY(2) = -9,38 kN
FX(3) = 5,25 kN	FY(3) = -9,38 kN	FX(4) = 5,25 kN	FY(4) = -9,38 kN
FX(5) = 0,00 kN	FY(5) = 0,00 kN	FX(6) = 0,00 kN	FY(6) = 0,00 kN
FX(7) = 0,00 kN	FY(7) = 0,00 kN	FX(8) = 2,10 kN	FY(8) = 3,75 kN
FX(9) = 4,20 kN	FY(9) = 7,50 kN	FX(10) = 4,20 kN	FY(10) = 7,50 kN



2,63 kN $\xrightarrow{15}$ 2,10 kN QW1 QW2

FX(15) = 4,73 kN

Joint load FX(3) and FY(3) forces of joint 3.

$X1(4) - X1(3) = 5,625 - 3,750 = 1,88 \text{ m}$
 $Y1(4) - Y1(3) = 3,150 - 2,100 = 1,05 \text{ m}$

$L1 = \text{Sqr}(1,88^2 + 1,05^2) = \text{Sqr}(4,63) = 2,15 \text{ m}$
 Or click PDATA, with L1 = 2,149 m.

Wind load 5 kN/m over 2,15 m, $5 \times 2,15 = 10,75 \text{ kN}$,
 on joint 3 and 4 $10,75/2 = 5,38 \text{ kN}$

$FX(4)/1,05 = 5,38/2,15$

$FX(4) = 1,05 \times (5,38/2,15) = 2,63 \quad *2 = 5,26 \text{ kN}$

$FY(4)/1,88 = 5,38/2,15$

$FY(4) = 1,88 \times (5,38/2,15) = 4,70 \quad *2 = 9,40 \text{ kN}$

V9=3 L9= 20 m H9= 6 m Z=0.4 m

After input of these data click ProTruss5 and type in TSTRING FY(9)=-7 Enter.

(FY(I) is assumed upward, therefore here a minus sign.)

Next DrawTF, TrussNumb, Calculate, DrawTFD and click go to FDATA.

There click with right mouse button!! AMEFORCES to get D5(,), D6(,) and MF(,).

Fig.1.

Equilibrium of joint 9.

$$\begin{aligned} D5(9,7) &= 8,33 \text{ kN} & D5(9,11) &= -8,33 \text{ kN} \\ D6(9,7) &= -0,33 \text{ kN} & D6(9,11) &= 0,33 \text{ kN} \end{aligned}$$

$$\begin{aligned} D5(9,8) &= 0 \text{ kN} & D5(9,10) &= 0 \text{ kN} \\ D6(9,8) &= -7,00 \text{ kN} & D6(9,10) &= 0 \text{ kN} \end{aligned}$$

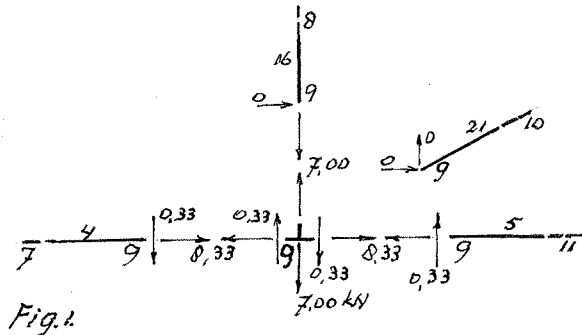


Fig.1

The member end forces acting at the member ends are drawn with their real directions. At the joint act forces as large as but opposite directed.

Fig.2.

member 8

$$\begin{aligned} NAA(2,4) &= 4,86 \text{ kN} & NAA(4,2) &= -4,86 \text{ kN} \\ DAA(2,4) &= 0 \text{ kN} & DAA(4,2) &= 0 \text{ kN} \end{aligned}$$

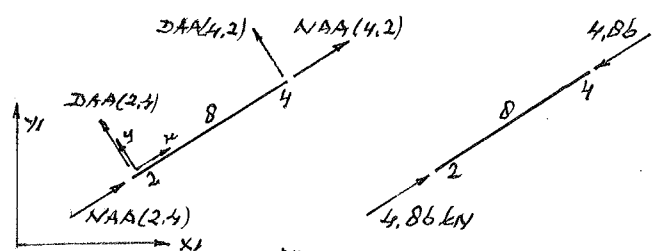
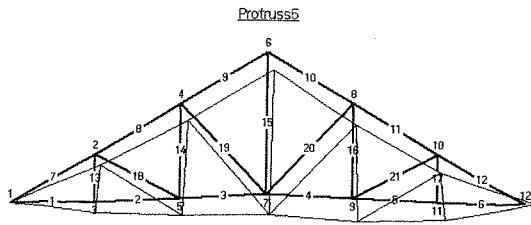


Fig.2.

Figure on the right with member and forces drawn with their real directions, the forces push at the member ends, it's a compression member. It has been agreed to indicate it with a minus sign, so MFS(8)= -4,86 kN.

Fig.3.

Only joint load force FY(9)= -7 kN, and no own weight. There are 6 zero members.... without them the truss would collapse... because of the member end hinges.



V9= 3 L9= 20 m H9= 6 m Z= 0,4 m
N9= 12 joints and P9= 23 members

- group a) the bottom border members 1 to 6
- group b) the top border members 7 to 12
- group c) the vertical plane members 13 to 17
- group d) the sloping plane members 18 to 21

V9=3 L9=20 H9=6 Z=0.4 ProTruss4 ProTruss5 ProTruss6
QE= OK EX4 EX5 EX6 EX8
Loads zero Calculate DrawTF TrussNumb DrawTFD
Alt over again to form FDATA UH(I)=0 UV(I)=4 STORE NR= GET

ProTruss5 the bottom border members			
MFS(1) =	4,17 kN	MFS(2) =	4,17 kN
D5(1,3) =	-4,17	D5(3,5) =	-4,17
D6(1,3) =	-0,17	D6(3,5) =	-0,17
MFS(3) =	4,17 kN	MFS(4) =	8,34 kN
D5(5,7) =	-4,17	D5(7,9) =	-8,33
D6(5,7) =	-0,17	D6(7,9) =	-0,33
MFS(5) =	8,34 kN	MFS(6) =	8,34 kN
D5(9,11) =	-8,33	D5(11,12) =	-8,33
D6(9,11) =	0,33	D6(11,12) =	0,33
LTF(4) =	8,34 kN	LCF(6) =	0,00 kN

ProTruss5 the vertical plane members			
MFS(13) =	0,00 kN	MFS(14) =	0,00 kN
D5(2,3) =	0,00	D5(4,5) =	0,00
D6(2,3) =	0,00	D6(4,5) =	0,00
MFS(15) =	5,00 kN	MFS(16) =	7,00 kN
D5(6,7) =	0,00	D5(8,9) =	0,00
D6(6,7) =	0,00	D6(8,9) =	0,00
MFS(17) =	0,00 kN	MFS(18) =	0,00 kN
D5(10,11) =	0,00	D5(12,13) =	0,00
D6(10,11) =	0,00	D6(12,13) =	0,00
LTF(16) =	7,00 kN	LCF(18) =	0,00 kN

the sloping plane members			
MFS(18) =	0,00 kN	MFS(19) =	0,00 kN
D5(2,5) =	0,00	D5(7,10) =	0,00
D6(2,5) =	0,00	D6(7,10) =	0,00
MFS(20) =	-6,13 kN	MFS(21) =	0,00 kN
D5(7,9) =	4,17	D5(9,12) =	0,00
D6(7,9) =	4,50	D6(9,12) =	0,00
LTF(21) =	0,00 kN	LCF(20) =	-6,13 kN

ProTruss5 the bottom border members			
MFS(1) =	4,17 kN	MFS(2) =	4,17 kN
NAA(1,3) =	-4,17	NAA(3,5) =	-4,17
DAA(1,3) =	0,00	DAA(3,5) =	0,00
MFS(3) =	4,17 kN	MFS(4) =	8,34 kN
NAA(5,7) =	-4,17	NAA(7,9) =	-8,34
DAA(5,7) =	0,00	DAA(7,9) =	0,00
MFS(5) =	8,34 kN	MFS(6) =	8,34 kN
NAA(9,11) =	-8,34	NAA(11,12) =	-8,34
DAA(9,11) =	0,00	DAA(11,12) =	0,00
LTF(4) =	8,34 kN	LCF(6) =	0,00 kN

the top border members			
MFS(7) =	-4,86 kN	MFS(8) =	-4,86 kN
NAA(1,2) =	4,86	NAA(2,4) =	4,86
DAA(1,2) =	0,00	DAA(2,4) =	0,00
MFS(9) =	-4,86 kN	MFS(10) =	-4,86 kN
NAA(4,6) =	4,86	NAA(6,8) =	4,86
DAA(4,6) =	0,00	DAA(6,8) =	0,00
MFS(11) =	-9,72 kN	MFS(12) =	-9,72 kN
NAA(8,10) =	9,72	NAA(10,12) =	9,72
DAA(8,10) =	0,00	DAA(10,12) =	0,00
LTF(8) =	0,00 kN	LCF(11) =	-9,72 kN

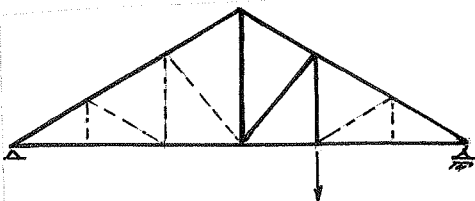
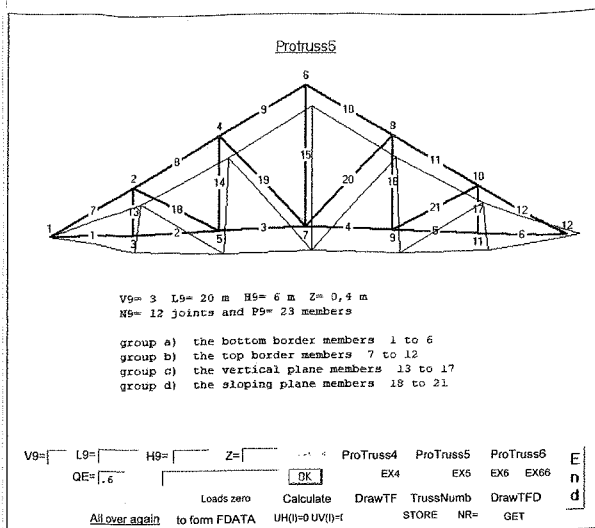


Fig.3.



Example.

V9=3 L9= 20 m H9= 6 m Z=0.4 m
After input of these data click ProTruss5.

Suppose own weight of the members QE=0.6 kN/m. type 0.6 in TOE, at same time all members have For P=1 To P9 QEE(P)=.6. (With input QE not necessary to click ProTruss5 again.) Next DrawTF, TrussNumb, Calculate, DrawTFD, the truss and deformation appear.

Click go to FDATA and click PDATA for member data and X1Y1 for joint coordinates and AMEFORCES to get the member end forces NAA(,), DAA(,) and MFS(,).

Fig.1.

member 8

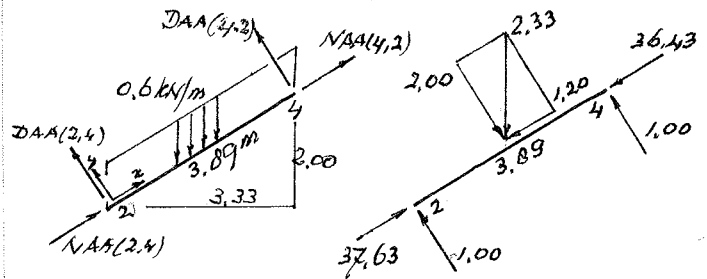
The member ends are hinges. QE= 0,6 kN/m. PDATA gives length L1= 3,887 m.
a= X1(4)-X1(2)= 6,667-3,334= 3,334 m
b= Y1(4)-Y1(2)= 4,000-2,000= 2,000 m
Length L1= Sqr(3,334^2+2,000^2)= 3,888 m

own weight is 3,89*0,6= 2,33 kN

The components are

(2,33/3,89)*3,33= 2,00 kN

(2,33/3,89)*2,00= 1,20 kN



NAA(2,4)= 37,63 kN

NAA(4,2)= -36,43 kN

DAA(2,4)= 1,00 kN

DAA(4,2)= 1,00 kN

These member end forces acting at the member ends are drawn with their real directions. Both forces push at the member ends, compression, 37,63 is larger than 36,43 therefore

MFS(8)= -37,63 kN, a compression member.

Joint load forces FY(2) and FY(4).

Joint load force FY(I) assumed upward.
Joint 2 with FY(2)= -4,02 kN is sum of

member 7	(3,89*0,6)/2= 1,17 kN
member 8	(3,89*0,6)/2= 1,17 kN
member 13	(1,87*0,6)/2= 0,56 kN
member 18	(3,76*0,6)/2= 1,13 kN
	4,03 kN ok

Joint 4 with FY(4)= -4,92 kN

member 7	(3,89*0,6)/2= 1,17 kN
member 8	(3,89*0,6)/2= 1,17 kN
member 13	(3,73*0,6)/2= 1,12 kN
member 18	(3,76*0,6)/2= 1,47 kN
	4,93 kN ok

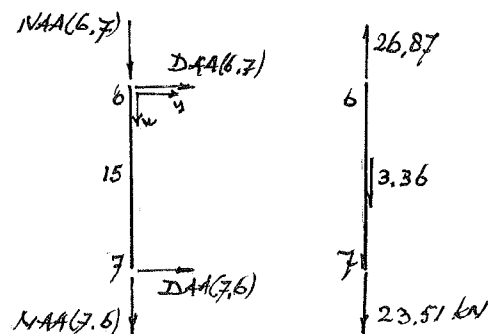
P	All	L1	QE	P	All	L1	QE	P	All	L1	QE	P	All	L1	QE
1	1,00	3,336	0,60	2	1,00	3,336	0,60	3	1,00	3,336	0,60	4	1,00	3,336	0,60
5	1,00	3,336	0,60	6	1,00	3,336	0,60	7	1,00	3,336	0,60	8	1,00	3,336	0,60
9	1,00	3,336	0,60	10	1,00	3,336	0,60	11	1,00	3,336	0,60	12	1,00	3,336	0,60
13	1,00	1,967	0,60	14	1,00	3,733	0,60	15	1,00	5,600	0,60	16	1,00	3,733	0,60
17	1,00	1,967	0,60	18	1,00	3,733	0,60	19	1,00	4,906	0,60	20	1,00	4,906	0,60
21	1,00	3,757	0,60												

X1(1)= 0,000 m	Y1(1)= 0,000 m	X1(2)= 3,333 m	Y1(2)= 2,000 m
X1(3)= 3,333 m	Y1(3)= 3,133 m	X1(4)= 6,667 m	Y1(4)= 4,000 m
X1(5)= 6,667 m	Y1(5)= 3,267 m	X1(6)= 10,000 m	Y1(6)= 4,000 m
X1(7)= 10,000 m	Y1(7)= 0,400 m	X1(8)= 13,333 m	Y1(8)= 2,000 m
X1(9)= 13,333 m	Y1(9)= 0,267 m	X1(10)= 16,667 m	Y1(10)= 0,900 m
X1(11)= 16,667 m	Y1(11)= 0,133 m	X1(12)= 20,000 m	Y1(12)= 0,900 m

FX(1)= 0,00 kN	FY(1)= -2,17 kN	FX(2)= 0,00 kN	FY(2)= -4,02 kN
FX(3)= 0,00 kN	FY(3)= -2,56 kN	FX(4)= 0,00 kN	FY(4)= -4,52 kN
FX(5)= 0,00 kN	FY(5)= -4,26 kN	FX(6)= 0,00 kN	FY(6)= -4,01 kN
FX(7)= 0,00 kN	FY(7)= -6,63 kN	FX(8)= 0,00 kN	FY(8)= -4,52 kN
FX(9)= 0,00 kN	FY(9)= -4,26 kN	FX(10)= 0,00 kN	FY(10)= -4,02 kN
FX(11)= 0,00 kN	FY(11)= -2,56 kN	FX(12)= 0,00 kN	FY(12)= -2,17 kN

the top border members			
MFS(7)= -44,40 kN	NAA(2,1)= -43,28	MFS(8)= -37,63 kN	NAA(4,2)= -36,43
DAA(1,2)= 1,90	DAA(2,1)= 1,00	DAA(2,4)= 1,00	DAA(4,2)= 1,00
MFS(9)= -29,98 kN	NAA(6,4)= -27,79	MFS(10)= -38,98 kN	NAA(8,6)= -29,98
DAA(4,6)= 1,90	DAA(6,4)= 1,00	DAA(6,9)= 1,90	DAA(8,6)= 1,00
MFS(11)= -37,63 kN	NAA(10,8)= -37,63	MFS(12)= -44,43 kN	NAA(12,10)= -44,43
DAA(8,10)= 1,00	DAA(10,8)= 1,00	DAA(10,12)= 1,00	DAA(12,10)= 1,00
LTF(9)= 0,00 kN	LCF(7)= -44,40 kN		

ProTruss5 the vertical plane members			
MFS(13)= 26,87 kN	NAA(3,2)= 2,00	MFS(14)= 8,66 kN	NAA(5,4)= 6,42
DAA(2,3)= 0,90	DAA(3,2)= 0,00	DAA(4,5)= 0,90	DAA(5,4)= 0,90
MFS(15)= 26,87 kN	NAA(7,6)= 23,51	MFS(16)= 8,66 kN	NAA(9,8)= 6,42
DAA(6,7)= 0,90	DAA(7,6)= 0,00	DAA(8,9)= 0,00	DAA(9,8)= 0,00
MFS(17)= 3,12 kN	NAA(11,10)= 2,00		
DAA(10,11)= 0,90	DAA(11,10)= 0,00		
LTF(16)= 26,87 kN	LCF(9)= 0,00 kN		



member 15 Fig.2.

L1= 5,60 m 5,60*0,6= 3,36 kN
NAA(6,7)= -26,87 NAA(7,6)= 23,51 kN
MFS(15)= 26,87 kN, tension member.

ProTruss6

V9= 4 L9= 20 m H9= 2,9 m Z= 1,1 m
 N9= 13 joints and P9= 23 members

group a) the top border members 1 to 8
 group b) the sloping plane members 10 to 15
 group c) the vertical plane members 17 to 20
 group d) the bottom border members 9 16 21 to 23

V9= 4 L9= 20 H9= 2,9 Z= 1,1 Label1 ProTruss4 ProTruss5 ProTruss6
 QE= 0,5 OK EX4 EX5 EX6 EX66
 Loads zero Calculate DrawTF TrussNumb DrawTFD
 All over again to form FDATA UH(0)=0 UV(0)= STORE NR= GET

X1(1) = 0,000 m	Y1(1) = 2,900 m	X1(2) = 2,500 m	Y1(2) = 0,000 m
X1(3) = 2,500 m	Y1(3) = 3,175 m	X1(4) = 5,000 m	Y1(4) = 3,450 m
X1(5) = 7,500 m	Y1(5) = 0,000 m	X1(6) = 7,500 m	Y1(6) = 3,725 m
X1(7) = 10,000 m	Y1(7) = 4,200 m	X1(8) = 12,500 m	Y1(8) = 0,000 m
X1(9) = 12,500 m	Y1(9) = 3,725 m	X1(10) = 15,000 m	Y1(10) = 3,450 m
X1(11) = 17,500 m	Y1(11) = 0,000 m	X1(12) = 17,500 m	Y1(12) = 3,175 m
X1(13) = 20,000 m	Y1(13) = 2,900 m		

UH(1) = 0,00 /EA	UV(1) = 20,76 /EA	UH(13) = 20,76 /EA	UV(13) = 20,76 /EA
UH(2) = 0,00 /EA	UV(2) = 0,00 /EA	UH(2) = -307,28 /EA	UV(2) = -381,81 /EA
UH(3) = 4,28 /EA	UV(3) = -380,52 /EA	UH(4) = -2,48 /EA	UV(4) = -676,75 /EA
UH(5) = -190,48 /EA	UV(5) = -855,80 /EA	UH(6) = -59,84 /EA	UV(6) = -853,56 /EA
UH(7) = -122,17 /EA	UV(7) = -859,06 /EA	UH(8) = -59,84 /EA	UV(8) = -855,80 /EA
UH(9) = -190,50 /EA	UV(9) = -853,56 /EA	UH(10) = -241,51 /EA	UV(10) = -676,75 /EA
UH(11) = 62,94 /EA	UV(11) = -381,81 /EA	UH(12) = -248,62 /EA	UV(12) = -388,32 /EA
UH(13) = -244,34 /EA	UV(13) = 0,00 /EA		

P	All	L1	QE	P	All	L1	QE	P	All	L1	QE	P	All	L1	QE
1	1,00	2,515	0,50	2	1,00	2,515	0,50	3	1,00	2,515	0,50	4	1,00	2,515	0,50
5	1,00	2,515	0,50	6	1,00	2,515	0,50	7	1,00	2,515	0,50	8	1,00	2,515	0,50
9	1,00	3,929	0,50	10	1,00	4,261	0,50	11	1,00	4,261	0,50	12	1,00	4,717	0,50
13	1,00	4,717	0,50	14	1,00	4,261	0,50	15	1,00	4,261	0,50	16	1,00	3,929	0,50
17	1,00	3,175	0,50	18	1,00	3,725	0,50	19	1,00	3,725	0,50	20	1,00	3,175	0,50
21	1,00	5,000	0,50	22	1,00	5,000	0,50	23	1,00	5,000	0,50				

the sloping plane members			
MFS(10) = -14,94 kN		MFS(11) = 8,99 kN	
NAA(2,4) = 14,94	NAA(4,2) = -13,21	NAA(4,5) = -8,99	NAA(5,4) = 7,26
DAA(2,4) = 0,63	DAA(4,2) = 0,62	DAA(4,5) = 0,62	DAA(5,4) = 0,63
MFS(12) = 2,52 kN		MFS(13) = 2,52 kN	
NAA(5,7) = -0,52	NAA(7,5) = 2,52	NAA(7,8) = -2,52	NAA(8,7) = 0,52
DAA(5,7) = 0,63	DAA(7,5) = 0,62	DAA(7,8) = 0,63	DAA(8,7) = 0,62
MFS(14) = 8,99 kN		MFS(15) = -14,94 kN	
NAA(9,10) = -7,26	NAA(10,9) = 8,99	NAA(10,11) = 13,21	NAA(11,10) = -14,94
DAA(9,10) = 0,62	DAA(10,9) = 0,63	DAA(10,11) = 0,62	DAA(11,10) = 0,63
LTF(14) = 8,99 kN	LTF(15) = -14,94 kN		

ProTruss6			
the top border members			
MFS(1) = -15,26 kN	NAA(3,1) = -15,12	MFS(2) = -15,26 kN	NAA(4,3) = -15,12
DAA(1,3) = 0,62	DAA(3,1) = 0,63	DAA(3,4) = 0,63	DAA(4,3) = 0,63
MFS(3) = -28,37 kN	NAA(6,4) = -28,23	MFS(4) = -28,37 kN	NAA(7,6) = -28,23
NAA(4,6) = 0,63	DAA(6,4) = 0,63	DAA(6,7) = 0,63	DAA(7,6) = 0,63
MFS(5) = -28,37 kN	NAA(9,7) = -28,37	MFS(6) = -28,37 kN	NAA(10,9) = -28,37
NAA(7,9) = 28,23	DAA(9,7) = 0,63	NAA(9,10) = 28,23	DAA(10,9) = 0,63
DAA(7,9) = 0,63	DAA(9,7) = 0,63	DAA(9,10) = 0,62	DAA(10,9) = 0,63
MFS(7) = -15,26 kN	NAA(12,10) = -15,26	MFS(8) = -15,26 kN	NAA(13,12) = -15,26
NAA(10,12) = 15,12	DAA(12,10) = 0,63	NAA(12,13) = 15,12	DAA(13,12) = 0,63
DAA(10,12) = 0,62	DAA(12,10) = 0,63	DAA(12,13) = 0,63	DAA(13,12) = 0,62
LTF(10) = 0,00 kN	LTF(11) = -28,37 kN		

Example.

EX6

V9=4 L9= 20 m H9= 2.9 m Z=1.1 m
 After input of these data click ProTruss6.

Suppose own weight of the members QE=0.5 kN/m.
 type 0.5 in TQE.
 Next DrawTF, TrussNumb, Calculate, DrawTFD, the
 truss and the truss deformation is drawn.

Click go to FDATA and click PDATA for member
 data and X1Y1 for joint coordinates and
AMEFORCES to get the member end forces NAA(,),
 DAA(,) and MFS().
 Next page with printer prints with a click
 on AMEFORCESPR.

Fig.1.
 member 11

$$a = X1(5) - X1(4) = 7,50 - 5,00 = 2,50 \text{ m}$$

$$b = Y1(4) - Y1(5) = 3,45 - 0,00 = 3,45 \text{ m}$$

$$L1 = \text{Sqr}(2,50^2 + 3,45^2) = 4,26 \text{ m}$$

$$UH(4) = -2,4 /EA \quad UV(4) = -676,8 /EA$$

$$UH(5) = -190,5 /EA \quad UV(5) = -855,8 /EA$$

The displacements at the member ends are drawn
 here below with real directions, not on same
 scale, otherwise not 'visible'.
 Calculation of the components.

$$\text{joint 4} \quad a = (2,4/4,26) * 2,50 = 1,4 /EA$$

$$b = (676,8/4,26) * 3,45 = 548,1 /EA$$

$$\text{joint 5} \quad c = (190,5/4,26) * 2,50 = 111,8 /EA$$

$$d = (855,8/4,26) * 3,45 = 693,1 /EA$$

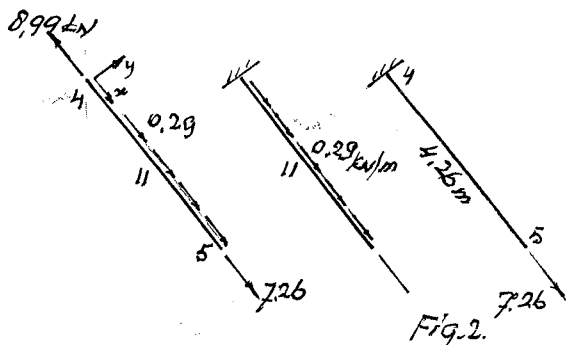


Fig.2.

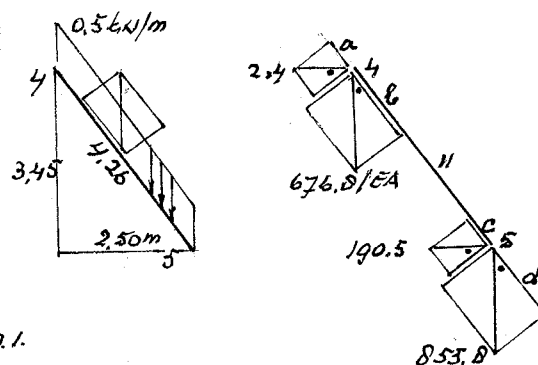


Fig.1.

$$b - a = 548,1 - 1,4 = 546,7 /EA$$

$$d - c = 693,1 - 111,8 = 581,3 /EA$$

$$\text{member 11 lengthens } 581,3 - 546,7 = 34,6 /EA$$

Fig.2.

$$NAA(4,5) = -8,99 \text{ kN} \quad NAA(5,4) = 7,26 \text{ kN}$$

$$MFS(11) = 8,99 \text{ kN}, \text{ a tension member.}$$

Distributed member load along the member is
 $(0,5/4,26) * 3,45 = 0,40 \text{ kN/m}$

$$0,40 * 4,26 = 1,70 \text{ kN} \quad 8,99 - 7,26 = 1,73 \text{ kN} \text{ ok}$$

$$\text{Lengthening due to } 0,40 \text{ kN/m is}$$

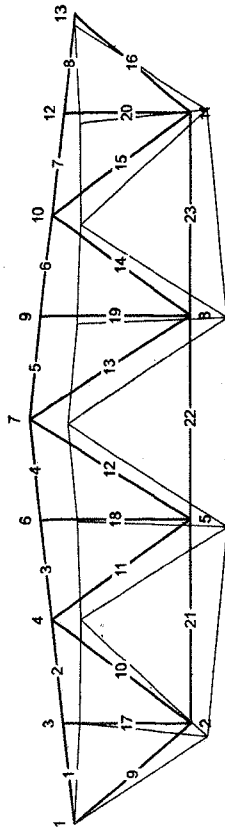
$$(0,4 * 4,26^2) / 2 = 3,63 /EA$$

$$\text{and due to } 7,26 \text{ kN, Hooke,}$$

$$(7,26 * 4,26) / EA = 30,93 /EA, \text{ together}$$

$$3,63 + 30,93 = 34,56 \text{ is } 34,6 /EA. \text{ ok}$$

ProTruss6



V9= 4 I9= 20 m H9= 2,9 m Z= 1,1 m

N9= 13 joints and P9= 23 members

group a) the top border members 1 to 8

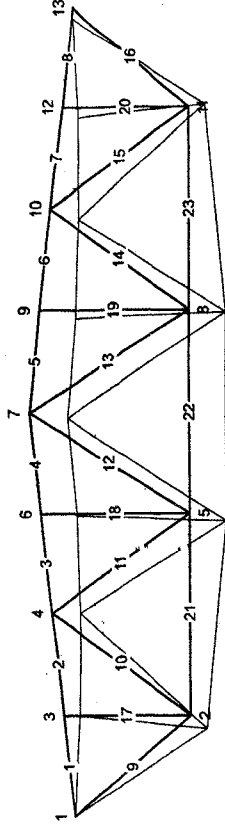
group b) the sloping plane members 10 to 15

group c) the vertical plane members 17 to 20

group d) the bottom border members 9 16 21 to 23

ProTruss6 the top border members		the sloping plane members		the vertical plane members	
MFS(1)	= -15,26 kN	MFS(2)	= -15,26 kN	MFS(17)	= -2,85 kN
NAA(1,3)	= 15,26 kN	NAA(3,4)	= 15,26 kN	NAA(2,3)	= 2,85 kN
DAA(2,3)	= 0,63 kN	DAA(3,4)	= 0,63 kN	NAA(5,6)	= -1,26 kN
MFS(3)	= -28,37 kN	MFS(4)	= -28,37 kN	DAA(5,6)	= 0,00 kN
NAA(4,6)	= 28,37 kN	NAA(6,7)	= 28,37 kN	MFS(18)	= -3,12 kN
DAA(4,6)	= 0,63 kN	DAA(7,6)	= 0,63 kN	NAA(11,12)	= 2,85 kN
MFS(5)	= -28,37 kN	MFS(6)	= -28,37 kN	DAA(11,12)	= 0,00 kN
NAA(7,9)	= 28,37 kN	NAA(9,10)	= 28,37 kN	MFS(19)	= -3,12 kN
DAA(7,9)	= 0,63 kN	DAA(10,9)	= 0,63 kN	NAA(12,11)	= 2,85 kN
MFS(7)	= -15,26 kN	MFS(8)	= -15,26 kN	DAA(12,11)	= 0,00 kN
NAA(10,12)	= 15,26 kN	NAA(12,13)	= 15,26 kN	MFS(20)	= -3,12 kN
DAA(10,12)	= 0,63 kN	DAA(13,12)	= 0,63 kN	NAA(13,11)	= 2,85 kN
LTF(0)	= 0,00 kN	LCF(3)	= -28,37 kN	DAA(13,11)	= 0,63 kN
the bottom border members		the sloping plane members		the vertical plane members	
MFS(10)	= -14,94 kN	MFS(11)	= 8,99 kN	MFS(17)	= -2,85 kN
NAA(2,4)	= 14,94 kN	NAA(4,5)	= -8,99 kN	NAA(2,3)	= 2,85 kN
DAA(2,4)	= 0,63 kN	DAA(5,4)	= 0,62 kN	NAA(5,6)	= -1,26 kN
MFS(12)	= 2,52 kN	MFS(13)	= -2,52 kN	DAA(5,6)	= 0,00 kN
NAA(5,7)	= -0,52 kN	NAA(7,8)	= 2,52 kN	MFS(18)	= -3,12 kN
DAA(5,7)	= 0,63 kN	DAA(8,7)	= -0,63 kN	NAA(11,12)	= 2,85 kN
MFS(14)	= 8,99 kN	MFS(15)	= -14,94 kN	DAA(11,12)	= 0,00 kN
NAA(8,10)	= -7,26 kN	NAA(10,11)	= 13,21 kN	MFS(19)	= -3,12 kN
DAA(8,10)	= 0,62 kN	DAA(10,11)	= 0,62 kN	NAA(12,11)	= 2,85 kN
LTF(14)	= 8,99 kN	LCF(15)	= -14,94 kN	DAA(12,11)	= 0,00 kN
the bottom border members		the sloping plane members		the vertical plane members	
MFS(10)	= -14,94 kN	MFS(11)	= 8,99 kN	MFS(17)	= -2,85 kN
NAA(2,4)	= 14,94 kN	NAA(4,5)	= -8,99 kN	NAA(2,3)	= 2,85 kN
DAA(2,4)	= 0,63 kN	DAA(5,4)	= 0,62 kN	NAA(5,6)	= -1,26 kN
MFS(12)	= 2,52 kN	MFS(13)	= -2,52 kN	DAA(5,6)	= 0,00 kN
NAA(5,7)	= -0,52 kN	NAA(7,8)	= 2,52 kN	MFS(18)	= -3,12 kN
DAA(5,7)	= 0,63 kN	DAA(8,7)	= -0,63 kN	NAA(11,12)	= 2,85 kN
MFS(14)	= 8,99 kN	MFS(15)	= -14,94 kN	DAA(11,12)	= 0,00 kN
NAA(8,10)	= -7,26 kN	NAA(10,11)	= 13,21 kN	MFS(19)	= -3,12 kN
DAA(8,10)	= 0,62 kN	DAA(10,11)	= 0,62 kN	NAA(12,11)	= 2,85 kN
LTF(14)	= 8,99 kN	LCF(15)	= -14,94 kN	DAA(12,11)	= 0,00 kN

ProTruss6



V9= 4 I9= 20 m H9= 2,9 m Z= 1,1 m

N9= 13 joints and P9= 23 members

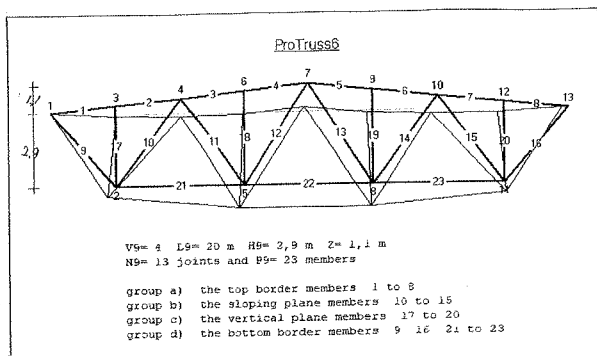
group a) the top border members 1 to 8

group b) the sloping plane members 10 to 15

group c) the vertical plane members 17 to 20

group d) the bottom border members 9 16 21 to 23

ProTruss6 the top border members		the sloping plane members		the vertical plane members	
MFS(1)	= -15,26 kN	MFS(2)	= -15,26 kN	MFS(17)	= -2,85 kN
NAA(1,3)	= 15,26 kN	NAA(3,4)	= 15,26 kN	NAA(2,3)	= 2,85 kN
DAA(2,3)	= 0,63 kN	DAA(3,4)	= 0,63 kN	NAA(5,6)	= -1,26 kN
MFS(3)	= -28,37 kN	MFS(4)	= -28,37 kN	DAA(5,6)	= 0,00 kN
NAA(4,6)	= 28,37 kN	NAA(6,7)	= 28,37 kN	MFS(18)	= -3,12 kN
DAA(4,6)	= 0,63 kN	DAA(7,6)	= 0,63 kN	NAA(11,12)	= 2,85 kN
MFS(5)	= -28,37 kN	MFS(6)	= -28,37 kN	DAA(11,12)	= 0,00 kN
NAA(7,9)	= 28,37 kN	NAA(9,10)	= 28,37 kN	MFS(19)	= -3,12 kN
DAA(7,9)	= 0,63 kN	DAA(10,9)	= 0,63 kN	NAA(12,11)	= 2,85 kN
MFS(7)	= -15,26 kN	MFS(8)	= -15,26 kN	DAA(12,11)	= 0,00 kN
NAA(10,12)	= 15,26 kN	NAA(12,13)	= 15,26 kN	MFS(20)	= -3,12 kN
DAA(10,12)	= 0,63 kN	DAA(13,12)	= 0,63 kN	NAA(13,11)	= 2,85 kN
LTF(0)	= 0,00 kN	LCF(3)	= -28,37 kN	DAA(13,11)	= 0,63 kN
the bottom border members		the sloping plane members		the vertical plane members	
MFS(10)	= -14,94 kN	MFS(11)	= 8,99 kN	MFS(17)	= -2,85 kN
NAA(2,4)	= 14,94 kN	NAA(4,5)	= -8,99 kN	NAA(2,3)	= 2,85 kN
DAA(2,4)	= 0,63 kN	DAA(5,4)	= 0,62 kN	NAA(5,6)	= -1,26 kN
MFS(12)	= 2,52 kN	MFS(13)	= -2,52 kN	DAA(5,6)	= 0,00 kN
NAA(5,7)	= -0,52 kN	NAA(7,8)	= 2,52 kN	MFS(18)	= -3,12 kN
DAA(5,7)	= 0,63 kN	DAA(8,7)	= -0,63 kN	NAA(11,12)	= 2,85 kN
MFS(14)	= 8,99 kN	MFS(15)	= -14,94 kN	DAA(11,12)	= 0,00 kN
NAA(8,10)	= -7,26 kN	NAA(10,11)	= 13,21 kN	MFS(19)	= -3,12 kN
DAA(8,10)	= 0,62 kN	DAA(10,11)	= 0,62 kN	NAA(12,11)	= 2,85 kN
LTF(14)	= 8,99 kN	LCF(15)	= -14,94 kN	DAA(12,11)	= 0,00 kN
the bottom border members		the sloping plane members		the vertical plane members	
MFS(10)	= -14,94 kN	MFS(11)	= 8,99 kN	MFS(17)	= -2,85 kN
NAA(2,4)	= 14,94 kN	NAA(4,5)	= -8,99 kN	NAA(2,3)	= 2,85 kN
DAA(2,4)	= 0,63 kN	DAA(5,4)	= 0,62 kN	NAA(5,6)	= -1,26 kN
MFS(12)	= 2,52 kN	MFS(13)	= -2,52 kN	DAA(5,6)	= 0,00 kN
NAA(5,7)	= -0,52 kN	NAA(7,8)	= 2,52 kN	MFS(18)	= -3,12 kN
DAA(5,7)	= 0,63 kN	DAA(8,7)	= -0,63 kN	NAA(11,12)	= 2,85 kN
MFS(14)	= 8,99 kN	MFS(15)	= -14,94 kN	DAA(11,12)	= 0,00 kN
NAA(8,10)	= -7,26 kN	NAA(10,11)	= 13,21 kN	MFS(19)	= -3,12 kN
DAA(8,10)	= 0,62 kN	DAA(10,11)	= 0,62 kN	NAA(12,11)	= 2,85 kN
LTF(14)	= 8,99 kN	LCF(15)	= -14,94 kN	DAA(12,11)	= 0,00 kN



UH(1) = 0,00 /EA	UV(1) = 0,00 /EA	RV(13) = 20,76 kN	UH(2) = -307,28 /EA	UV(2) = -381,81 /EA
UH(3) = 4,28 /EA	UV(3) = -388,32 /EA	UH(4) = -2,43 /EA	UV(4) = -676,79 /EA	
UH(5) = -190,49 /EA	UV(5) = -385,80 /EA	UH(6) = -53,44 /EA	UV(6) = -863,96 /EA	
UH(7) = -122,17 /EA	UV(7) = -890,06 /EA	UH(8) = -53,86 /EA	UV(8) = -855,20 /EA	
UH(9) = -190,90 /EA	UV(9) = -383,96 /EA	UH(10) = -241,91 /EA	UV(10) = -676,79 /EA	
UH(11) = 62,94 /EA	UV(11) = -391,81 /EA	UH(12) = -240,62 /EA	UV(12) = -399,22 /EA	
UH(13) = -244,94 /EA	UV(13) = 0,00 /EA			

P	All	L1	QE	P	All	L1	QE	P	All	L1	QE	P	All	L1	QE
1	1,00	2,515	0,50	6	1,00	2,515	0,50	11	1,00	2,515	0,50	16	1,00	2,515	0,50
2	1,00	2,515	0,50	7	1,00	2,515	0,50	12	1,00	2,515	0,50	17	1,00	2,515	0,50
3	1,00	2,515	0,50	8	1,00	2,515	0,50	13	1,00	2,515	0,50	18	1,00	2,515	0,50
4	1,00	2,515	0,50	9	1,00	2,515	0,50	14	1,00	2,515	0,50	19	1,00	2,515	0,50
5	1,00	2,515	0,50	10	1,00	2,515	0,50	15	1,00	2,515	0,50	20	1,00	2,515	0,50
6	1,00	2,515	0,50	11	1,00	2,515	0,50	16	1,00	2,515	0,50	21	1,00	2,515	0,50
7	1,00	2,515	0,50	12	1,00	2,515	0,50	17	1,00	2,515	0,50	22	1,00	2,515	0,50
8	1,00	2,515	0,50	13	1,00	2,515	0,50	18	1,00	2,515	0,50	23	1,00	2,515	0,50
9	1,00	2,515	0,50	14	1,00	2,515	0,50	19	1,00	2,515	0,50				
10	1,00	2,515	0,50	15	1,00	2,515	0,50	20	1,00	2,515	0,50				
11	1,00	2,515	0,50	16	1,00	2,515	0,50	21	1,00	2,515	0,50				
12	1,00	2,515	0,50	17	1,00	2,515	0,50	22	1,00	2,515	0,50				
13	1,00	2,515	0,50	18	1,00	2,515	0,50	23	1,00	2,515	0,50				
14	1,00	2,515	0,50	19	1,00	2,515	0,50								
15	1,00	2,515	0,50	20	1,00	2,515	0,50								
16	1,00	2,515	0,50	21	1,00	2,515	0,50								
17	1,00	2,515	0,50	22	1,00	2,515	0,50								
18	1,00	2,515	0,50	23	1,00	2,515	0,50								
19	1,00	2,515	0,50												
20	1,00	2,515	0,50												
21	1,00	2,515	0,50												
22	1,00	2,515	0,50												
23	1,00	2,515	0,50												

Continuation of preceding two pages, of EX6.

For the supports 1 and 13 are
PV(1)=1, PH(1)=1 and PV(13)=1
which are set when clicking **ProTruss6**.

UH(2)= -307,28 /EA UV(2)= -381,81 /EA
UH(11)= 62,94 /EA UV(11)= -381,81 /EA

Now for supports 2 and 11 will become
PV(2)=1, PH(2)=1 and PV(11)=1.

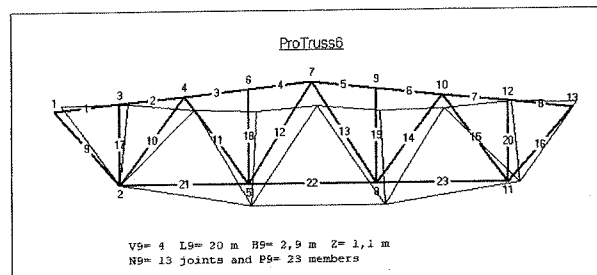
Removing support 1 and 13, to type in TSTRING,
PV(1)=0 Enter, PH(1)=0 Enter and
PV(13)=0 Enter.

For the new supports 2 and 11,
PV(2)=1 Enter, PH(2)=1 Enter and
PV(11)=1 Enter.

Next click **DrawTF**, **TrussNumb**, **Clis** and first
UH(I)=0 UV(I)=0 ! and after that **Calculate** and
DrawTFD. Then go to **FDATA**.
NB If a support displacement is prescribed and
unequal zero, then put in that value after
clicking UH(I)=0 UV(I)=0 before **Calculate**.

Click **UHUV** for UH(I) and UV(I). Since the indi-
cations PV(I) and PH(I) are not printed note
the displacements of the supports
UV(2)=0, UH(2)=0 and UV(11)=0.

And to compare with the case before,
UH(1)= 99,10 /EA UV(1)= 75,76 /EA
UH(13)= 55,78 /EA UV(13)= 75,76 /EA



UH(2) = 99,10 /EA	UV(2) = 0,00 /EA	RV(11) = 20,76 kN	UH(3) = 41,57 /EA	UV(3) = -385,80 /EA
UH(4) = 139,89 /EA	UV(4) = -182,78 /EA		UH(5) = -190,49 /EA	UV(5) = -385,80 /EA
UH(6) = 111,82 /EA	UV(6) = -310,54 /EA		UH(7) = -122,17 /EA	UV(7) = -890,06 /EA
UH(8) = 113,31 /EA	UV(8) = -302,38 /EA		UH(9) = -190,90 /EA	UV(9) = -383,96 /EA
UH(10) = 20,59 /EA	UV(10) = -182,75 /EA		UH(11) = 62,94 /EA	UV(11) = -391,81 /EA
UH(12) = 43,55 /EA	UV(12) = -6,51 /EA		UH(13) = -244,94 /EA	UV(13) = 0,00 /EA

ProTruss6				ProTruss6				ProTruss6				ProTruss6			
the top border members				the sloping plane members				the vertical plane members				the bottom border members			
MFS(1) = 1,33 kN				MFS(2) = 1,33 kN				MFS(3) = 1,33 kN				MFS(4) = 1,33 kN			
D5(1,3) =	-1,25	D5(3,1) =	1,25	D5(4,1) =	-1,25	D5(4,5) =	1,25	D5(4,1) =	-1,25	D5(4,5) =	1,25	D5(4,1) =	-1,25	D5(4,5) =	1,25
D6(1,3) =	0,49	D6(3,1) =	0,77	D6(4,1) =	0,49	D6(4,5) =	0,77	D6(4,1) =	0,49	D6(4,5) =	0,77	D6(4,1) =	0,49	D6(4,5) =	0,77
MFS(5) = -14,19 kN				MFS(6) = -14,19 kN				MFS(7) = -14,19 kN				MFS(8) = -14,19 kN			
D5(5,6) =	-14,19	D5(6,4) =	-14,19	D5(6,7) =	14,19	D5(7,6) =	-14,19	D5(6,7) =	14,19	D5(7,6) =	-14,19	D5(6,7) =	14,19	D5(7,6) =	-14,19
D6(4,6) =	2,19	D6(6,4) =	-0,93	D6(6,7) =	2,19	D6(7,6) =	-0,93	D6(6,7) =	2,19	D6(7,6) =	-0,93	D6(6,7) =	2,19	D6(7,6) =	-0,93
MFS(5) = -14,35 kN				MFS(6) = -14,35 kN				MFS(7) = -14,35 kN				MFS(8) = -14,35 kN			
D5(7,9) =	14,19	D5(9,7) =	-14,19	D5(9,10) =	14,19	D5(10,9) =	-14,19	D5(9,10) =	14,19	D5(10,9) =	-14,19	D5(9,10) =	14,19	D5(10,9) =	-14,19
D6(7,9) =	-0,93	D6(9,7) =	0,93	D6(9,10) =	-0,93	D6(10,9) =	0,93	D6(9,10) =	-0,93	D6(10,9) =	0,93	D6(9,10) =	-0,93	D6(10,9) =	0,93
MFS(7) = 1,33 kN				MFS(8) = 1,33 kN				MFS(9) = 1,33 kN				MFS(10) = 1,33 kN			
D5(10,12) =	-1,25	D5(12,10) =	1,25	D5(12,13) =	-1,25	D5(13,12) =	1,25	D5(12,13) =	-1,25	D5(13,12) =	1,25	D5(12,13) =	-1,25	D5(13,12) =	1,25
D6(10,12) =	0,77	D6(12,10) =	0,49	D6(12,13) =	0,77	D6(13,12) =	0,49	D6(12,13) =	0,77	D6(13,12) =	0,49	D6(12,13) =	0,77	D6(13,12) =	0,49
LTF(10) = 1,92 kN				LCF(9) = -14,35 kN				LTF(11) = 1,92 kN				LCF(10) = -14,35 kN			
the sloping plane members				the sloping plane members				the sloping plane members				the sloping plane members			
MFS(10) = -17,16 kN				MFS(11) = 10,98 kN				MFS(12) = 10,98 kN				MFS(13) = 10,98 kN			
D6(2,4) =	9,56	D6(4,2) =	-9,56	D6(4,3) =	-9,56	D6(5,4) =	9,56	D6(5,4) =	9,56	D6(6,4) =	-9,56	D6(6,4) =	-9,56	D6(7,4) =	9,56
D6(2,12) =	-1,25	D6(4,2) =	-12,13	D6(4,3) =	9,13	D6(5,4) =	-7,05	D6(5,4) =	9,13	D6(6,4) =	-7,05	D6(6,4) =	9,13	D6(7,4) =	-7,05
MFS(12) = -1,25 kN				MFS(13) = -1,25 kN				MFS(14) = -1,25 kN				MFS(15) = -1,25 kN			
D6(5,7) =	0,15	D5(7,5) =	-0,15	D5(7,8) =	-0,15	D6(8,7) =	-0,15	D5(7,8) =	-0,15	D6(8,7) =	-0,15	D5(7,8) =	-0,15	D6(8,7) =	-0,15
D6(5,7) =	1,43	D6(7,5) =	0,93	D6(7,8) =	0,93	D6(8,7) =	0,93	D6(7,8) =	0,93	D6(8,7) =	0,93	D6(7,8) =	0,93	D6(8,7) =	0,93
MFS(14) = 10,98 kN				MFS(15) = -17,16 kN				MFS(16) = -17,16 kN				MFS(17) = -17,16 kN			
D6(8,10) =	-9,59	D5(10,8) =	5,98	D5(10,11) =	5,56	D6(11,10) =	-9,56	D5(10,11) =	5,56	D6(11,10) =	-9,56	D5(10,11) =	5,56	D6(11,10) =	-9,56
D6(8,10) =	-7,05	D6(10,8) =	5,19	D6(10,11) =	-12,13	D6(11,10) =	14,26	D6(10,11) =	-12,13	D6(11,10) =	14,26	D6(10,11) =	-12,13	D6(11,10) =	14,26
LTF(11) = 10,98 kN				LCF(10) = -17,16 kN				LTF(12) = 10,98 kN				LCF(11) = -17,16 kN			

ProTruss6

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
N9=22 joints and P9=41 members

group a) the top border members 1 to 14
group b) the sloping plane members 16 to 27
group c) the vertical plane members 29 to 35
group d) the bottom border members 15 28 36 to 41

V9=7 L9=18.2 H9=2.45 Z=1.1 Label: ProTruss4 ProTruss5 ProTruss6
QE= EX4 EX5 EX6 EX66
OK
Loads zero Calculate DrawTF TrussNumb DrawTFD
All over again to form FDATA UH(0)=0 UV(0)=0 STORE NR= GET

P	All	L1	QE	P	All	L1	QE	P	All	L1	QE	P	All	L1	QE
1	5,00	1,309	0,80	2	5,00	1,309	0,80	3	5,00	1,309	0,80	4	5,00	1,309	0,80
5	5,00	1,309	0,80	6	5,00	1,309	0,80	7	5,00	1,309	0,80	8	5,00	1,309	0,80
9	5,00	1,309	0,80	10	5,00	1,309	0,80	11	5,00	1,309	0,80	12	5,00	1,309	0,80
13	5,00	1,309	0,80	14	5,00	1,309	0,80	15	1,00	2,774	0,16	16	1,00	3,055	0,16
17	1,00	3,055	0,16	18	1,00	3,342	0,16	19	1,00	3,342	0,16	20	1,00	3,342	0,16
21	1,00	3,342	0,16	22	1,00	3,633	0,16	23	1,00	3,633	0,16	24	1,00	3,633	0,16
25	1,00	3,633	0,16	26	1,00	3,924	0,16	27	1,00	3,924	0,16	28	1,00	3,924	0,16
29	1,00	2,607	0,16	30	1,00	2,921	0,16	31	1,00	3,236	0,16	32	1,00	3,550	0,16
33	1,00	3,236	0,16	34	1,00	2,921	0,16	35	1,00	2,607	0,16	36	2,00	2,600	0,32
37	2,00	2,600	0,32	38	2,00	2,600	0,32	39	2,00	2,600	0,32	40	2,00	2,600	0,32
41	2,00	2,600	0,32												

UH(1) = 0,00 /EA	UV(1) = 0,00 /EA	UH(2) = -60,28 /EA	UV(2) = -80,16 /EA
UH(3) = -61,77 /EA	UV(3) = -82,14 /EA	UH(4) = -15,21 /EA	UV(4) = -187,47 /EA
UH(5) = -44,08 /EA	UV(5) = -217,24 /EA	UH(6) = -18,51 /EA	UV(6) = -220,58 /EA
UH(7) = 15,64 /EA	UV(7) = -266,54 /EA	UH(8) = -19,53 /EA	UV(8) = -297,38 /EA
UH(9) = 18,45 /EA	UV(9) = -301,61 /EA	UH(10) = 14,43 /EA	UV(10) = -318,21 /EA
UH(11) = 7,35 /EA	UV(11) = -312,90 /EA	UH(12) = 7,35 /EA	UV(12) = -295,29 /EA
UH(13) = 0,27 /EA	UV(13) = -313,21 /EA	UH(14) = 34,23 /EA	UV(14) = -257,38 /EA
UH(15) = -3,76 /EA	UV(15) = -301,61 /EA	UH(16) = -4,94 /EA	UV(16) = -266,54 /EA
UH(17) = 58,78 /EA	UV(17) = -217,24 /EA	UH(18) = -3,81 /EA	UV(18) = -220,58 /EA
UH(19) = -0,52 /EA	UV(19) = -187,47 /EA	UH(20) = 74,58 /EA	UV(20) = -80,16 /EA
UH(21) = 6,52 /EA	UV(21) = -33,44 /EA	UH(22) = 14,70 /EA	UV(22) = 0,00 /EA

ProTruss6
the bottom border members

MFS(15) = 15,54 kN	MFS(20) = 15,54 kN	NAA(22,20) = 15,54
NAA(1,2) = -15,54	NAA(2,1) = 15,15	NAA(20,22) = 0,10
DAA(1,2) = 0,10	DAA(2,1) = 0,10	DAA(20,22) = 0,10
MFS(36) = 12,46 kN	MFS(37) = 18,08 kN	NAA(8,5) = 18,08
NAA(2,5) = -12,46	NAA(5,2) = 12,46	NAA(5,8) = 0,42
DAA(2,5) = 0,42	DAA(5,2) = 0,42	DAA(5,8) = 0,42
MFS(39) = 20,68 kN	MFS(40) = 20,68 kN	NAA(11,14) = 20,68
NAA(9,11) = -20,68	NAA(11,9) = 20,68	NAA(14,11) = 0,42
DAA(9,11) = 0,42	DAA(11,9) = 0,42	DAA(11,14) = 0,42
MFS(40) = 18,08 kN	MFS(41) = 12,46 kN	NAA(17,20) = 12,46
NAA(14,17) = -18,08	NAA(17,14) = 18,08	NAA(17,20) = 0,42
DAA(14,17) = 0,42	DAA(17,14) = 0,42	DAA(17,20) = 0,42
LCF(10) = 20,68 kN	LCF(10) = 0,00 kN	

ProTruss6

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
N9=22 joints and P9=41 members

group a) the top border members 1 to 14
group b) the sloping plane members 16 to 27
group c) the vertical plane members 29 to 35
group d) the bottom border members 15 28 36 to 41

UH(1) = 0,00 /EA	UV(1) = 0,00 /EA	UH(2) = -16,19 /EA	UV(2) = -27,69 /EA
UH(3) = 2,59 /EA	UV(3) = -30,94 /EA	UH(4) = 4,36 /EA	UV(4) = -48,64 /EA
UH(5) = -10,64 /EA	UV(5) = -69,35 /EA	UH(6) = 4,34 /EA	UV(6) = -64,09 /EA
UH(7) = 3,13 /EA	UV(7) = -59,81 /EA	UH(8) = -8,20 /EA	UV(8) = -51,68 /EA
UH(9) = 1,98 /EA	UV(9) = -55,90 /EA	UH(10) = -2,25 /EA	UV(10) = -28,15 /EA
UH(11) = -4,34 /EA	UV(11) = 0,00 /EA	UH(12) = -4,34 /EA	UV(12) = -6,44 /EA
UH(13) = -6,44 /EA	UV(13) = -28,15 /EA	UH(14) = -3,46 /EA	UV(14) = -51,68 /EA
UH(15) = -10,57 /EA	UV(15) = -55,90 /EA	UH(16) = -11,32 /EA	UV(16) = -59,91 /EA
UH(17) = 1,55 /EA	UV(17) = -48,64 /EA	UH(18) = -13,63 /EA	UV(18) = -64,09 /EA
UH(19) = -13,05 /EA	UV(19) = -48,64 /EA	UH(20) = 7,51 /EA	UV(20) = -27,69 /EA
UH(21) = -11,67 /EA	UV(21) = -30,96 /EA	UH(22) = -8,69 /EA	UV(22) = 0,00 /EA

ProTruss6
the vertical plane members

MFS(25) = -1,46 kN	MFS(30) = -1,51 kN	NAA(5,2) = -1,05
NAA(2,3) = 1,46	NAA(3,2) = -1,05	NAA(2,5) = 0,30
DAA(2,3) = 0,00	DAA(3,2) = 0,00	DAA(2,5) = 0,30
MFS(31) = -1,57 kN	MFS(32) = -2,10 kN	NAA(11,12) = 2,10
NAA(8,9) = 1,57	NAA(9,8) = -1,05	NAA(11,12) = 0,00
DAA(8,9) = 0,00	DAA(9,8) = 0,00	DAA(11,12) = 0,00
MFS(33) = -1,57 kN	MFS(34) = -1,51 kN	NAA(17,18) = 1,51
NAA(14,15) = 1,57	NAA(15,14) = -1,05	NAA(17,18) = 0,00
DAA(14,15) = 0,00	DAA(15,14) = 0,00	DAA(17,18) = 0,00
MFS(35) = -1,46 kN	MFS(36) = -1,46 kN	NAA(21,20) = -1,05
NAA(20,21) = 1,46	NAA(21,20) = -1,05	DAA(20,21) = 0,00
DAA(20,21) = 0,00	DAA(21,20) = 0,00	LCF(12) = -2,20 kN
LCF(10) = 0,00 kN	LCF(12) = -2,20 kN	

Example.

EX66

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
After input of these data click **ProTruss6**.
At the start all A11(P)=1 EA.

Now some changes, strain stiffness 5EA for the members P=1 to 14, in TSTRING **PA11,P1,P2,A1** is **PA11,1,14,5** Enter,
and 2EA for members P=36 to 41, so **PA11,36,41,2** Enter.

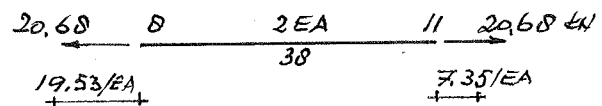
And, just some arbitrarily chosen own weight QEE(P) of groups of members, **PQEE,P1,P2,QE**.
QE=0.8 kN/m for the members 1 to 14, **PQEE,1,14,8** Enter, further

PQEE,15,35,0.16 Enter.

PQEE,36,41,0.32 Enter.

With go to **FDATA** to the second form and click **PDATA** to see the strain stiffnesses and the distributed member loads, back to first form.
Next click **DrawTF**, **TrussNumb**, **Calculate** and **DrawTFD**, the truss plus deformation is drawn.

member 38 L1=2,60 m
NAA(8,11)= -20,68 kN NAA(11,8)= 20,68 kN



UH(8)= -19,53/EA UH(11)= 7,35/EA
The member lengths (19,53+7,35)/EA= 26,88/EA

Hooke (20,68*2,60)/2EA= 26,88/EA ok

Going on with the current case.
Suppose joint 11 is a horizontal roller support, type in TSTRING **PV(11)=1** Enter.
Click **Cls** before drawing again the truss.
Click **DrawTF** and **TrussNumb**, truss with numbering appears, next
UH(I)=0 UV(I)=0 and after that **Calculate** and **DrawTFD** to get the deformation as well.

member 30

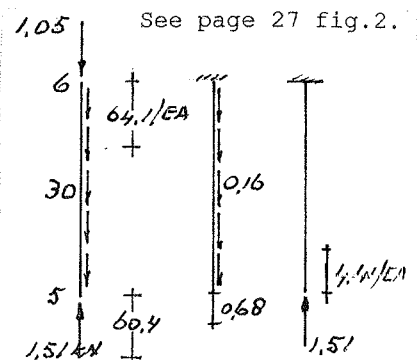
L1=2,92 m

Own weight 0,16 kN/m

NAA(6,5)= -1,05 kN
NAA(5,6)= 1,51 kN

member with 1EA

UV(6)= -64,1/EA
UV(5)= 60,4/EA



Member 30 shortens (64,1-60,4)/EA= 3,7/EA.
Due to 0,32 kN/m (0,16*2,92^2)/2= 0,68/EA.
Due to 1,51 kN (1,51*2,92)/EA= 4,41/EA.

(4,41-0,68)/EA= 3,73/EA is 3,7/EA ok

ProTruss6

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
N9=22 joints and P9=41 members

group a) the top border members 1 to 14
group b) the sloping plane members 16 to 27
group c) the vertical plane members 29 to 35
group d) the bottom border members 15 28 36 to 41

V9=7 L9=18.2 H9=2.45 Z=1.1 Label: ProTruss4 ProTruss5 ProTruss6 E
QE= OK EX4 EX5 EX6 EX66 n
Loads zero Calculate DrawTF TrussNumb DrawTFD d
All over again to form FDATA UH(I)=0 UV(I)=0 STORE NR= GET

P	All	L1	QE	P	All	L1	QE	P	All	L1	QE	P	All	L1	QE
1	5,00	1,305	0,80	2	5,00	1,305	0,80	3	5,00	1,305	0,80	4	5,00	1,305	0,80
5	5,00	1,305	0,80	6	5,00	1,305	0,80	7	5,00	1,305	0,80	8	5,00	1,305	0,80
9	5,00	1,305	0,80	10	5,00	1,305	0,80	11	5,00	1,305	0,80	12	5,00	1,305	0,80
13	5,00	1,305	0,80	14	5,00	1,305	0,80	15	1,00	2,774	0,16	16	1,00	3,055	0,16
17	1,00	3,055	0,16	18	1,00	3,055	0,16	19	1,00	3,055	0,16	20	1,00	3,055	0,16
21	1,00	3,055	0,16	22	1,00	3,055	0,16	23	1,00	3,055	0,16	24	1,00	3,055	0,16
25	1,00	3,055	0,16	26	1,00	3,055	0,16	27	1,00	3,055	0,16	28	1,00	3,055	0,16
29	1,00	3,055	0,16	30	1,00	3,055	0,16	31	1,00	3,055	0,16	32	1,00	3,055	0,16
33	1,00	3,055	0,16	34	1,00	3,055	0,16	35	1,00	3,055	0,16	36	2,00	2,600	0,32
37	2,00	2,600	0,32	38	2,00	2,600	0,32	39	2,00	2,600	0,32	40	2,00	2,600	0,32
41	2,00	2,600	0,32												

RV(1) = 0,00 kN	RV(11) = 15,17 kN	RV(22) = 15,17 kN	UV(2) = -80,16 /EA
UH(1) = 0,00 /EA	UV(11) = 0,00 /EA	UH(12) = -60,28 /EA	UV(4) = -157,47 /EA
UH(3) = 8,17 /EA	UV(3) = -89,44 /EA	UH(4) = 15,21 /EA	UV(6) = -220,98 /EA
UH(5) = -44,08 /EA	UV(5) = -217,24 /EA	UH(6) = 18,51 /EA	UV(8) = -297,39 /EA
UH(7) = 19,64 /EA	UV(7) = -266,54 /EA	UH(8) = -19,53 /EA	UV(10) = -319,21 /EA
UH(9) = 18,45 /EA	UV(9) = -301,61 /EA	UH(10) = 14,63 /EA	
UH(11) = 7,35 /EA	UV(11) = -312,00 /EA	UH(12) = 7,35 /EA	UV(12) = -359,29 /EA
UH(13) = 0,27 /EA	UV(13) = -313,21 /EA	UH(14) = 34,23 /EA	UV(14) = -257,38 /EA
UH(15) = -3,76 /EA	UV(15) = -301,61 /EA	UH(16) = -4,94 /EA	UV(16) = -266,54 /EA
UH(17) = 58,78 /EA	UV(17) = -217,24 /EA	UH(18) = -7,81 /EA	UV(18) = -220,98 /EA
UH(19) = -0,52 /EA	UV(19) = -157,47 /EA	UH(20) = 74,98 /EA	UV(20) = -80,16 /EA
UH(21) = 6,52 /EA	UV(21) = -89,44 /EA	UH(22) = 14,70 /EA	UV(22) = 0,00 /EA

ProTruss6
the bottom border members

HFS(15) = 15,54 kN	NAA(2,1) = 15,15	HFS(20) = 15,54 kN	NAA(22,20) = 15,54
DAA(1,2) = 0,10	DAA(2,1) = 0,10	DAA(20,22) = 0,10	DAA(22,20) = 0,10
HFS(36) = 12,46 kN	NAA(5,2) = 12,46	HFS(37) = 18,88 kN	NAA(8,5) = 18,88
DAA(2,5) = 0,42	DAA(5,2) = 0,42	DAA(5,8) = 0,42	DAA(8,5) = 0,42
HFS(38) = 20,68 kN	NAA(6,11) = 20,68	HFS(41) = 12,46 kN	NAA(11,6) = 12,46
DAA(6,11) = 0,42	DAA(11,6) = 0,42	DAA(11,14) = 0,42	DAA(14,11) = 0,42
HFS(40) = 18,88 kN	NAA(14,17) = 18,88	HFS(41) = 12,46 kN	NAA(17,14) = 12,46
DAA(14,17) = 0,42	DAA(17,14) = 0,42	DAA(17,20) = 0,42	DAA(20,17) = 0,42
LTF(38) = 20,68 kN	LTF(40) = 0,00 kN		

ProTruss6

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
N9=22 joints and P9=41 members

group a) the top border members 1 to 14
group b) the sloping plane members 16 to 27
group c) the vertical plane members 29 to 35
group d) the bottom border members 15 28 36 to 41

RV(1) = 0,00 kN	RV(11) = 6,46 kN	RV(12) = 17,41 kN	RV(22) = 6,46 kN
UH(1) = 0,00 /EA	UV(11) = 0,00 /EA	UH(12) = -16,19 /EA	UV(2) = -27,69 /EA
UH(3) = 2,95 /EA	UV(3) = -30,56 /EA	UH(4) = 4,36 /EA	UV(4) = -48,64 /EA
UH(5) = -10,64 /EA	UV(5) = -60,35 /EA	UH(6) = 4,94 /EA	UV(6) = -64,09 /EA
UH(7) = 3,13 /EA	UV(7) = -59,81 /EA	UH(8) = -5,20 /EA	UV(8) = -51,68 /EA
UH(9) = 1,88 /EA	UV(9) = -58,90 /EA	UH(10) = -2,26 /EA	UV(10) = -28,15 /EA
UH(11) = -4,34 /EA	UV(11) = 0,00 /EA	UH(12) = -4,34 /EA	UV(12) = -6,44 /EA
UH(13) = -6,44 /EA	UV(13) = -28,15 /EA	UH(14) = -3,48 /EA	UV(14) = -51,68 /EA
UH(15) = -10,57 /EA	UV(15) = -58,90 /EA	UH(16) = -11,82 /EA	UV(16) = -59,81 /EA
UH(17) = 1,95 /EA	UV(17) = -60,35 /EA	UH(18) = -13,63 /EA	UV(18) = -64,09 /EA
UH(19) = -13,05 /EA	UV(19) = -60,35 /EA	UH(20) = 7,51 /EA	UV(20) = -27,69 /EA
UH(21) = -11,67 /EA	UV(21) = -30,56 /EA	UH(22) = -8,65 /EA	UV(22) = 0,00 /EA

ProTruss6
the vertical plane members

HFS(29) = -1,46 kN	NAA(3,2) = -1,05	HFS(30) = -1,51 kN	NAA(6,5) = -1,05
DAA(2,3) = 0,00	DAA(3,2) = 0,00	DAA(5,6) = 0,00	DAA(6,5) = 0,00
HFS(32) = -1,57 kN	NAA(8,9) = -1,05	HFS(33) = 2,10 kN	NAA(12,11) = -1,53
DAA(8,9) = 0,00	DAA(9,8) = 0,00	DAA(11,12) = 0,00	DAA(12,11) = 0,00
HFS(39) = -1,57 kN	NAA(15,14) = -1,05	HFS(40) = 1,51 kN	NAA(18,17) = -1,05
DAA(14,15) = 0,00	DAA(15,14) = 0,00	DAA(17,18) = 0,00	DAA(18,17) = 0,00
HFS(35) = -1,46 kN	NAA(21,20) = -1,05		
DAA(20,21) = 0,00	DAA(21,20) = 0,00		
LTF(30) = 0,00 kN	LTF(32) = -2,10 kN		

Example.

EX66

V9=7 L9=18.2 m H9=2.45 m Z=1.1 m
After input of these data click ProTruss6.
At the start all A11(P)=1 EA.

Now some changes, strain stiffness 5EA for the members P=1 to 14, in TSTRING PA11,P1,P2,A1 is PA11,1,14,5 Enter,
and 2EA for members P=36 to 41, so PA11,36,41,2 Enter.

And, just some arbitrarily chosen own weight QEE(P) of groups of members, QEE,P1,P2,QE.
QE=0.8 kN/m for the members 1 to 14, QEE,1,14,0.8 Enter, further

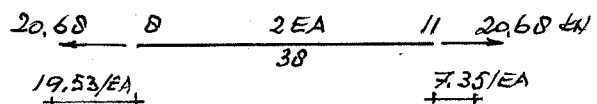
QEE,15,35,0,16 Enter and

QEE,36,41,0,32 Enter.

With go to FDATA to the second form and click PDATA to see the strain stiffnesses and the distributed member loads, back to first form. Next click DrawTF, TrussNumb, Calculate and DrawTFD, the truss plus deformation is drawn.

member 38 L1=2,60 m

NAA(8,11)=-20,68 kN NAA(11,8)=20,68 kN



UH(8)=-19,53/EA UH(11)=7,35/EA
The member lengths (19,53+7,35)/EA=26,88/EA

Hooke (20,68*2,60)/2EA=26,88/EA ok

Going on with the current case.
Suppose joint 11 is a horizontal roller support, type in TSTRING PH(11)=1 Enter.

Click DrawTF and TrussNumb, truss with numbering appears, next
UH(I)=0 UV(I)=0 and after that Calculate and DrawTFD to get the deformation as well.

member 30

L1=2,92 m

Own weight 0,16 kN/m

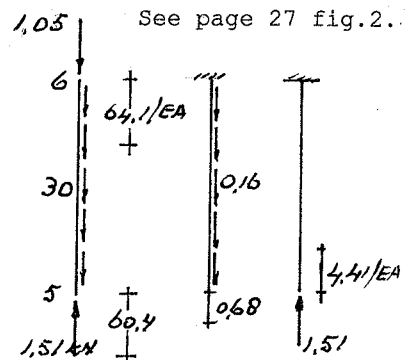
NAA(6,5)=-1,05 kN

NAA(5,6)=1,51 kN

member with 1EA

UV(6)=-64,1/EA

UV(5)=60,4/EA



Member 30 shortens (64,1-60,4)/EA=3,7/EA.
Due to 0,32 kN/m (0,16*2,92^2)/2=0,68/EA.
Due to 1,51 kN (1,51*2,92)/EA=4,41/EA.

(4,41-0,68)/EA=3,73/EA is 3,7/EA ok

```

Private Sub PROTRUSS4()
N9=15 : P9=27 : BW=L9/8 : CH=H9/4
FH=(H9-Z)/2 : D=(H9/2-Z)*H9/(4*BW)
AW=(2*BW+D)/2 : EW=(4*BW-2*AW)/2

```

'The joint data.

T=0 : S=1

For I=1 To 6

If I<5 Then

X1(I)=T*BW : Y1(I)=T*CH

X1(I+7)=L9-T*BW : Y1(I+7)=T*CH

T=T+1

ElseIf I=5 Or I=6 Then

Private Sub PROTRUSS4()

Programming joint and member data of the truss shown below.

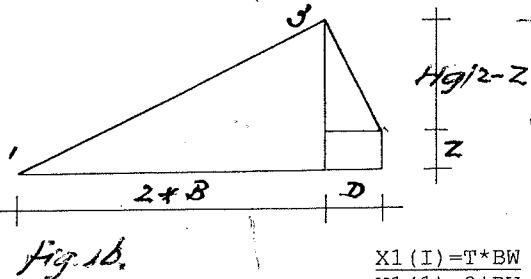
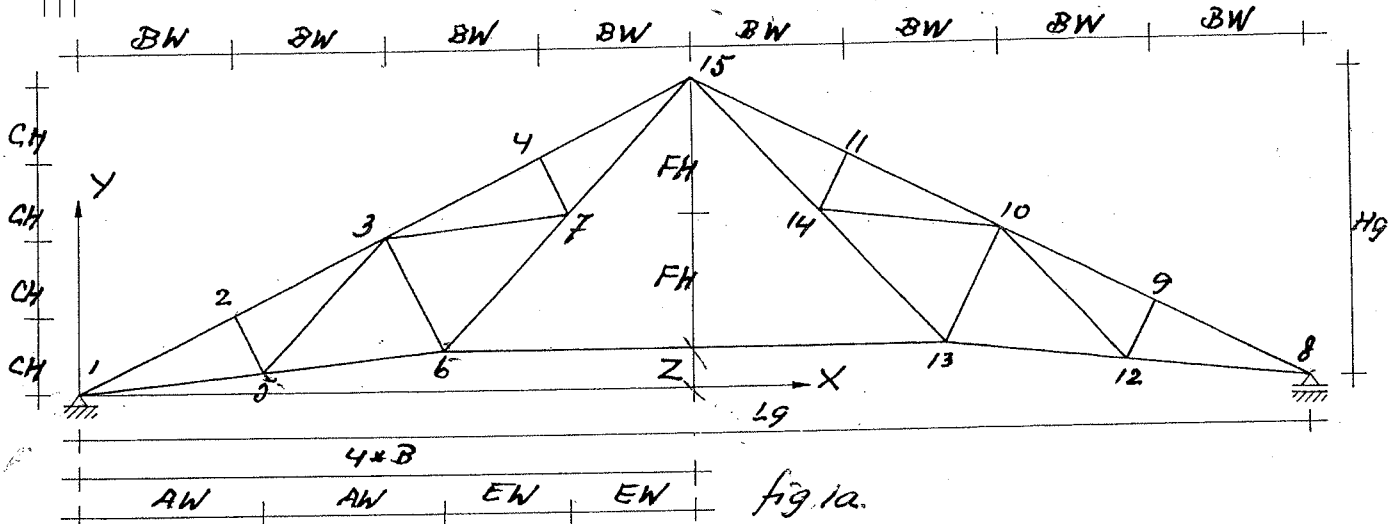
Fig.1a and 1b.

First the basic data, L9, H9 and Z.

The number of joints N9=15, the number of members, see next page, is P9=27.

The joint data.

The joints are numbered as follows, first the left part and then the right part, taking in account the symmetrie of the truss.



Similarity of triangles gives

$D/(H9/2-Z) = H9/(4*BW)$ so that
 $D = (H9/2-Z) * H9/(4*BW)$, then become

$AW = (2*B1+D)/2$ and $EW = (4*B1-2*AW)/2$.

Then the joint coordinates are following. See the code on the left.

X1(I)=T*BW

X1(1)=0*BW

X1(2)=1*BW

X1(3)=2*BW

X1(4)=3*BW

X1(I)=S*AW

X1(5)=1*AW

X1(6)=2*AW

X1(7)=2*AW+EW

X1(I+7)=L9-T*BW

X1(8)=L9-0*BW

X1(9)=L9-1*BW

X1(10)=L9-2*BW

X1(11)=L9-3*BW

X1(I+7)=L9-S*AW

X1(12)=L9-1*AW

X1(13)=L9-2*AW

Y1(I)=T*CH

Y1(1)=0*CH

Y1(2)=1*CH

Y1(3)=2*CH

Y1(4)=3*CH

Y1(I)=S*Z/2

Y1(5)=1*Z/2

Y1(6)=2*Z/2

Y1(I+7)=T*CH

Y1(8)=0*CH

Y1(9)=1*CH

Y1(10)=2*CH

Y1(11)=3*CH

Y1(I+7)=S*Z/2

Y1(12)=1*Z/2

Y1(13)=2*Z/2

X1(I)=S*AW : Y1(I)=S*Z/2

X1(I+7)=L9-S*AW : Y1(I+7)=S*Z/2

S=S+1

End If

Next I

X1(7)=2*AW+EW : Y1(7)=FH+Z

X1(14)=L9-2*AW-EW : Y1(14)=FH+Z

X1(15)=L9/2 : Y1(15)=H9

For I=1 To 15

PH(I)=0 : PV(I)=0

UH(I)=0 : UV(I)=0

SH(I)=0 : SV(I)=0

Next I

PH(1)=1 : PV(1)=1 : PV(8)=1

X1(14)=L9-2*AW-EW Y1(7)=FH+Z Y1(14)=FH+Z
X1(15)=L9/2 Y1(15)=H9

When the coordinates of the joints are known the member lengths L11(P) can be calculated. All other joint data are set zero. After that follow for the supports:

PH(1)=1 because the horizontal displacement of joint 1 is prescribed, and PV(1)=1 and PV(8)=1 because the vertical displacements of these joints are prescribed.

NB. FX(I)=0 : FY(I)=0, and QEE(P)=0 is in PROTRUSS4, -5 and -6 omitted, see page 221.

```

For P=1 To 13
If P<4 Then LL(P)=P : HH(P)=P+1
If P=4 Then LL(P)=4 : HH(P)=15
If P=5 Then LL(P)=1 : HH(P)=5
If P=6 Or P=7 Then
LL(P)=P-1 : HH(P)=P
If P=8 Then LL(P)=7 : HH(P)=15

```

The member data.

Fig.2.

First the members of the left part are numbered in a chosen order as shown here, after that the members of the right part taking into account the symmetrie of the truss.

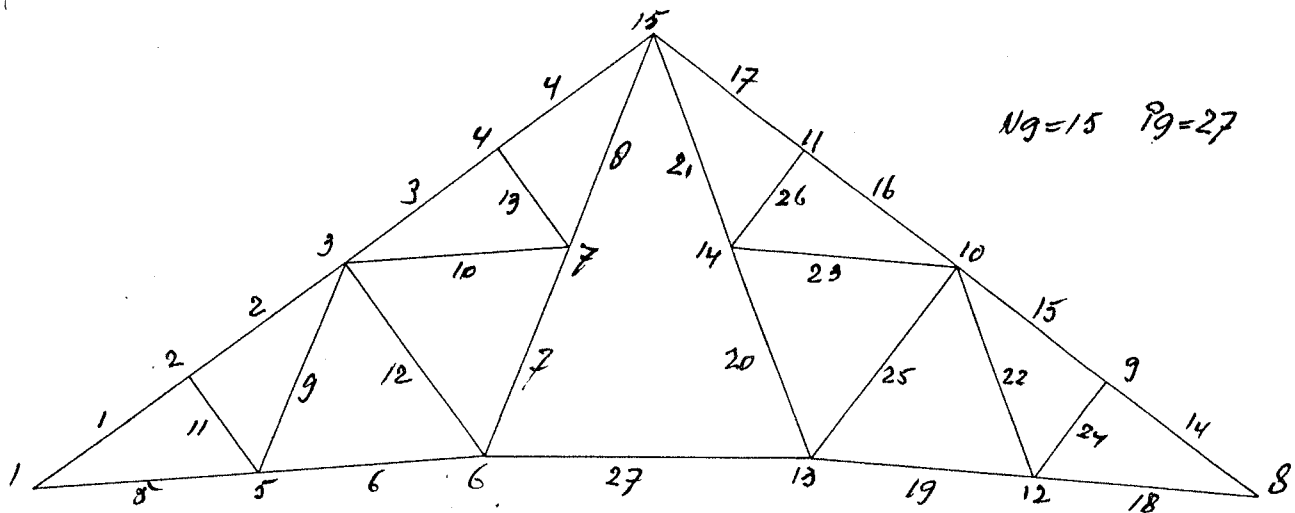


Fig.2.

```

If P=9 Then LL(P)=3 : HH(P)=5
If P=10 Then LL(P)=3 : HH(P)=7
If P>10 Then
LL(P)=P-9 : HH(P)=LL(P)+3
End If
Next P

```

Then follow the the member numbers with their lowest member end numbers LL(P) and highest member end numbers HH(P).

First the data of the first 13 members determined, after that the other 13 members of the right part with $E=P+13$, $LL(P+7)$ and $HH(P+7)$ except member $17=4+13$ and member $21=8+13$ with $LL(P+7)$ and $HH(P+7)$. See the code left above.

```

For P=1 To 13 : E=P+13
If P=4 Or P=8 Then
LL(E)=LL(P)+7 : HH(E)=15
Else
LL(E)=LL(P)+7 : HH(E)=HH(P)+7
End If
Next P : LL(27)=6 : HH(27)=13

For P=1 To P9 : L=LL(P) : H=HH(P)
D1=X1(H)-X1(L) : D2=Y1(H)-Y1(L)
L11(P)=Sqr(D1^2+D2^2)
A11(P)=1 : EAA(P)=A11(P)
Next P
End Sub

```

left part			right part				
P	L	H	P	L	H		
1	1	2	14	8	9	1+7= 8	2+7= 9
2	2	3	15	9	10	2+7= 9	3+7=10
3	3	4	16	10	11		
4	4	15	17	11	15	P=4	
5	1	5	18	8	12		
6	5	6	19	12	13		
7	6	7	20	13	14		
8	7	15	21	14	15	P=8	
9	3	5	22	10	12	3+7=10	5+7=12
10	3	7	23	10	14	3+7=10	7+7=14
11	2	5	24	9	12	2+7= 9	5+7=12
12	3	6	25	10	13		
13	4	7	26	11	14		

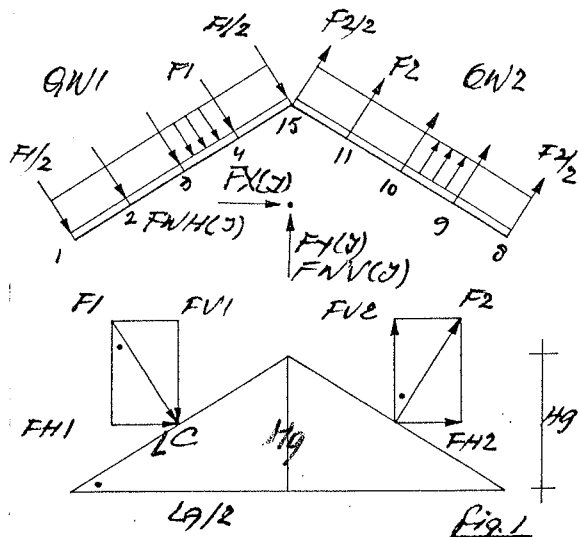
Finally member 27
with $LL(27)=6$ and $HH(27)=13$.

On the left the code for $LL(P)$ and $HH(P)$ for the first 13 members now with Select Case - End Select. There's not much difference in a situation like this, but in other cases it gives great advantages. For instance
If $P=3$ Or $P=7$ Or $P=11$ Or $P=12$
can be shorter when writing
Case 3,7,9,11,12
See page , page .

```

For P = 1 To 13
Select Case P
Case Is < 4 : LL(P)=P : HH(P)=P + 1
Case 4 : LL(P)=4 : HH(P)=15
Case 5 : LL(P)=1 : HH(P)=5
Case 6,7 : LL(P)=P-1 : HH(P)=P
Case 8 : LL(P)=7 : HH(P)=15
Case 9 : LL(P)=3 : HH(P)=5
Case 10 : LL(P)= 3: HH(P)= 7
Case Is > 10: LL(P)=P-9 : HH(P)=
LL(P)+3
End Select
Next P

```



Private Sub WINDLOAD4()

Calculation of joint load forces FWH(I) and FWV(I) due to wind load.
This subroutine belongs to PROTRUSS4 page .

Fig.1.

The wind blows horizontally from the left. Then on the left roof plane acts a wind load QW1 kN/m, wind pressure, and on the right roof plane a wind load QW2 kN/m, wind sucking, both perpendicular to the roof plane. With height H9 and half length L9/2 follows length $LC = \text{Sqr}(H9^2 + (L9/2)^2)$.

On the joints, at the places of the purlins, act the concentrated forces, $F1 = QW1 * LC/4$ and $F1/2$ on the left, and $F2 = QW2 * LC/4$ and $F2/2$ on the right.

With similarity of triangles follow

$$\begin{aligned} FH1/F1 &= H9/LC & \text{then} & \quad FH1 = F1 * H9/LC \\ FV1/F1 &= (L9/2)/LC & \text{then} & \quad FV1 = F1 * (L9/2)/LC \end{aligned}$$

$$\begin{aligned} FH2/F2 &= H9/LC & \text{then} & \quad FH2 = F2 * H9/LC \\ FV2/F2 &= (L9/2)/LC & \text{then} & \quad FV2 = F2 * (L9/2)/LC \end{aligned}$$

Now the horizontal and vertical joint load forces due to the wind, FWH(I) resp. FWV(I), can be written

For I=1 To 15, so for all the joints. This is done with Select Case - End Select.
Case I=1 for which follows, see fig. 1,
 $FWH(I) = FH1/2$: $FWV(I) = -FV1/2$.

The assumption for vertical joint load forces is upward, therefore $-FV1/2$. Then Case 2 To 4 for the joints 2,3 and 4 with $FWH(I) = FH1$: $FWV(I) = -FV1$. And Then Case 8 and Case 9 To 11, and then joint 15 Case 15 with contributions from both sides,
 $FWH(I) = FH1/2 + FH2/2$ and
 $FWV(I) = -FV1/2 + FV2/2$.

Finally Case Else for all the other joints with $FWH(I) = 0$: $FWV(I) = 0$.

End Select

Next I

End Sub

Private Sub SNOWLOAD4()

Calculation of joint load forces FSV(I) due to snow load.

The snow is a vertical distributed load of QS/m on a horizontal plane with length L9, then is $FS = QS * L9/8$ kN.

Now the vertical joint loads FSV(I) can be determined with Select Case - End Select with For I=1 To 15 joints.

Case 1,8 : $FSV(I) = -FS/2$

Case 2,3,4,9,10,11 : $FSV(I) = -FS$

(One can write also Case 2 To 4,9 To 11 :)

And for the other joints without snow load,

Case Else : $FSV(I) = 0$.

End Select

Next I

End Sub

Private Sub WINDLOAD4()

$LC = \text{Sqr}(H9^2 + (L9/2)^2)$

$F1 = QW1 * LC/4$: $F2 = QW2 * LC/4$

$FH1 = F1 * H9/LC$: $FV1 = F1 * (L9/2)/LC$

$FH2 = F2 * H9/LC$: $FV2 = F2 * (L9/2)/LC$

For I=1 To 15

Select Case I

Case 1

$FWH(I) = FH1/2$: $FWV(I) = -FV1/2$

Case 2 To 4

$FWH(I) = FH1$: $FWV(I) = -FV1$

Case 8

$FWH(I) = FH2/2$: $FWV(I) = FV2/2$

Case 9 To 11

$FWH(I) = FH2$: $FWV(I) = FV2$

Case 15

$FWH(I) = FH1/2 + FH2/2$

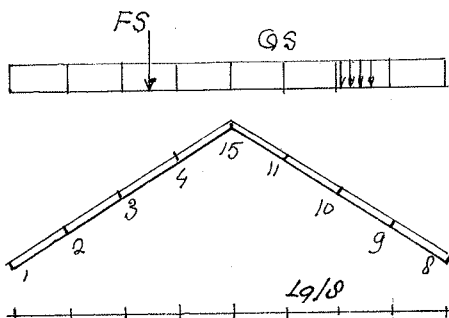
$FWV(I) = -FV1/2 + FV2/2$

Case Else : $FWH(I) = 0$: $FWV(I) = 0$

End Select

Next I

End Sub



Private Sub SNOWLOAD4()

$FS = QS * L9/8$

For I=1 To 15

Select Case I

Case 1,8 : $FSV(I) = -FS/2$

Case 2,3,4,9,10,11 : $FSV(I) = -FS$

Case Else : $FSV(I) = 0$

End Select

Next I

End Sub

```

Private Sub PROTRUSS5()
N9=V9*4 : P9=V9*8-3
BW=L9/(V9*2) : CH=H9/V9
T=0 : S=0
For I=1 To V9*4-1 Step 2
X1(I)=T*BW : Y1(I)=S*Z/V9
T=T+1
If I<V9*2+1 Then S=S+1 Else S=S-1
Next I
X1(N9)=T*BW : Y1(N9)=0

```

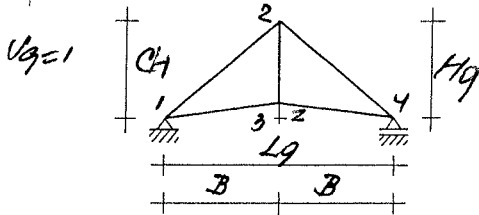


fig.1a.

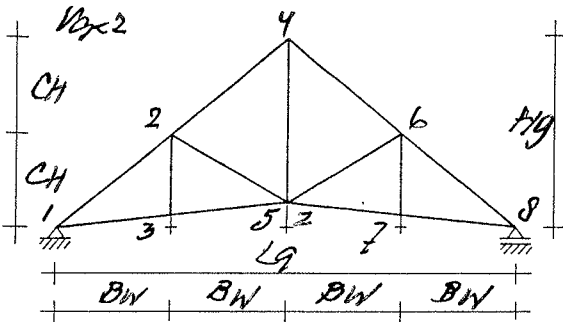


fig.1b

V9=2			V9=3		
I	X1(I)	Y1(I)	I	X1(I)	Y1(I)
	T*BW	S*Z/V9		T*BW	S*Z/V9
1	0*BW	0*Z/2	1	0*BW	0*Z/3
3	1*BW	1*Z/2	3	1*BW	1*Z/3
5	2*BW	2*Z/2	5	2*BW	2*Z/3
7	3*BW	1*Z/2	7	3*BW	3*Z/3
8	4*BW	0*Z/2	9	4*BW	2*Z/3
			11	5*BW	1*Z/3
			12	6*BW	0*Z/3

V9=2			V9=3		
I	X1(I)	Y1(I)	I	X1(I)	Y1(I)
	T*BW	S*CH		T*BW	S*CH
2	1*BW	1*CH	2	1*BW	1*CH
4	2*BW	2*CH	4	2*BW	2*CH
6	3*BW	1*CH	6	3*BW	3*CH
			8	4*BW	2*CH
			10	5*BW	1*CH

```

T=1 : S=1
For I=2 To N9-2 Step 2
X1(I)=T*BW : Y1(I)=S*CH
T=T+1
If I<V9*2 Then S=S+1 Else S=S-1
Next I

```

```

For I=1 To N9
FX(I)=0 : FY(I)=0
PH(I)=0 : PV(I)=0
UH(I)=0 : UV(I)=0
SH(I)=0 : SV(I)=0
Next I
PH(1)=1 : PV(1)=1 : PV(N9)=1

```

Private Sub PROTRUSS5()

Programming joint and member data of the roof truss shown below.

Fig.1a, 1b and 1c.

The basic data are L9, H9, V and Z9.

V9 indicates the size of the construction.

The joint data.

The joints are numbered regularly in a chosen arbitrary way, from left to right. The number of joints are $N9=V9*2$, $BW=L9/(V9*2)$.

V9=1 $N9=1*2=2$ $BW=L9/(1*2)=L9/2$

V9=2 $N9=2*2=4$ $BW=L9/(2*2)=L9/4$

V9=3 $N9=3*2=6$ $BW=L9/(3*2)=L9/6$

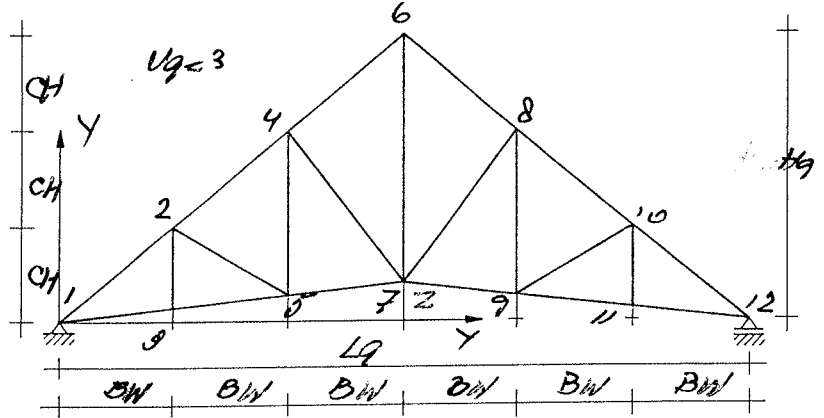


Fig.1c.

The coordinates X1(I) and Y1(I) of the joints of the bottom border are written on the left for V9=2 and V9=3.

See the code on left on top.

The successive joint number difference is 2 except of the last two joints. First T=0 and S=0. For V9=2 and V9=3 follow

For I=1 To 7 and For I=1 To 11 Step 2

Each time after X1(I) and Y1(I) becomes

T=T+1. And as long I<V9*2+1 becomes S=S+1. Is

I>V9*2+1 then is counted back with S=S-1. The last joint N9 is treated seperately, T got the correct value with T=T+1, then X1(N9)=T*BW.

And after that the joint coordinates of the joints at the places of the purlins between first joint 1 and last joint N9. See the code left below.

And after that the joint coordinates of the joints at the places of the purlins between first joint 1 and last joint N9. See the code left below. For I=2 To N9-2 Step 2.

CH=H9/V9 $N9-2$ $V9*2$

V9=1 $CH=H9/1$ $4-2=2$ $1*2=2$

V9=2 $CH=H9/2$ $8-2=6$ $2*2=4$

V9=3 $CH=H9/3$ $12-2=10$ $3*2=6$

The determination of X1(I) and Y1(I) is like before.

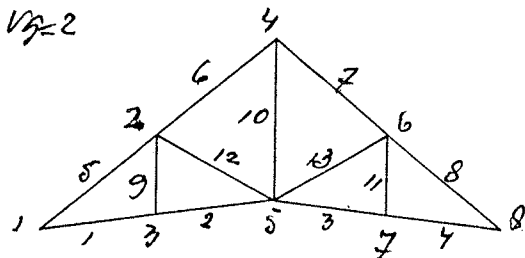
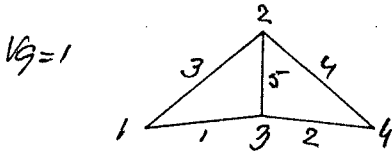
Then all other joint data are set zero. After that for the two supports, joint 1 and N9, follow because of prescribed displacements,

PH(1)=1 : PV(1)=1 : PV(N9)=1.

```

A=1 : B=1 : C=2 : D=2 : E=V9*2+1
For P=1 To P9
'a) The bottom border members.
If P<V9*2 Then
LL(P)=A : HH(P)=A+2 : A=HH(P)
ElseIf P=V9*2 Then
LL(P)=A : HH(P)=A+1

```



$V9=1$ $V9*2=1*2=2$
 $V9=2$ $V9*2=2*2=4$
 $V9=3$ $V9*2=3*2=6$

V9=1			V9=2			V9=3		
P	L	H	P	L	H	P	L	H
			1	1	3	1	1	3
1	1	3	2	3	5	2	3	5
2	3	4	3	5	7	3	5	7
			4	7	8	4	7	9
						5	9	11
						6	11	12

```

'b) The roof border members.
ElseIf P=V9*2+1 Then
LL(P)=B : HH(P)=B+1 : B=HH(P)
ElseIf P>V9*2+1 And P<V9*4+1 Then
LL(P)=B : HH(P)=B+2 : B=HH(P)

```

$V9*2+1$ $V9*4+1$
 $V9=1$ $1*2+1=3$ $1*4+1=5$
 $V9=2$ $2*2+1=5$ $2*4+1=9$
 $V9=3$ $3*2+1=7$ $3*4+1=13$

V9=1			V9=2			V9=3		
P	L	H	P	L	H	P	L	H
						7	1	2
			5	1	2	8	2	4
3	1	2	6	2	4	9	4	6
4	2	4	7	4	6	10	6	8
			8	6	8	11	8	10
						12	10	12

The member data.

Fig.2.

The members are numbered from left to right in the following order:

- The bottom border members,
- the roof border members,
- the vertical plane members, and
- the sloping plane members.

The number of members are $P9=V9*8-3$.

$V9=1$ $P9=1*8-3=8-3=5$
 $V9=2$ $P9=2*8-3=16-3=13$
 $V9=3$ $P9=3*8-3=24-3=21$

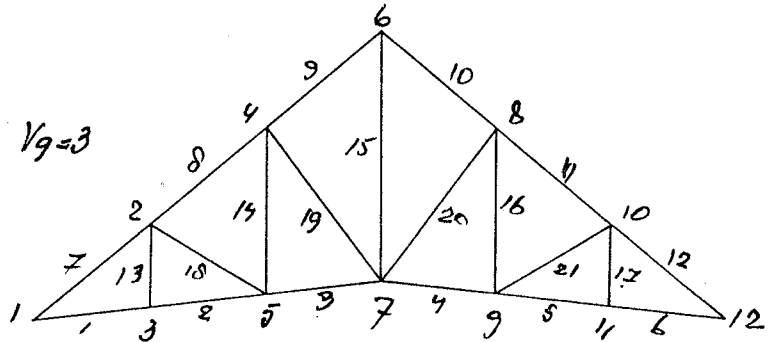


fig.2.

Determination of the lowest and highest member end numbers LL(P and HH(P) of the members P=1 To P9.

- The bottom border members.

For these members the difference between LL(P) and HH(P) is 2 except for the last member $V9*2$ with a difference of 1.

LL(P) of the first member is for every V9

LL(1)=1, therefore first A=1.

Is $P<P9*2$ then LL(P)=A and HH(P)=A+2 and becomes A=HH(P).

For V9=2 then follow

P=1 LL(1)=A=1 HH(1)=A+2=1+2=3 A=HH(1)=3

P=2 LL(2)=A=3 HH(2)=A+2=3+2=5 A=HH(2)=5

P=3 LL(3)=A=5 HH(3)=A+2=5+2=7 A=HH(3)=7

The last member $V9*2=2*2=4$ is taken apart.

Is $P=V9*2$ then LL(P)=A and HH(P)=A+1.

P=4 LL(P)=A=7 HH(P)=A+1=7+1=8

- The roof border members.

The difference between LL(P) and HH(P) is 2 except for the first member $P=V9*2+1$ with a joint number difference of 1. For each V9 is LL(P)=1, therefore first B=1. The first member is taken apart.

If $P=V9*2+1$ then LL(P)=B=1 and HH(P)=B+1=1+1=2, after that becomes B=HH(P), so B=2.

For V9=3 is $P=V9*2+1=3*2+1=6+1=7$ with LL(7)=1 and HH(7)=2, and B=2. Then follows

ElseIf $P>V9*2+1$ And $P<V9*4+1$

$P>3*2+1=6+1=7$ and $P<3*4+1=12+1=13$

P=8 LL(8)=B=2 HH(8)=B+2=2+2=4 B=HH(8)=4

P=9 LL(9)=B=4 HH(9)=B+2=4+2=6 B=HH(9)=6

P=10 LL(10)=B=6 HH(10)=B+2=6+2=8 B=HH(10)=8

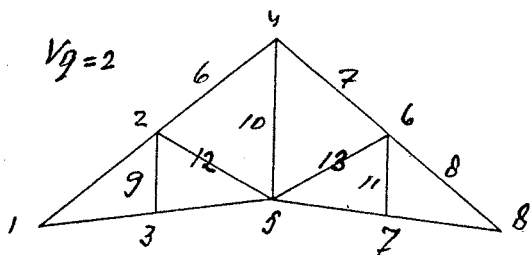
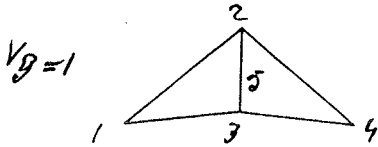
And so for member 11 and 12<13.

```

'c) The vertical plane members.
ElseIf P>=V9*4+1 And P<V9*6 Then
  LL(P)=C : HH(P)=C+1 : C=HH(P)+1

'd) The sloping plane members.
ElseIf P>=V9*6 And P<=V9*7-2 Then
  LL(P)=D : HH(P)=D+3 : D=HH(P)-1
ElseIf P>=V9*7-1 And P<=P9 Then
  LL(P)=E : HH(P)=E+1 : E=HH(P)+1
End If
Next P

```



```

For I=P To P9 : L=LL(P) : H=HH(P)
D1=X1(H)-X1(L) : D2=Y1(H)-Y1(L)
L11(P)=Sqr(D1^2+D2^2)
A11(P)=1 : EAA(P)=A11(P)
Next P
End Sub

```

	V9*4+1	V9*6	V9*7-1	P9
V9=1	5	6	6	5
V9=2	9	12	13	13
V9=3	13	18	20	21

V9=1			V9=2			V9=2		
P	L	H	P	L	H	P	L	H
						13	2	3
			9	2	3	14	4	5
5	2	3	10	4	5	15	6	7
			11	6	7	16	8	9
						17	10	11
						18	2	5
			12	2	5	19	4	7
			13	5	6	20	7	8
						21	9	10

Fig.3.

c) The vertical plane members.

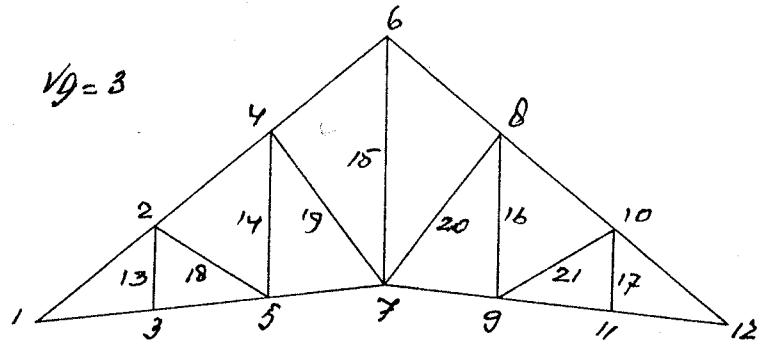
These are the members V9*4+1 to V9*6-1, so
 ElseIf P>=V9*4+1 And P<V9*6

V9=1 P>=1*4+1= 4+1= 5 and P<1*6= 6
 V9=2 P>=2*4+1= 8+1= 9 and P<2*6=12
 V9=3 P>=3*4+1=12+1=13 and P<3*6=18

The difference between the member end numbers LL(P) and HH(P) is 1. Of the vertical member always is LL(P)=2, therefore first C=2, see the preceding page before For P=1 To P9. Then are LL(P)=C and HH(P)=C+1 and becomes C=HH(P)+1 for the next member.

For V9=2 Then follow

P= 9 LL(9)=C=2 HH(9)=C+1=3 C=HH(9)+1= 4
 P=10 LL(10)=C=4 HH(10)=C+1=5 C=HH(10)+1= 6
 P=11 LL(11)=C=6 HH(11)=C+1=7 (C=HH(11)+1= 8)



d) The sloping plane members.

They are divided into two groups.

Left of the middle the members V9*6 To V9*7-2.

ElseIf P>=V9*6 And P<V9*7-1

Of the first member V9*6 is always LL(P)=2, therefore first D=2.

The difference between LL(P) and HH(P) is 3, so LL(P)=D and HH(P)=D+3 and becomes D=HH(P)-1.

For V9=1 follows

ElseIf P>=V9*6=6 And P<V9*7-1=6, there is no member 6 because P9=V9*8-3=1*8-3=5.

For V9=2 follows

ElseIf P>=V9*6=12 And P<V9*7-1=13, so only member 12 with

P=12 LL(12)=D=2 HH(12)=D+3=5 (D=HH(12)-1=4)

For V9=3 follows

ElseIf P>=3*6=18 and P<3*7-1=20, so the members 18 and 19.

P=18 LL(18)=D=2 HH(18)=D+3=5 D=HH(18)-1=4

P=19 LL(19)=D=4 HH(19)=D+3=7 (D=HH(19)-1=6)

Right of the middle the members V9*7-1 To P9.

ElseIf P>=V9*7-1 And P<=P9

For V9=2 then P>=2*7-1=13 to P9=V9*8-3=2*8-3=13.

For the first member always LL(P)=V9*2+1,

therefore first E=V9*2+1. The difference

between LL(P) and HH(P) is 1, so that

LL(P)=E and HH(P)=E+1 and becomes E=HH(P)+1.

For V9=2 follows with first E=V9*2+1=2*2+1=5;

P=13 LL(13)=E=5 HH(13)=E+1=6 (E=HH(P)+1=7)

End Sub

```

Private Sub WINDLOAD5()
  LC=Sqr(H9^2+(L9/2)^2)
  F1=QW1*LC/V9 : F2=QW2*LC/V9
  FH1=F1*H9/LC : FV1=F1*(L9/2)/LC
  FH2=F2*H9/LC : FV2=F2*(L9/2)/LC
  For I=1 To N9
    FWH(I)=0 : FWV(I)=0
  Next I

```

```

  FWH(1)=FH1/2 : FWV(1)=-FV1/2
  FWH(N9)=FH2/2 : FWV(N9)=FV2/2

```

```

  For I=2 To N9-2 Step 2
    If I<V9*2 Then
      FWH(I)=FH1 : FWV(I)=-FV1
    ElseIf I=V9*2 Then
      FWH(I)=FH1/2+FH2/2
      FWV(I)=-FV1/2+FV2/2
    ElseIf I>V9*2 Then
      FWH(I)=FH2 : FWV(I)=FV2
    End If
  Next I

```

```

End Sub

```

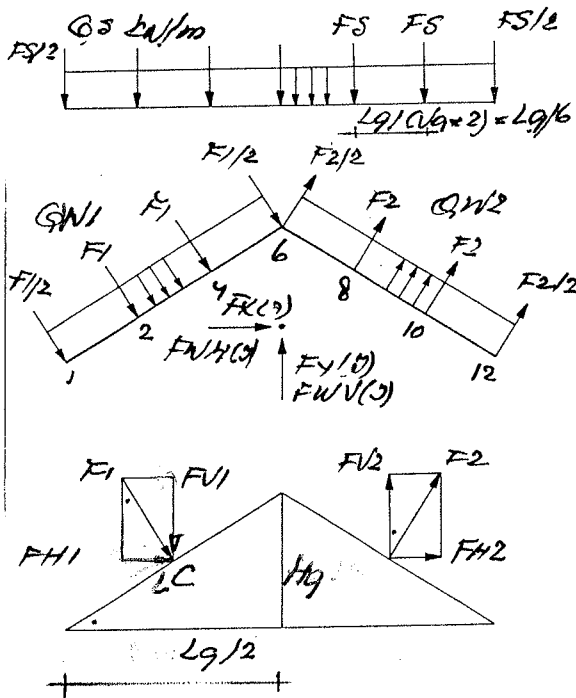


Fig.1.

```

Private Sub SNOWLOAD5()
  FS=QS*L9/(V9*2)
  For I=1 To N9
    FSV(I)=0
  Next I

  FSV(1)=-FS/2 : FSV(N9)=-FS/2

  For I=2 To N9-2 Step 2
    FSV(I)=-FS
  Next I

End Sub

```

Private Sub WINDLOAD5()

Calculation of joint load forces FWH(I) and FWV(I) due to wind load.
This subroutine belongs to PROTRUSS5 dealt with on the preceding pages.

Fig.1.

If the wind blows horizontally from the left then on the left roof border acts a wind load QW1 kN/m (that is snow load in kN/m² times distance in m between the trusses), wind pressure, and on the right roof border QW2 kN/m, wind sucking.
With height H9 and half length/width L9/2 is length LC=Sqr(H9²+(L9/2)²).

On the joints, at the places of the purlins act following concentrated load forces, FW1=QW1*LC/V9 and F1/2 on the left, and FW2=QW2*LC/V9 and F2/2 on the right.
For the figure is V9=3.

With similarity of triangles follow

FH1/F1=H9/LC then FH1=F1*H9/LC
FV1/F1=(L9/2)/LC then FV1=F1*(L9/2)/LC

FH2/F2=H9/LC then FH2=F2*H9/LC
FV2/F2=(L9/2)/LC then FV2=F2*(L9/2)/LC

First for all the N9 joints the wind load forces FWH(I) and FWV(I) are made zero.
Then follow the joint wind load forces for the joints of the roof borders. The first joint 1 and last joint N9 are taken apart;
FWH(1)=FH1/2 : FWV(1)=-FV1/2
FWH(N9)=FH2/2 : FWV(N9)=FV2/2.

After that follow the joints, if V9=3,
For I=2 To N9-2 Step 2. N9=V9*4=3*4=12 so
For I=2 To 12-2=10 Step 2.

If I<V9*2=6 then become
FWH(I)=FH1 and FWV(I)=-FV1.
If I=V9*2 then for the top joint are
FWH(I)=FH1/2+FH2/2 and
FWV(I)=-FV1/2+FV2/2.
If I>V9/2 Then become
FWH(I)=FH2 and FWV(I)=FV2. And Next and
End Sub.

Private Sub SNOWLOAD5()

Calculation of the vertical joint load forces FSV(I) due to snow load.
FS=QS*L9/(V9*2)
First for all joints the forces FSV(I) are made zero. After that follow for joint 1 and N9:
FSV(1)=-FS/2 and FSV(N9)=-FS/2. And then like here above
For I=2 To N9-2 Step 2 but without an exception for the top joint,
FSV(I)=-FS
V9=1 only joint 2, V9=2 joints 2, 4 and 6, and V9=3 the joints 2, 4, 6, 8 and 10.
Next I

End Sub

Private Sub PROTRUSS6()

Programming joint and member data of trusses with construction forms as shown here in the figures.

Fig.1a, 1b, 1c.

To begin with a single 'triangle' with a vertical. With every next figure a triangle with vertical is added.

V9 indicates how 'large' the truss is, the number of triangles with a vertical member.

Basic data are length L9, height H9, Z and V9.

The joint data.

For each triangle with a vertical the joints are numbered as follows. From left joint 1 down and to the right to joint 2, then vertical up to joint 3 and to the right to joint 4. Then for the next triangle starting with 4 down to 5 and up to 6 and to the right to 7. And so on. For each truss V9 the number of joint can be derived from the figures.

$$V9=1 \quad N9=V9*3+1=1*3+1=4 \quad (=4+0*3)$$

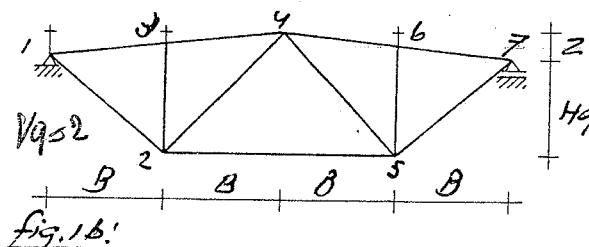
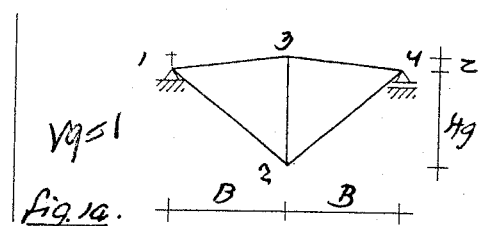
$$V9=2 \quad N9=V9*3+1=2*3+1=7 \quad (=4+1*3)$$

$$V9=3 \quad N9=V9*3+1=3*3+1=10 \quad (=4+2*3)$$

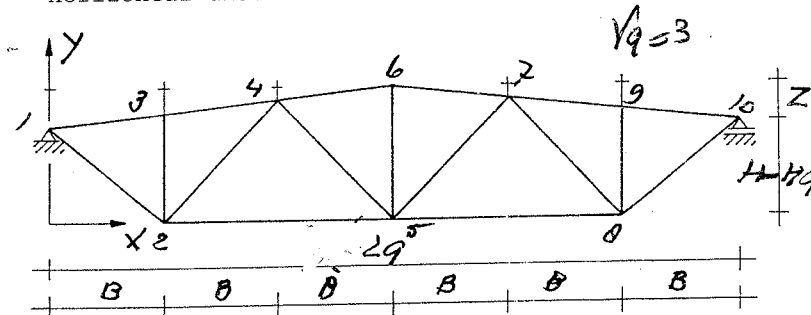
$$\dots$$

$$V9=7 \quad N9=V9*3+1=7*3+1=22 \quad (=4+6*3)$$

Horizontal distance B becomes $B=L9/(V9*2)$.



V9=1	X1(I)=	V9=2	X1(I)=	V9=3	X1(I)=
1	0	1	0	1	0
2	B+0*2*B	2	B+0*2*B	2	B+0*2*B
3	1*B	3	1*B	3	1*B
4	2*B	4	2*B	4	2*B
		5	B+1*2*B	5	B+1*2*B
		6	3*B	6	3*B
		7	4*B	7	4*B
		8	B+2*2*B	8	B+2*2*B
		9	5*B	9	5*B
		10	6*B	10	6*B



Private Sub PROTRUSS6()

N9=V9*3+1 : P9=V9*6-1

H=H9 : B=L9/(V9*2)

X1(I)=0

A=1 : S=0 : T=1

For I=2 To N9

If A=1 Then

X1(I)=B+S*2*B : A=A+1 : S=S+1

Else If A=2 Or A=3 Then

X1(I)=T*B : A=A+1 : T=T+1

End If

If A=4 Then A=1

Next I

The X1-coordinates according to construction axis X.

On the left the joint coordinates are written out for the three figures. Joint 1 is taken apart, X1(1)=0.

Then follow the joints For I=2 To N9.

First A=1 : S=0 : T=1.

If A=1 then follows X1(I)=B+S*2*B for the joints of the bottom border, 2, 2 and 5, 2 and 5 and 8. With A every three joints are counted.

If A=2 or A=3 then is X1(I)=T*B. When A has become 4 then another three joints follow, then A is set A=1 for the next first joint of three. Here below is written out the determination of the X1() coordinates for V9=2.

A=1 S=0 T=1

For I=2 To N9=7

I=2 A=1 X1(2)=B+0*2*B A=A+1=2 S=S+1=1

I=3 A=2 X1(3)=T*B=1*B A=A+1=3 T=T+1=2

I=4 A=3 X1(4)=T*B=2*B A=A+1=4 T=T+1=3

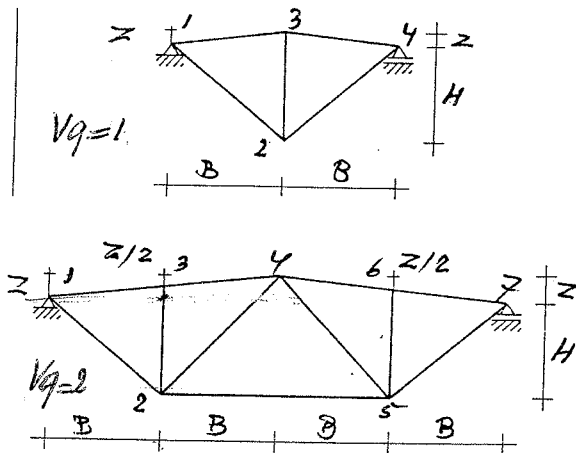
A=4 Is A=4 then becomes A=1.

I=5 A=1 X1(5)=B+1*2*B A=A+1=2 (S=S+1=2)

I=6 A=2 X1(6)=T*B=3*B A=A+1=3 T=T+1=4

I=7 A=3 X1(7)=T*B=4*B (A=A+1=4 T=T+1=5)

V9=1 Y1(I)=		V9=2 Y1(I)=		V9=3 Y1(I)=	
1	H	1	H	1	H
2	0	2	0	2	0
3	H+1*Z/1	3	H+1*Z/2	3	H+1*Z/3
4	H+0*Z/1	4	H+2*Z/2	4	H+2*Z/3
		5	0	5	0
		6	H+1*Z/2	6	H+3*Z/3
		7	H+0*Z/2	7	H+2*Z/3
				8	0
				9	H+1*Z/3
				10	H+0*Z/3



The Y1-coordinates according to construction axis Y.

Fig.2.

On the left the coordinates for the cases V9=1, 2 and 3 are written out.

Joint 1 is taken apart, Y1(1)=H.

First A=1 : S=1 : C=0.

Then follow the joints For I=2 To N9. See the code below on the left.

A=1 for the first joint I=2.

If A=1 then follows Y1(I)=0 for the joint of the bottom border, and becomes A=A+1=1+1=2 for the second joint of three which are counted with A.

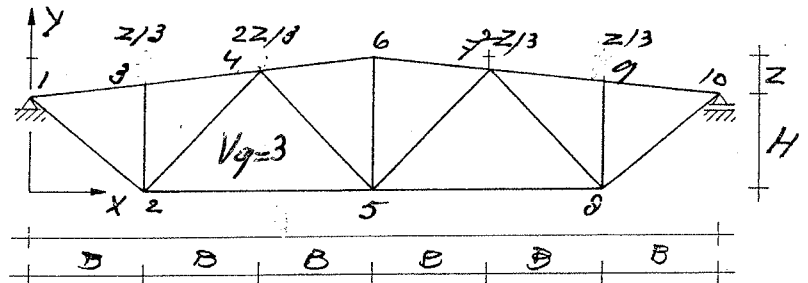
Is A=2 or A=3 then the Y1-coordinates become Y1(I)=H+S*Z/V9, with first S=1.

Starting with joint 3 the joints of the top chord are counted with C, before C=0.

As long as C<V9 the Y1-coordinate of a joint of the top chord becomes larger (up to and including the joint in the middle), and becomes S=S+1.

After the joint in the middle the Y1-coordinate becomes smaller, then becomes S=S-1.

After three joints then has become A=4 and follows A=1 for the next first joint of three.



Below determining the Y1-coordinates for V9=2.

A=1 S=1 C=0

Y1(I)=

I=2 A=1 Y1(2)=0 A=A+1=2

I=3 A=2 Y1(3)=H+1*Z/2 A=A+1=3 C=C+1=1
C=1<V9=2 yes, then S=S+1=2.

I=4 A=3 Y1(4)=H+2*Z/2 A=A+1=4 C=C+1=2
C=2<V9=2 no, now S=S-1=1
A=4 then becomes A=1.

I=5 A=1 Y1(5)=0 A=A+1=2

I=6 A=2 Y1(6)=H+1*Z/2 A=A+1=3 C=C+1=3
C=3<V9=2 no, and thus S=S-1=0.

I=7 A=3 Y1(7)=H+0*Z/2

Before starting the main calculation, (and input of loads), page , the start values of all N9 joint data are made zero. The displacements UH(1) and UV(I) of joint 1, and UV(N9) of joint N9 are prescribed, therefore PH(1)=1, PV(1)=1 and PV(N9)=1.

Y1(1)=H

A=1 : S=1 : C=0

For I=2 To N9

If A=1 Then

Y1(I)=0 : A=A+1

ElseIf A=2 Or A=3 Then

Y1(I)=H+S*Z/V9 : A=A+1 : C=C+1

If C<V9 Then

S=S+1

Else

S=S-1

End If

End If

If A=4 Then A=1

Next I

For I=1 To N9

~~FX(I)=0 : FY(I)=0~~

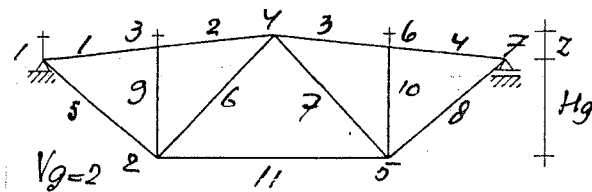
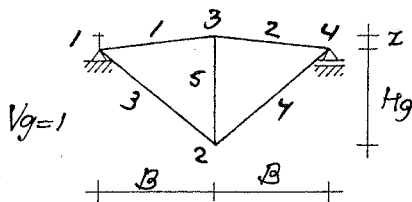
PH(I)=0 : PV(I)=0

UH(I)=0 : UV(I)=0

SH(I)=0 : SV(I)=0

Next I

PH(1)=1 : PV(1)=1 : PV(N9)=1



	V9*2	V9*4	V9*5	P9
V9=1	2	4	5	5
V9=2	4	8	10	11
V9=3	6	12	15	17

V9=1			V9=2			V9=3		
P	L	H	P	L	H	P	L	H
1	1	3	1	1	3	1	1	3
2	3	4	2	3	4	2	3	4
			3	4	6	3	4	6
			4	6	7	4	6	7
						5	7	9
						V9*2=6	9	10
3	1	2	5	1	2	7	1	2
4	2	4	6	2	4	8	2	4
			7	4	5	9	4	5
			8	5	7	10	5	7
						11	7	8
						V9*4=12	8	10
5	2	3	9	2	3	13	2	3
			10	5	6	14	5	6
						V9*5=15	8	9
			11	2	5	16	2	5
						P9=17	5	8

```

P9=V9*6-1
A=1 : B=1
For P=1 To V9*4 Step 2
  If P<V9*2 Then
    LL(P)=A : HH(P)=A+2 : A=HH(P)
    LL(P+1)=A : HH(P+1)=A+1
    A=HH(P+1)
  Else
    LL(P)=B : HH(P)=B+1 : B=HH(P)
    LL(P+1)=B : HH(P+1)=B+2
    B=HH(P+1)
  End If
Next P

```

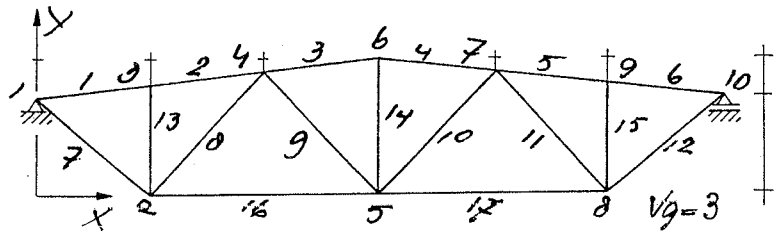
The member data.

The members are numbered from left to right as follows, first

- the top border members, then
- the sloping plane members, next
- the vertical plane members, and finally
- the bottom border members.

For a truss V9 one finds the following numbers of members.

$$\begin{aligned}
 V9=1 & \quad P9=V9*6-1=1*6-1=5 & (5+(V9-1)*6) \\
 V9=2 & \quad P9=V9*6-1=2*6-1=11 & \text{id} \\
 V9=3 & \quad P9=V9*6-1=3*6-1=17 & \text{id}
 \end{aligned}$$



Determination of the lowest and highest member end numbers LL(P) and HH(P).

On the left the member end numbers are given for V9=1 To 3 for the assumed joint numbering.

a) The top border members, number V9*2.

The group is divided into pairs. For the first member of a pair the difference between LL(P) and HH(P) is equal 2, and for the second member of the pair the difference is equal 1. Further is HH(P) of the first member equal to LL(P) of the second member. LL(P) of the first member of the group of top border members is always LL(P)=1, therefore first A=1.

Suppose V9=2, then follow if P<V9*2=4

P=1 P<V9*2 is 1<4 yes
The members 1 and 2.
LL(P)=LL(1)=A=1 HH(1)=A+2=3 A=HH(1)=3
LL(P+1)=LL(2)=A=3 HH(2)=A+1=4 A=HH(2)=4

P=3 P<V9*2 is 3<4 yes
The members 3 and 4.
LL(P)=LL(3)=A=4 HH(3)=A+2=6 A=HH(3)=6
LL(P+1)=LL(4)=A=6 HH(4)=A+1=7
After Next P P has become P=5.

b) The sloping plane members. The number is also V9*2. This group is divided into pairs as well. The difference between LL(P) and HH(P) of the first member of a pair is 1, and of the second member 2.

HH(P) of the first member is equal to LL(P) of the second member.

LL(P) of the first member of this group is for each V9 always one, therefore first B=1. Now going on with V9=2

P=5 P<V9*2 is 5<4 no
The members 5 and 6.
LL(P)=LL(5)=B=1 HH(5)=B+1=2 B=HH(5)=2
LL(P+1)=LL(6)=B=2 HH(6)=B+2=4 B=HH(6)=4

P=7 P<V9*2 is 7<4 no
LL(P)=LL(7)=B=4 HH(7)=B+1=5 B=HH(7)=5
LL(P+1)=LL(8)=B=5 HH(8)=B+2=7

Thus LL(P) and HH(P) of the first V9*4=8 members are determined.

V9=1			V9=2			V9=3		
P	L	H	P	L	H	P	L	H
						V9*4=12	8	10
5	2	3	9	2	3	13	2	3
			10	5	6	14	5	6
						V9*5=15	8	9
			11	2	5	16	2	5
						P9=17	5	8

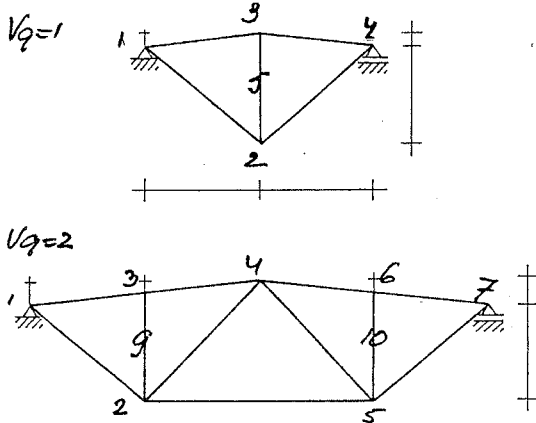


Fig. 4.

```

C=2 : D=2
For P=V9*4+1 To P9
  If P<V9*5+1 Then
    LL(P)=C : HH(P)=C+1 : C=HH(P)+2
  Else
    LL(P)=D : HH(P)=D+3 : D=HH(P)
  End If
  Next P

  For P=1 To P9 : L=LL(P) : H=HH(P)
  D1=X1(H)-X1(L) : D2=Y1(H)-Y1(L)
  L11(P)=SQR(D1^2+D2^2)
  All(P)=1 : EAA(P)=All(P) : QEE(P)=0
  Next P

```

End Sub

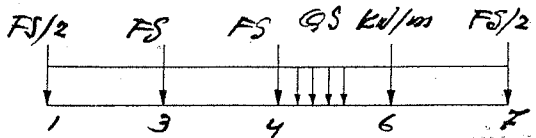


Fig. 5.

```

Private Sub SNOWLOAD6()
  FS=QS*L9/(V9*2)
  For I=1 To N9
    FSV(I)=0
  Next I
  FSV(1)=-FS/2 : FSV(N9)=-FS/2
  For I=3 To N9-1 Step 3
    If I<N9-1 Then
      FSV(I)=-FS : FSV(I+1)=-FS
    Else
      FSV(I)=-FS
    End If
  Next I
End Sub

```

End Sub

c) The vertical plane members.

Fig. 4.

These are the members V9*4+1 to V9*5. For each V9 for the first member of this group is always LL(P)=2, therefore first C=2. The difference between LL(P) and HH(P) is always 1, and LL(P) of a next member is equal to HH(P) of the preceding member plus 2.

With V9=3 is

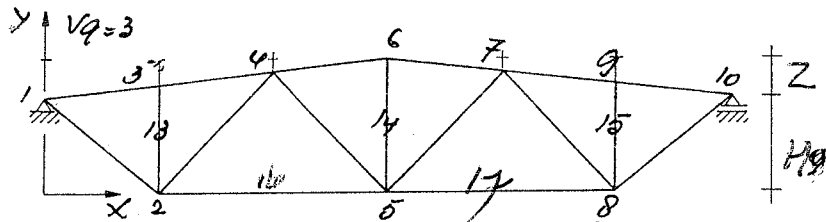
the first member V9*4+1=3*4+1=13, and the last member of the group is V9*5=3*5=15.

For P=V9*4+1 To P9=13 To 17

```

P=13  P<V9*5+1 is 13<16? yes
      LL(13)=C=2  HH(13)=C+1=3  C=HH(13)+2=5
P=14  14<16? yes
      LL(14)=C=5  HH(14)=C+1=6  C=HH(14)+2=8
P=15  15<16? yes
      LL(15)=C=8  HH(15)=C+1=9

```



d) The bottom border members.

These are the members V9*5+1 to P9. If V9=3 the members 16 and 17.

Of the first member of this group always is LL(P)=2, therefore first D=2.

The difference between LL(P) and HH(P) is always 3, and LL(P) of a next member is equal to HH(P) of the preceding member.

```

P=16  P<V9*5+1 is 16<16? no, then Else
      LL(16)=D=2  HH(16)=D+3=5  D=HH(16)=5
P=17  17<16? no
      LL(17)=D=5  HH(17)=D+3=8

```

And when V9=1?

For P=V9*4+1 To P9=5 To 5

```

P=5  P<V9*5+1 is 5<6? yes
      LL(5)=C=2  HH(5)=C+1=3
      for the vertical member.

```

With Next P becomes P=6, end of For-Next. There is no bottom border member P=6 for V9=1.

Next the member lengths are calculated and the strain stiffness becomes EAA(P)=1, and own weight is set QEE(P)=0.

End Sub.

Private Sub SNOWLOAD6() (see page)
Calculation of joint load forces of the top border due to snow load.

Fig. 5.

Due to QS kN/m is FS=QS*L9/(V9*2).

All N9 vertical forces FSV(I) are first set zero. For joint 1 and joint N9 follow FSV(1)=-FS/2 and FSV(N9)=-FS/2.

The first joint with a 'whole' FS is always joint 3, the last with FS joint N9-1.

For I=3 To N9-1 Step 3 With V9=2 as follows, For I=3 To 6 Step 3

```

I=3  3<N9-1=6? yes
      FSV(3)=-FS and FSV(3+1)=FSV(4)=-FS
I=6  6<6? no  FSV(6)=-FS

```

End Sub.